



(12) **United States Patent**  
**Mahgerefteh et al.**

(10) **Patent No.:** **US 9,405,066 B2**  
(45) **Date of Patent:** **Aug. 2, 2016**

(54) **TWO-STAGE ADIABATICALLY COUPLED PHOTONIC SYSTEMS**

(71) Applicant: **FINISAR CORPORATION**,  
Sunnyvale, CA (US)

(72) Inventors: **Daniel Mahgerefteh**, Los Angeles, CA (US); **Bryan Park**, Sunnyvale, CA (US); **Jianxiao Chen**, Fremont, CA (US); **Xiaojie Xu**, Pleasanton, CA (US); **Gilles P. Denoyer**, San Jose, CA (US); **Bernd Huebner**, Mountain View, CA (US)

(73) Assignee: **FINISAR CORPORATION**,  
Sunnyvale, CA (US)

(\*) Notice: Subject to any disclaimer, the term of this patent is extended or adjusted under 35 U.S.C. 154(b) by 0 days.

(21) Appl. No.: **14/938,815**

(22) Filed: **Nov. 11, 2015**

(65) **Prior Publication Data**

US 2016/0131837 A1 May 12, 2016

#### Related U.S. Application Data

(60) Provisional application No. 62/078,259, filed on Nov. 11, 2014, provisional application No. 62/120,194, filed on Feb. 24, 2015, provisional application No. 62/181,679, filed on Jun. 18, 2015, provisional application No. 62/238,542, filed on Oct. 7, 2015.

(51) **Int. Cl.**  
**G02B 6/12** (2006.01)  
**G02B 6/122** (2006.01)  
(Continued)

(52) **U.S. Cl.**  
CPC ..... **G02B 6/1228** (2013.01); **G02B 6/12016** (2013.01); **G02B 6/136** (2013.01);  
(Continued)

(58) **Field of Classification Search**

CPC .. G02B 6/1228; G02B 6/12002; G02B 6/131; G02B 6/4257; G02B 6/12004; G02B 6/305; G02B 6/14; G02B 2006/12152  
USPC ..... 385/14, 27, 31, 43, 50  
See application file for complete search history.

(56) **References Cited**

#### U.S. PATENT DOCUMENTS

7,532,784 B2 \* 5/2009 Tolshikhin ..... G02B 6/12007 385/14  
8,041,164 B2 \* 10/2011 Granstrand ..... B82Y 20/00 29/600

(Continued)

#### FOREIGN PATENT DOCUMENTS

EP 0389172 A2 9/1990  
EP 0561672 A1 9/1993

(Continued)

#### OTHER PUBLICATIONS

Shani et al., "Integrated optic adiabatic devices on silicon", IEEE Journal of Quantum Electronics, IEEE Service center, vol. 27, Issue 3, Mar. 1, 1991, pp. 556-566 (11 pages).

(Continued)

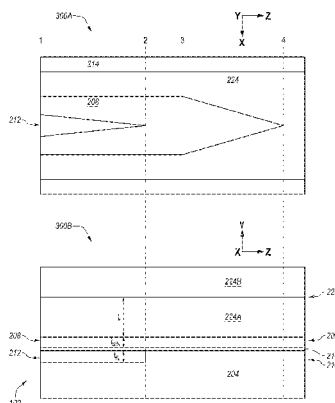
*Primary Examiner* — Ellen Kim

(74) *Attorney, Agent, or Firm* — Maschoff Brennan

(57) **ABSTRACT**

In an example, a coupled system includes a first waveguide, at least one second waveguide, and an interposer. The first waveguide has a first refractive index  $n_1$  and a tapered end. The at least one second waveguide each has a second refractive index  $n_2$ . The interposer includes a third waveguide having a third refractive index  $n_3$  and a coupler portion, where  $n_1 > n_2 > n_3$ . The tapered end of the first waveguide is adiabatically coupled to a coupler portion of one of the at least one second waveguide. A tapered end of one of the at least one second waveguide is adiabatically coupled to the coupler portion of the third waveguide of the interposer. The coupled system is configured to adiabatically couple light between the first waveguide and the at least one second waveguide and between the at least one second waveguide and the third waveguide.

**24 Claims, 50 Drawing Sheets**



- (51) **Int. Cl.**
- |                   |           |                  |         |               |              |
|-------------------|-----------|------------------|---------|---------------|--------------|
| <b>G02B 6/14</b>  | (2006.01) | 2015/0316720 A1* | 11/2015 | Yang .....    | G02B 6/305   |
| <b>G02B 6/32</b>  | (2006.01) | 2015/0338577 A1* | 11/2015 | Shi .....     | 385/14       |
| <b>G02B 6/293</b> | (2006.01) |                  |         |               | G02B 6/126   |
| <b>G02B 6/136</b> | (2006.01) | 2016/0047983 A1* | 2/2016  | Collins ..... | 385/11       |
| <b>G02B 6/30</b>  | (2006.01) |                  |         |               | G02B 6/12002 |
| <b>G02B 6/42</b>  | (2006.01) |                  |         |               | 385/14       |

## FOREIGN PATENT DOCUMENTS

- (52) **U.S. Cl.**
- |           |  |    |                |         |
|-----------|--|----|----------------|---------|
| CPC ..... | <b>G02B 6/14</b> (2013.01); <b>G02B 6/2938</b>           | EP | 2664949 A2     | 11/2013 |
|           | (2013.01); <b>G02B 6/305</b> (2013.01); <b>G02B 6/32</b> | JP | H05 216079 A   | 8/1993  |
|           | (2013.01); <b>G02B 6/423</b> (2013.01); <b>G02B</b>      | WO | 01/88577 A1    | 11/2001 |
|           | <b>2006/12061</b> (2013.01); <b>G02B 2006/12069</b>      | WO | 2009/106139 A1 | 9/2009  |
|           | (2013.01); <b>G02B 2006/12121</b> (2013.01); <b>G02B</b> | WO | 2009/106140 A1 | 9/2009  |
|           | <b>2006/12123</b> (2013.01); <b>G02B 2006/12147</b>      |    |                |         |
|           | (2013.01); <b>G02B 2006/12157</b> (2013.01)              |    |                |         |

## OTHER PUBLICATIONS

(56) **References Cited**

## U.S. PATENT DOCUMENTS

- |                  |         |                 |              |
|------------------|---------|-----------------|--------------|
| 2003/0081902 A1* | 5/2003  | Blauvelt .....  | G02B 6/12002 |
|                  |         |                 | 385/50       |
| 2009/0324163 A1* | 12/2009 | Dougherty ..... | B82Y 20/00   |
|                  |         |                 | 385/14       |
| 2012/0093456 A1* | 4/2012  | Taillaert ..... | G02B 6/1228  |
|                  |         |                 | 385/14       |

International Search Report and Written Opinion mailed May 23, 2016, as received in Application No. PCT/US2015/060223 (13 Pages).

International Search Report and Written Opinion mailed May 13, 2016, as received in Application No. PCT/US2015/060224 (11 Pages).

Shani et al., "Integrated optic adiabatic devices on silicon", Applied Physics Letter, American Institute of Physics, vol. 56, No. 2, Jan. 8, 1990, pp. 120-121, (2 pages).

\* cited by examiner

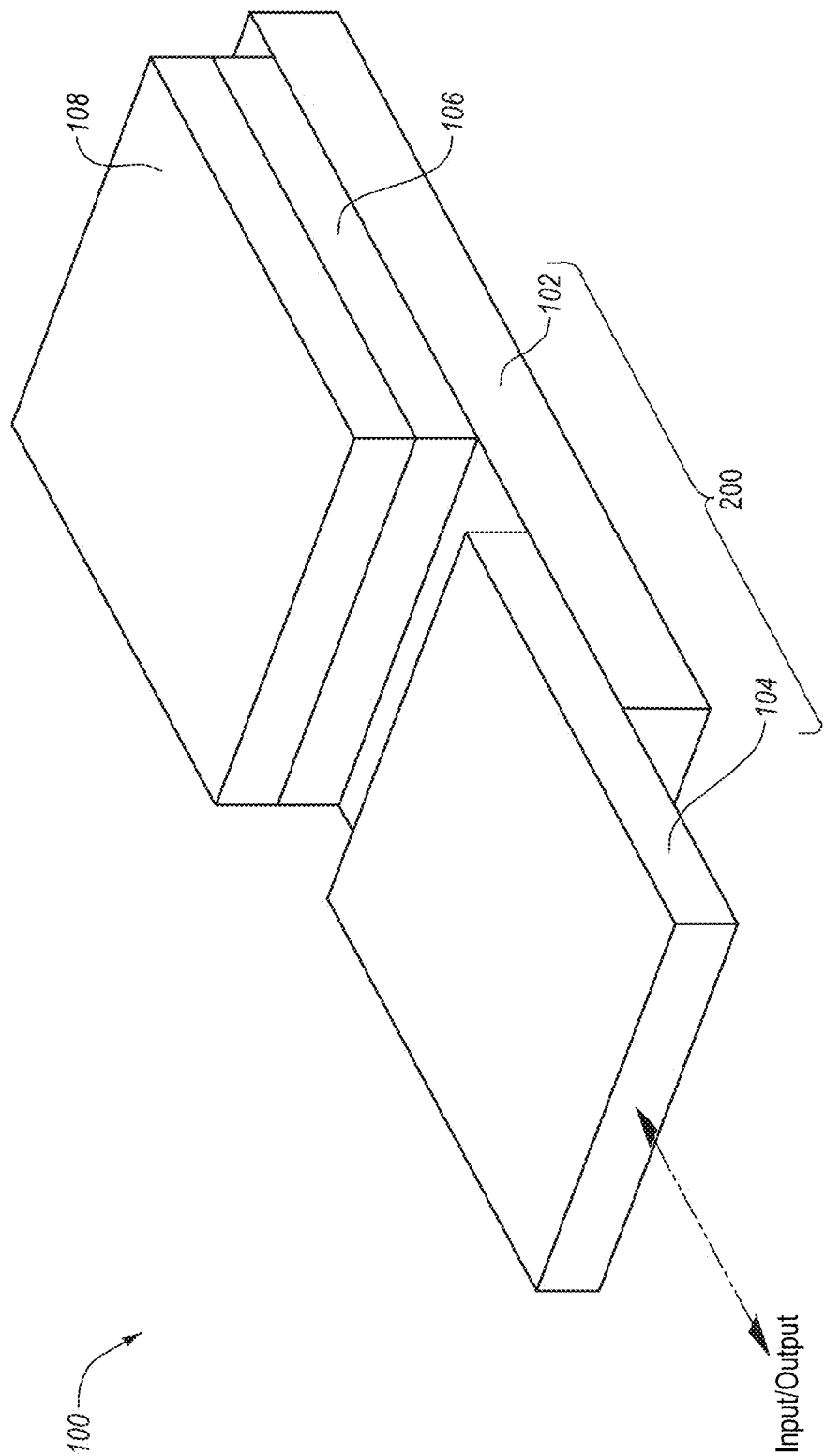
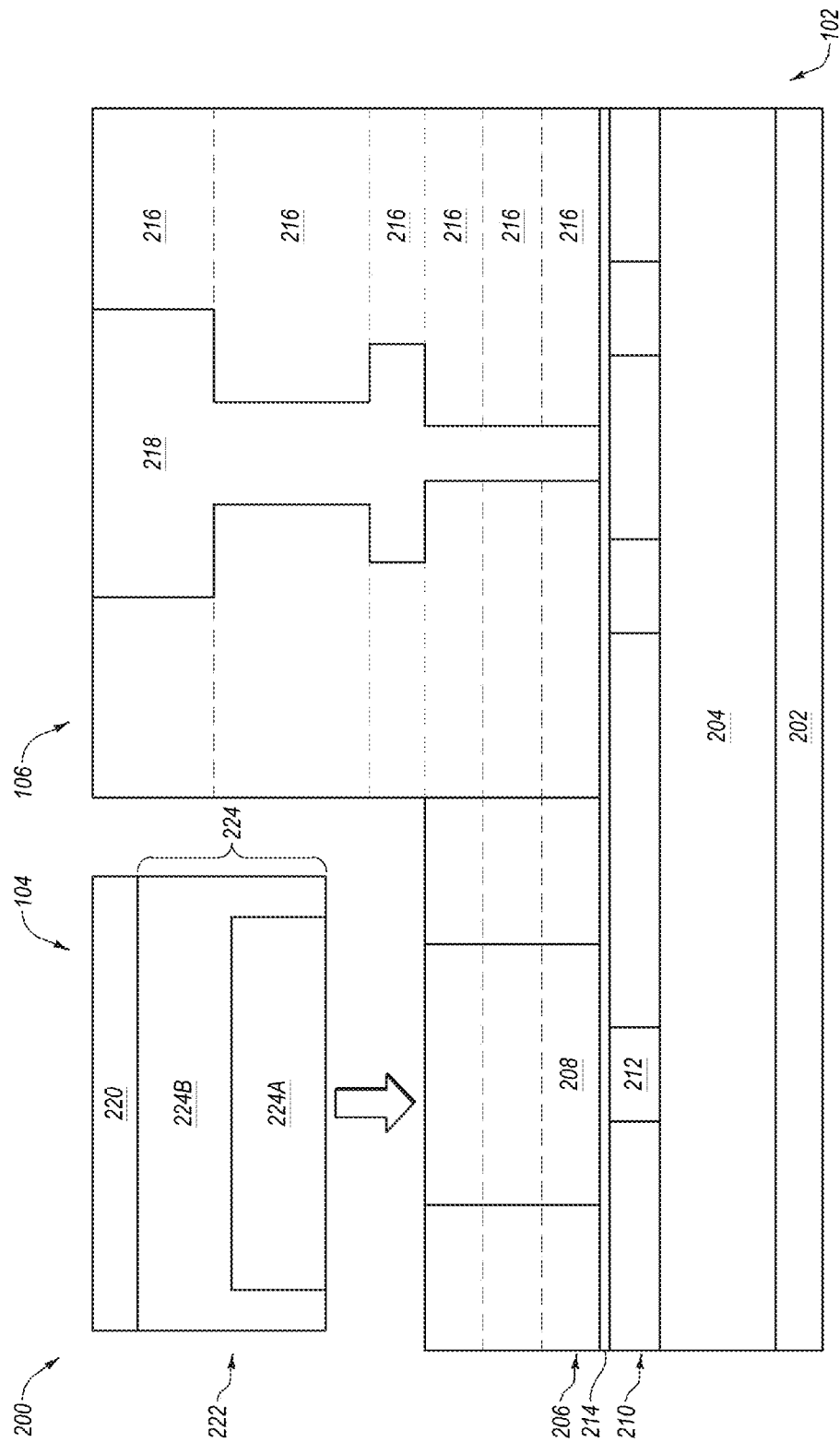


FIG. 1



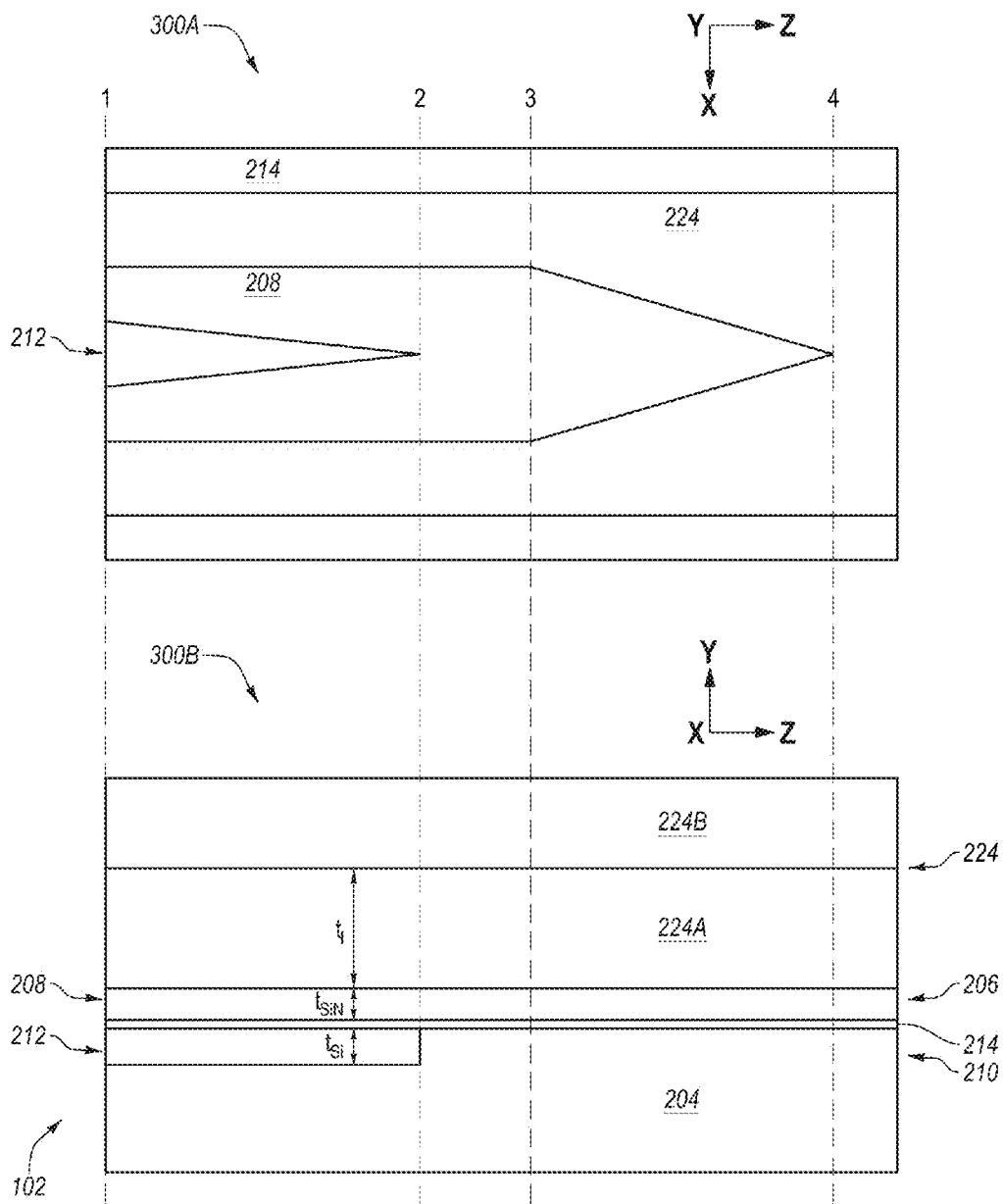


FIG. 3A

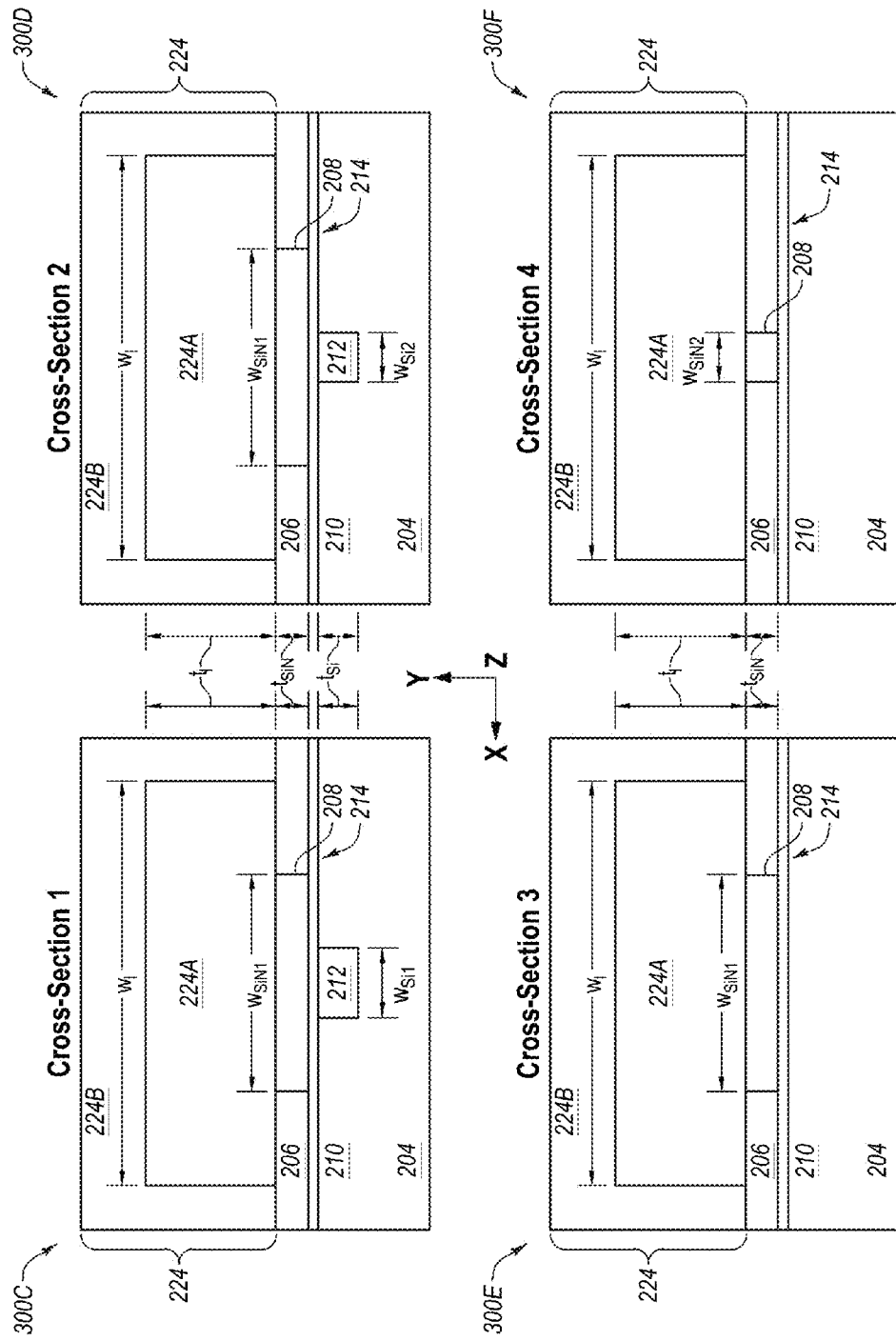
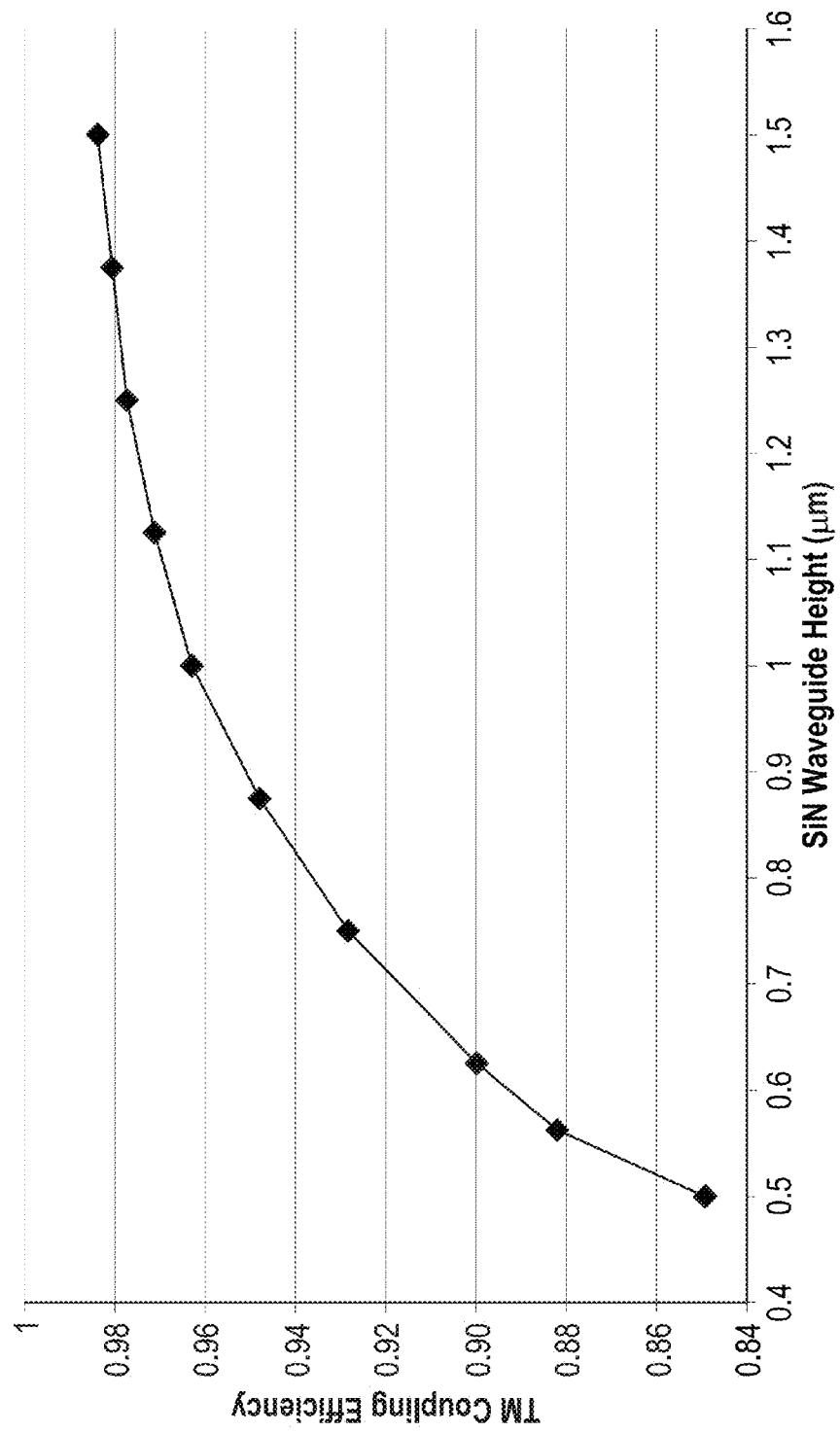
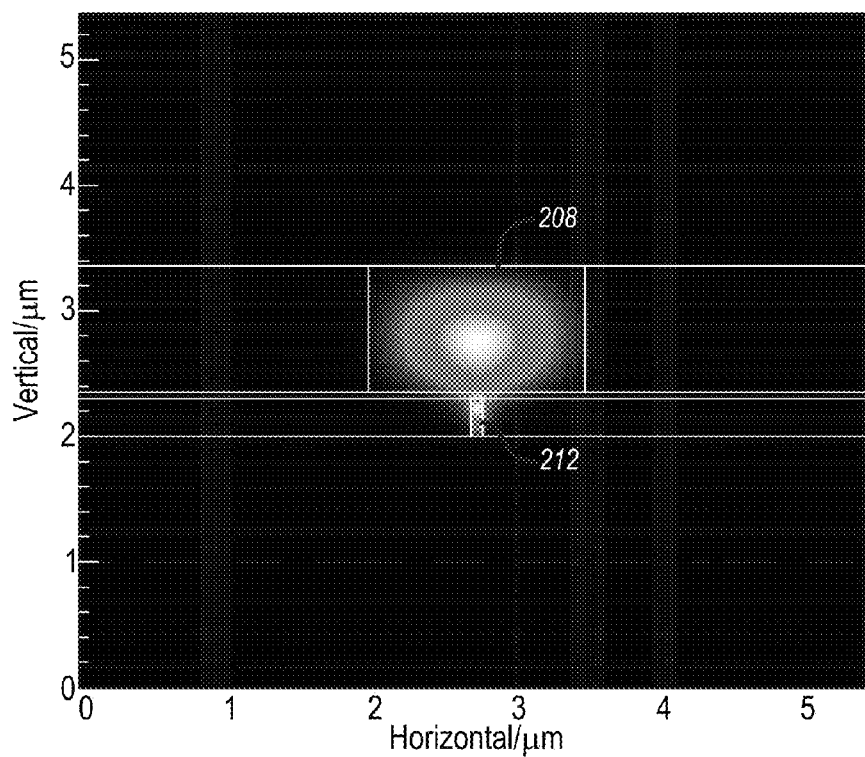
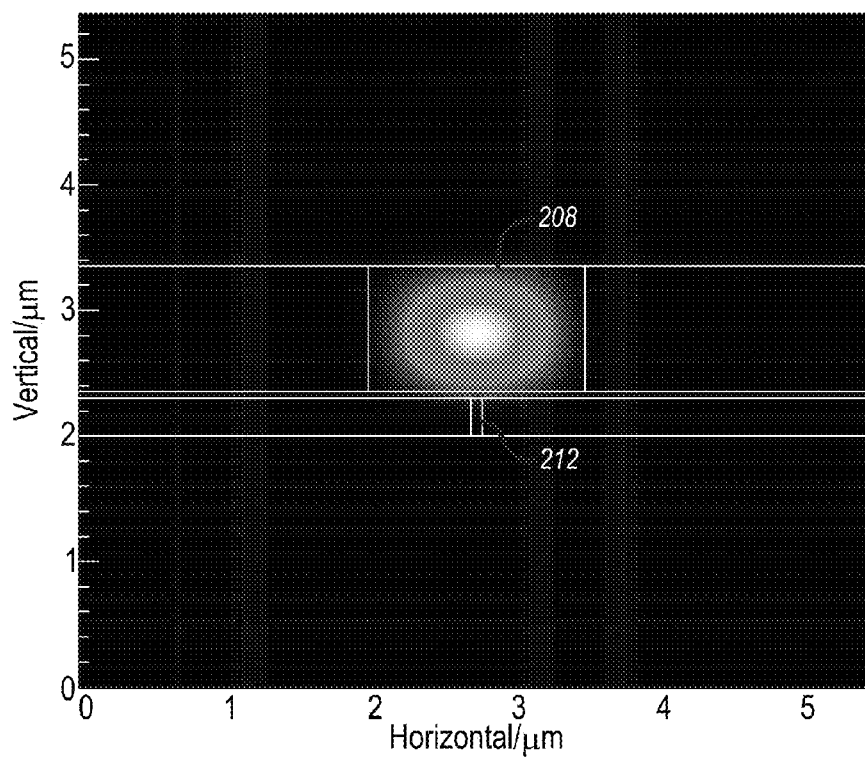


FIG. 3B

**FIG. 4**

**FIG. 5A****FIG. 5B**



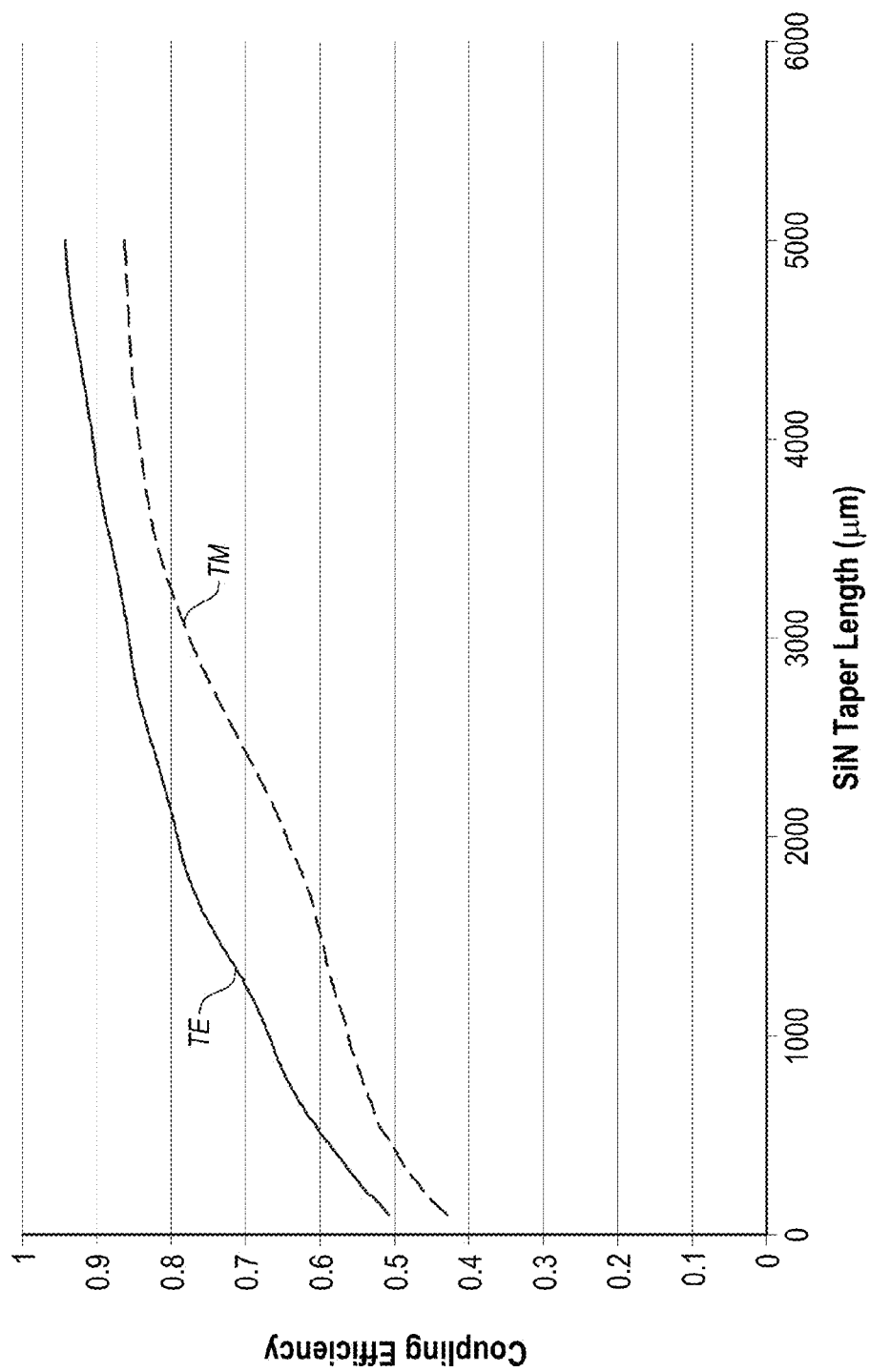
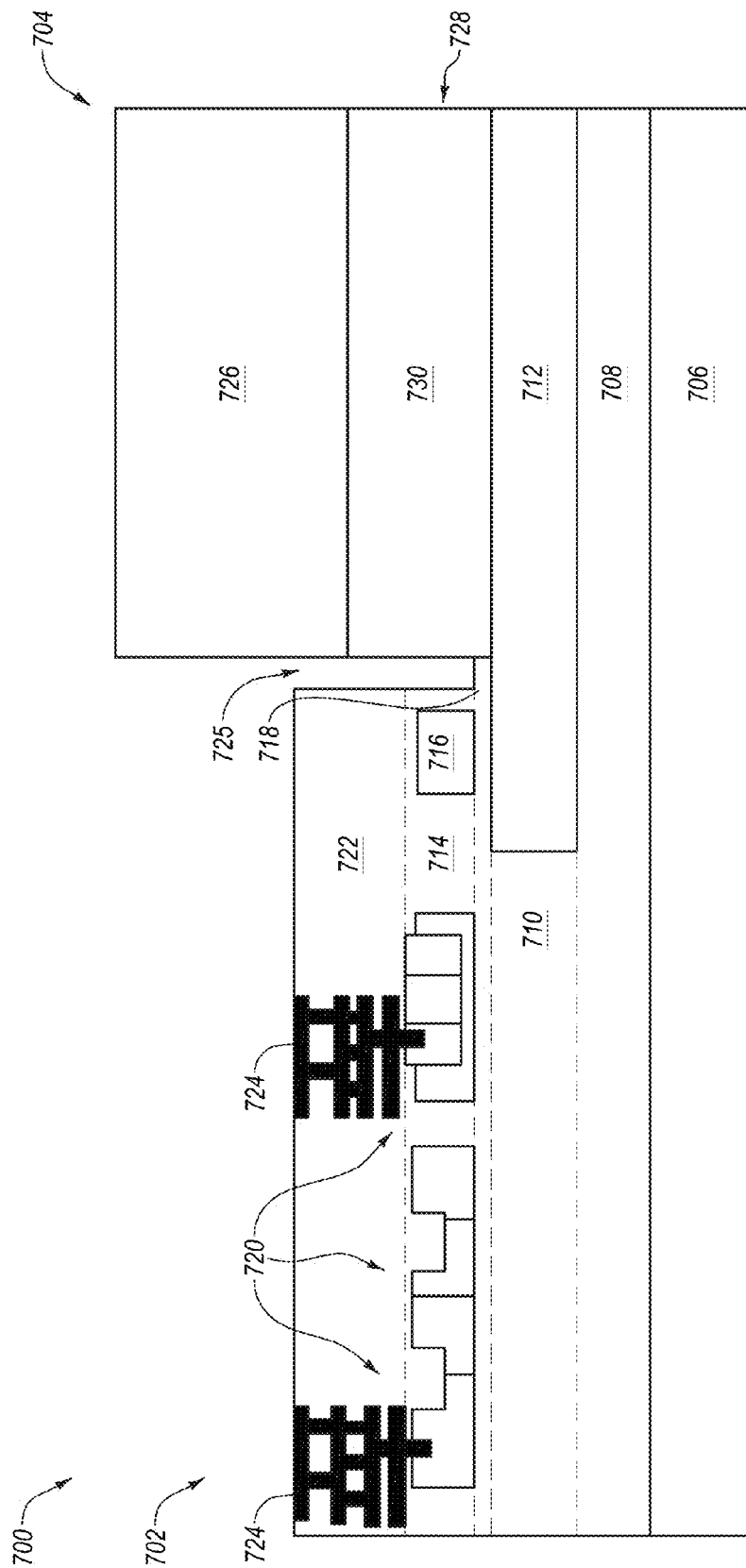


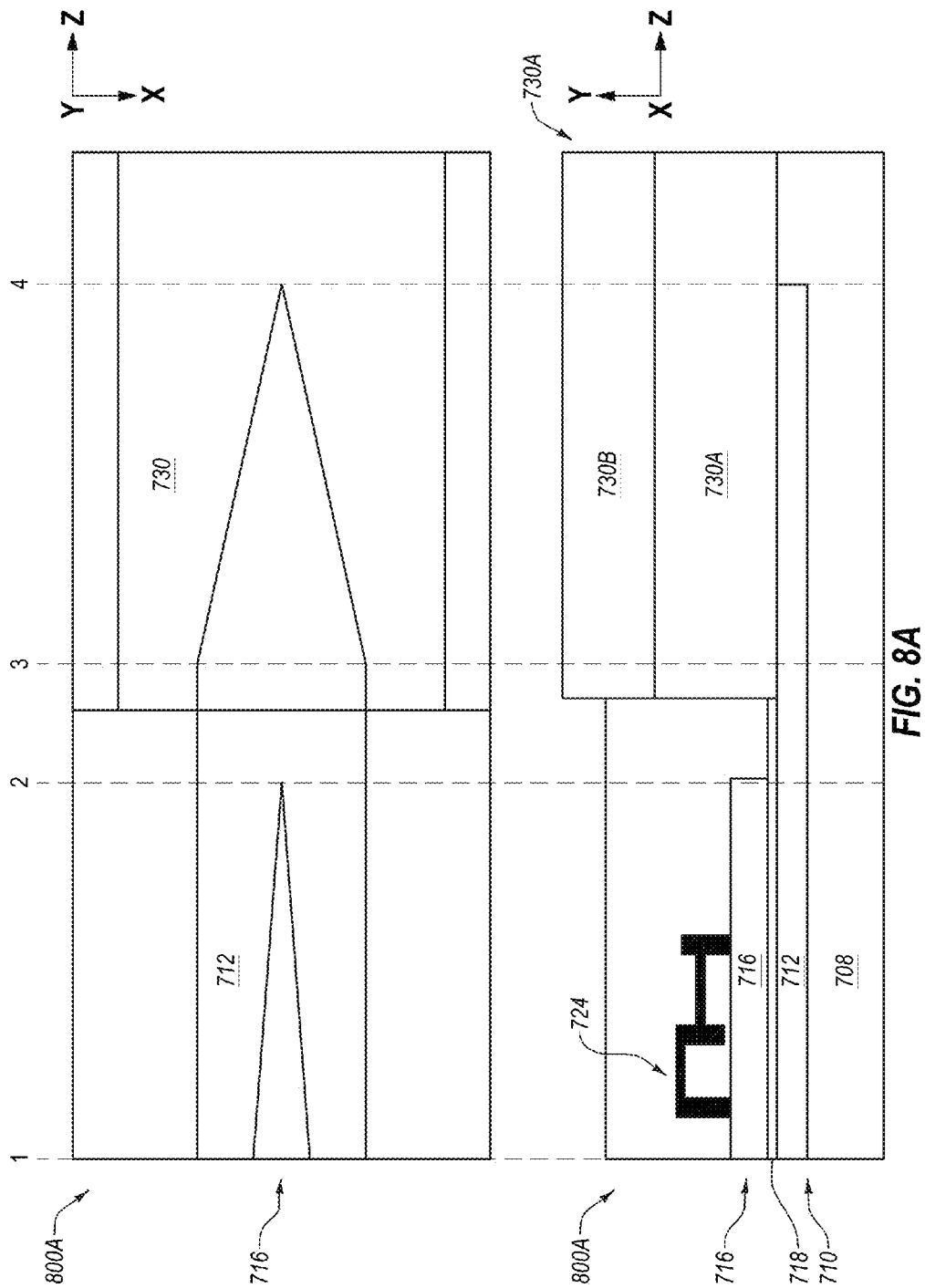
FIG. 6



Passives

Actives

FIG. 7



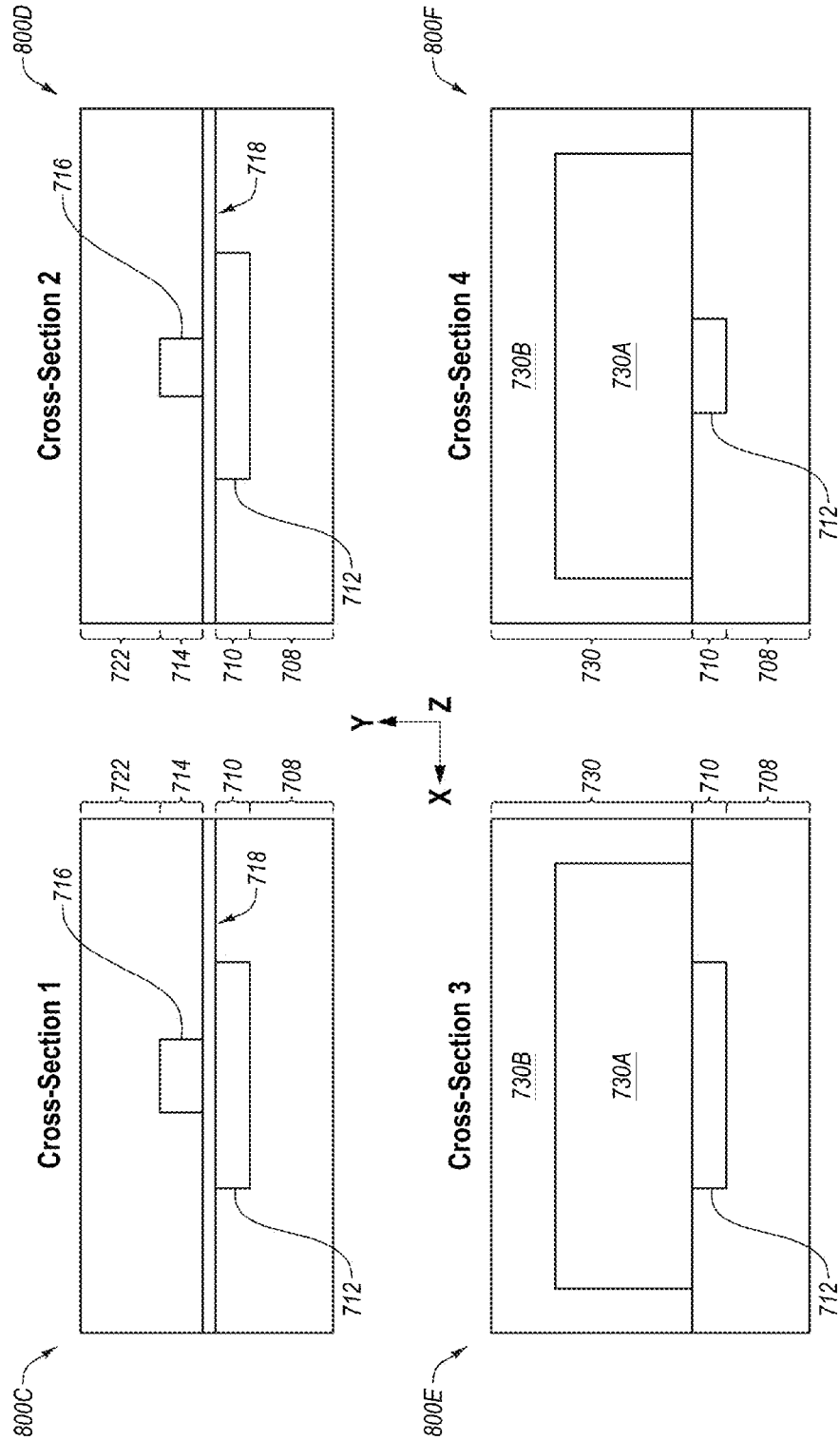


FIG. 8B

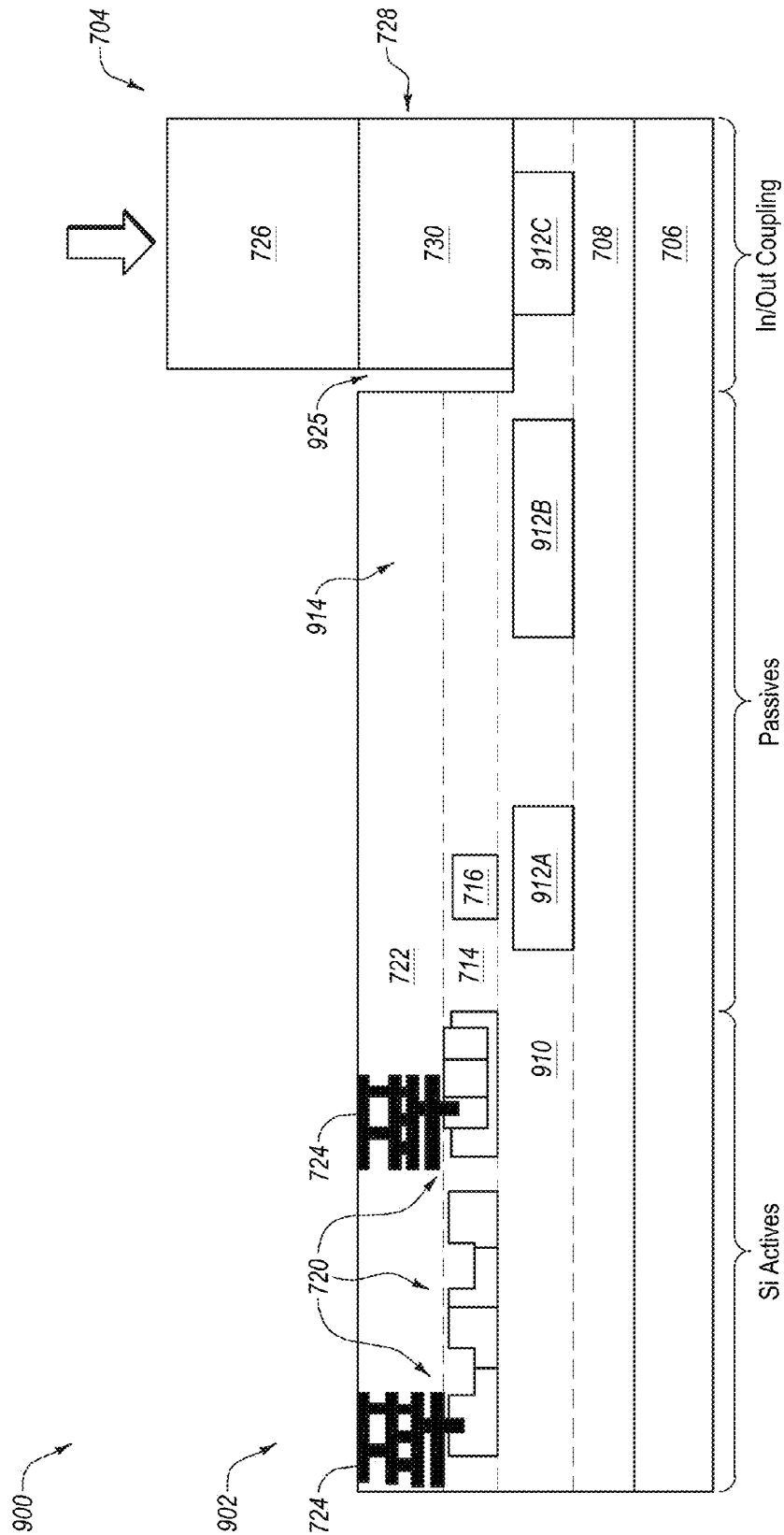


FIG. 9

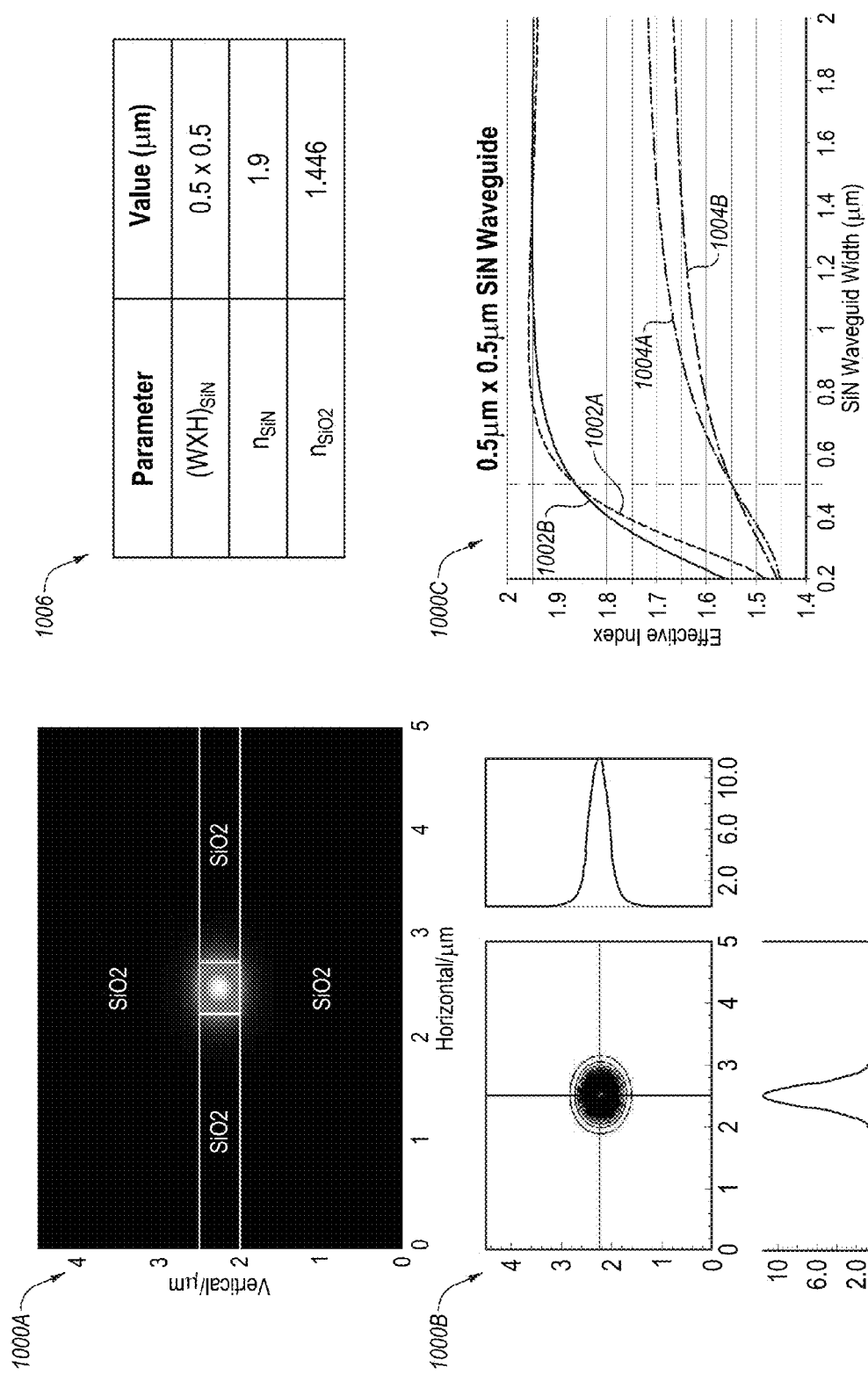


FIG. 10

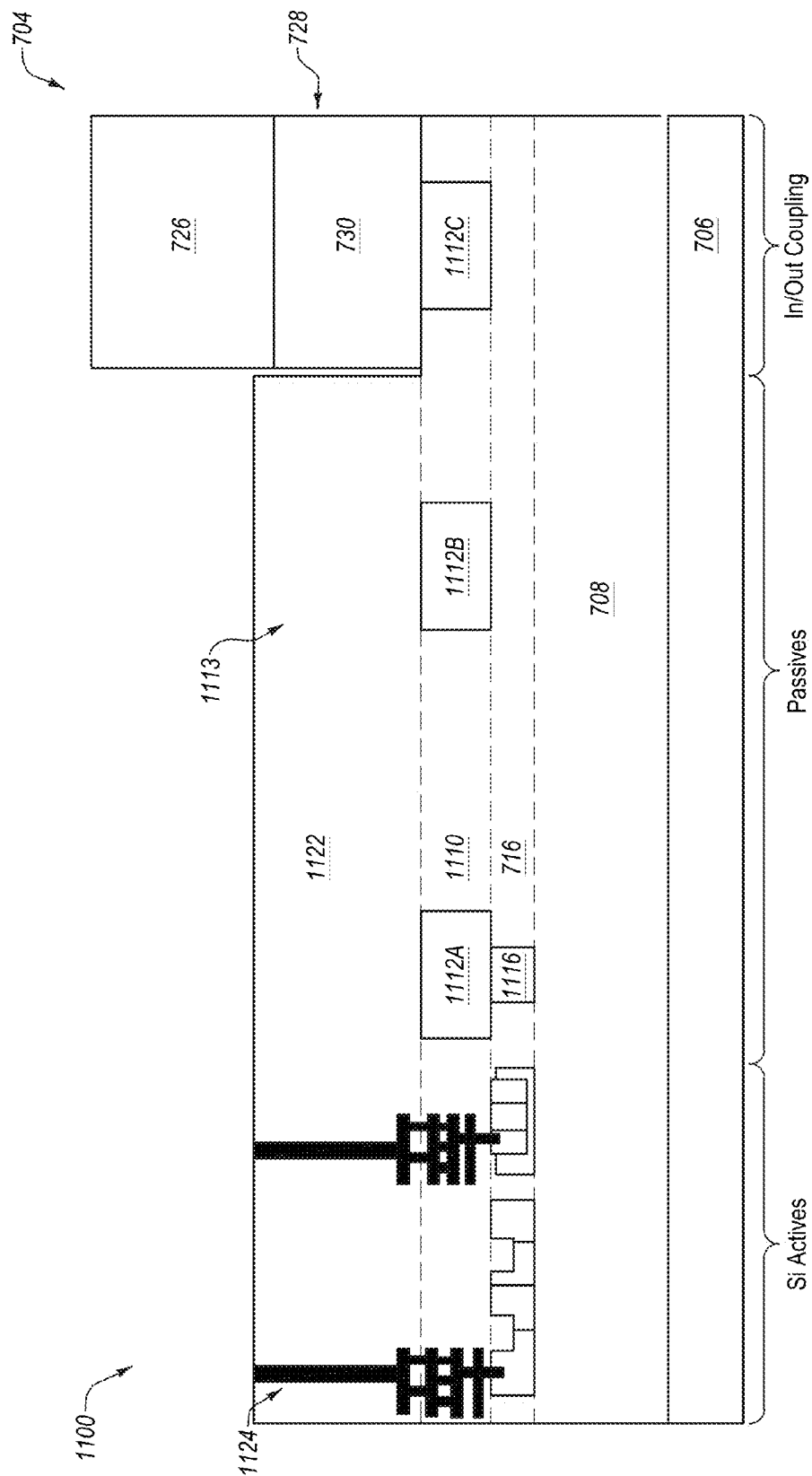


FIG. 11

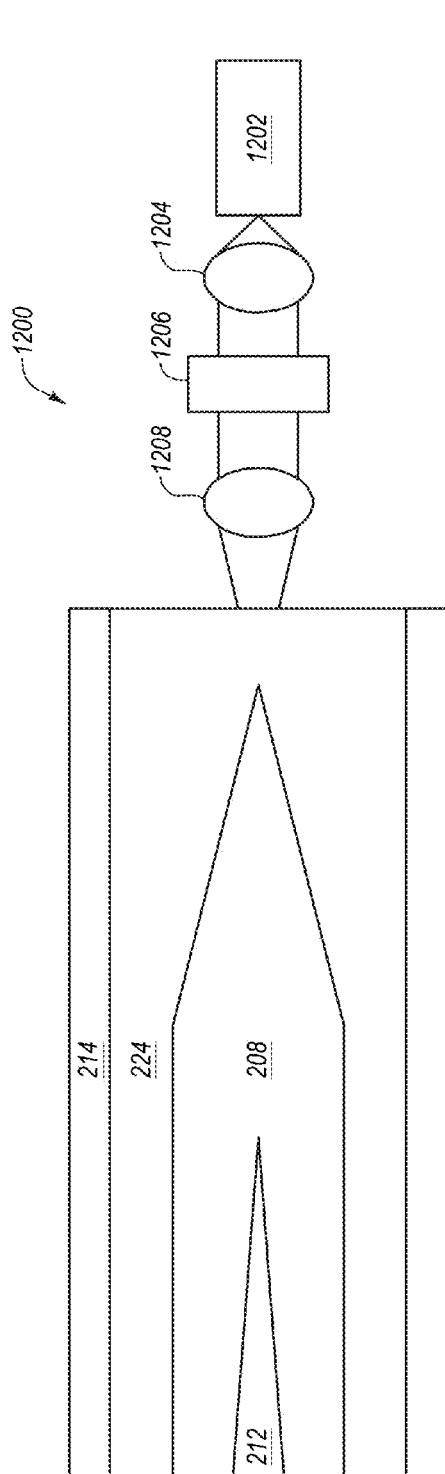


FIG. 12A

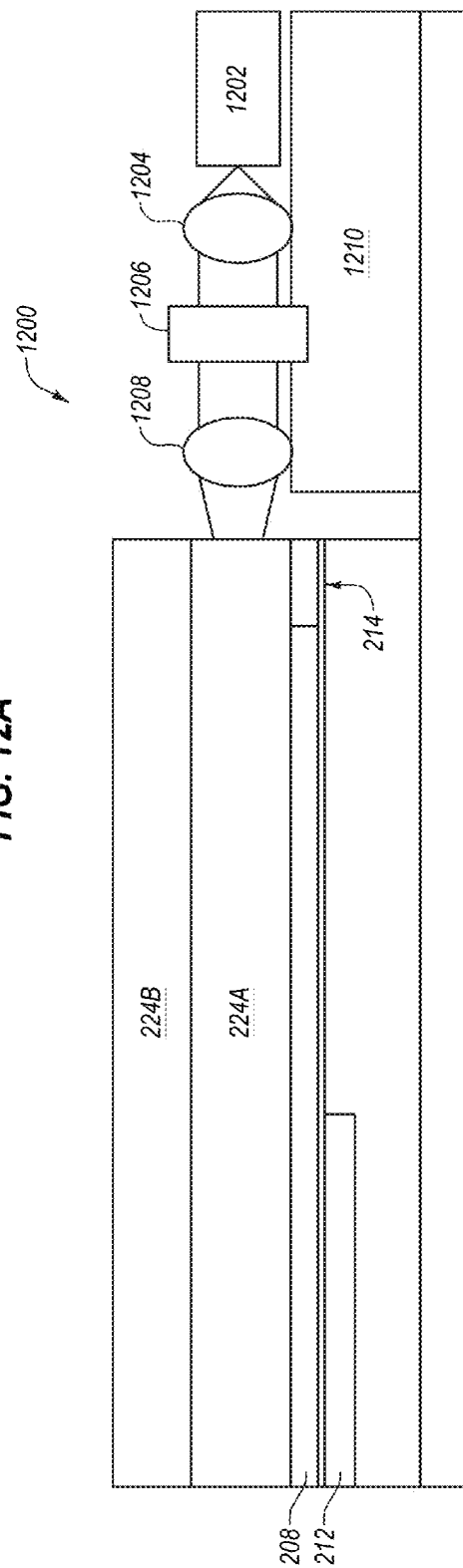


FIG. 12B



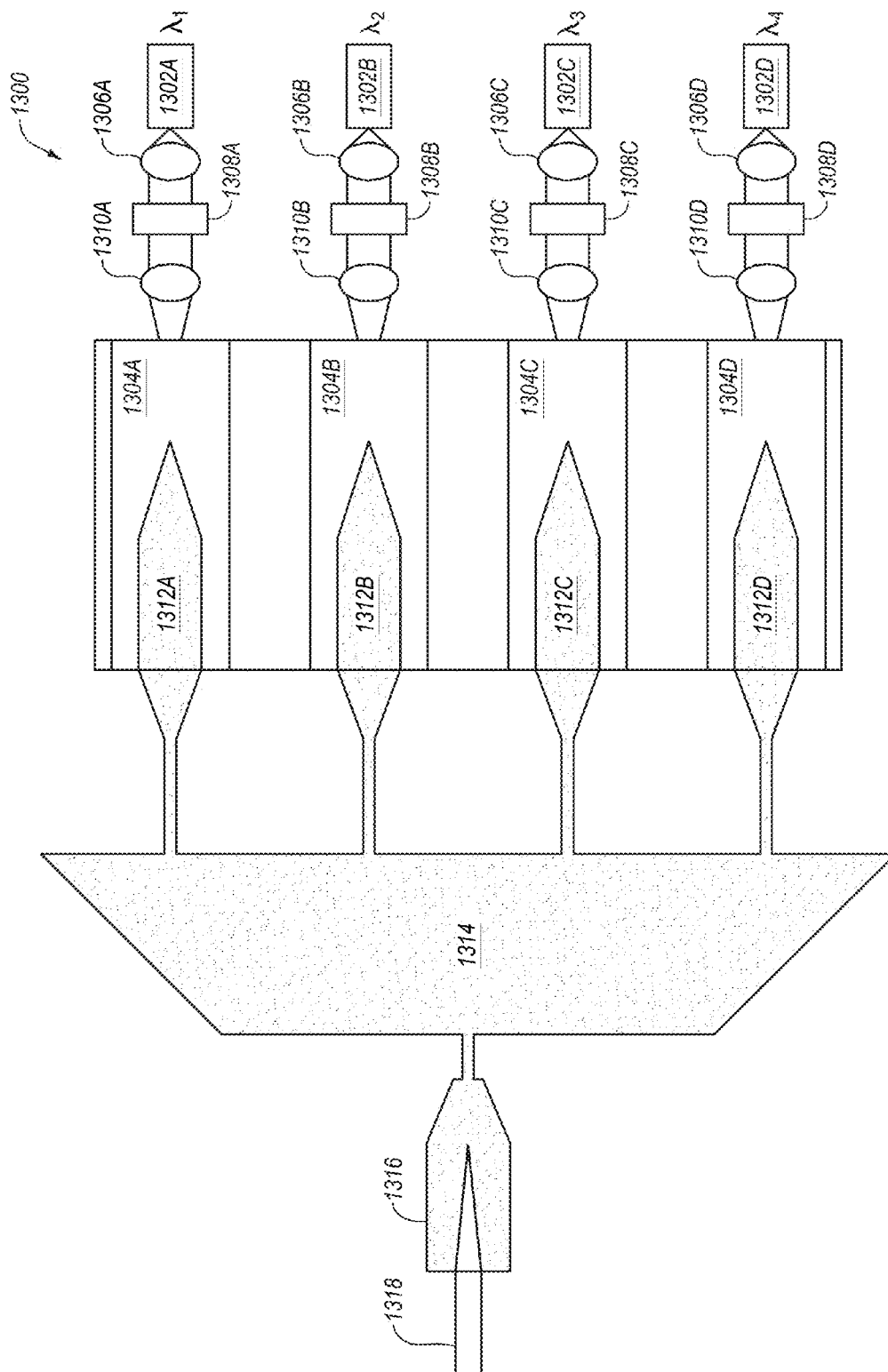


FIG. 13

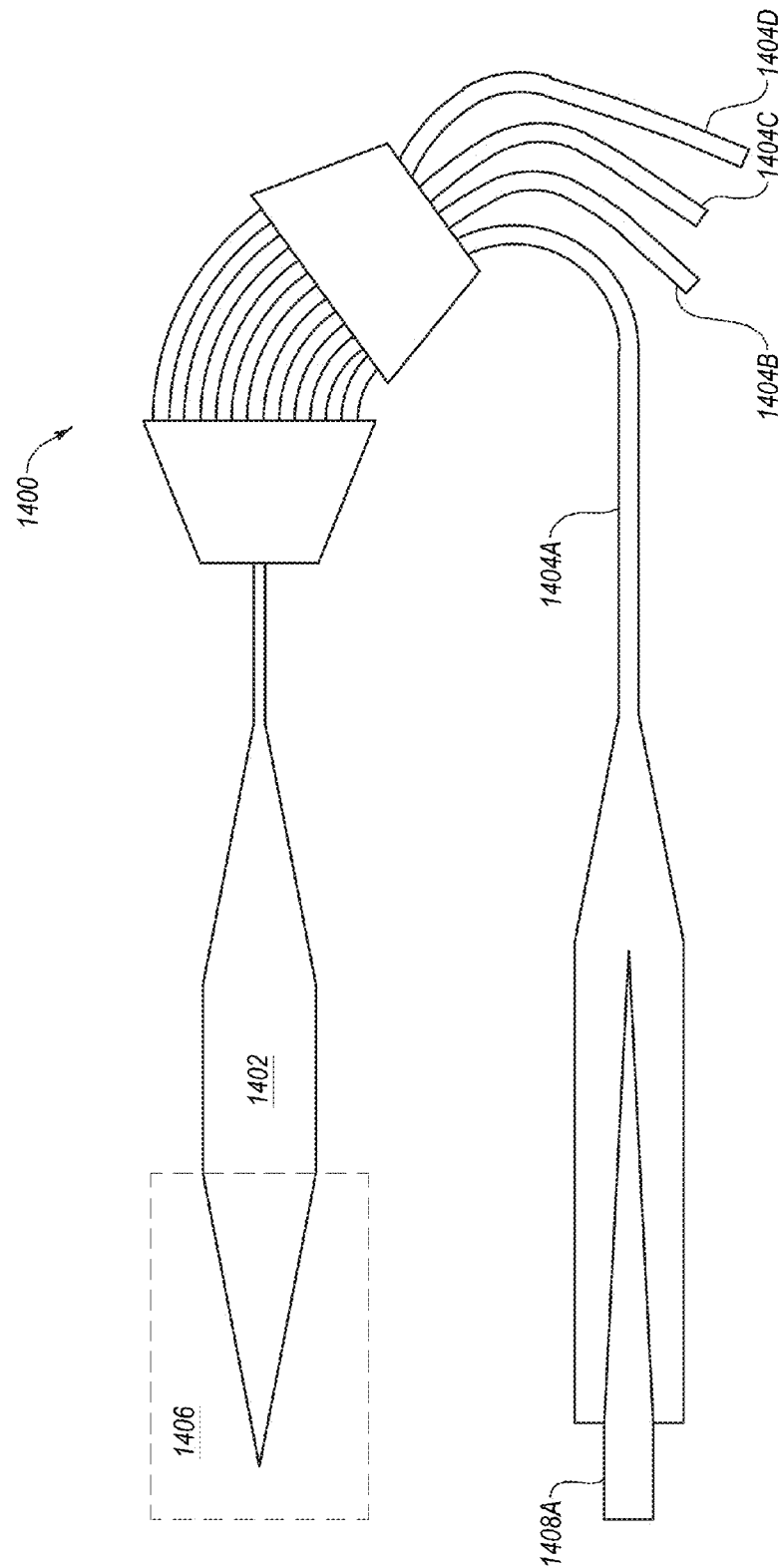


FIG. 14

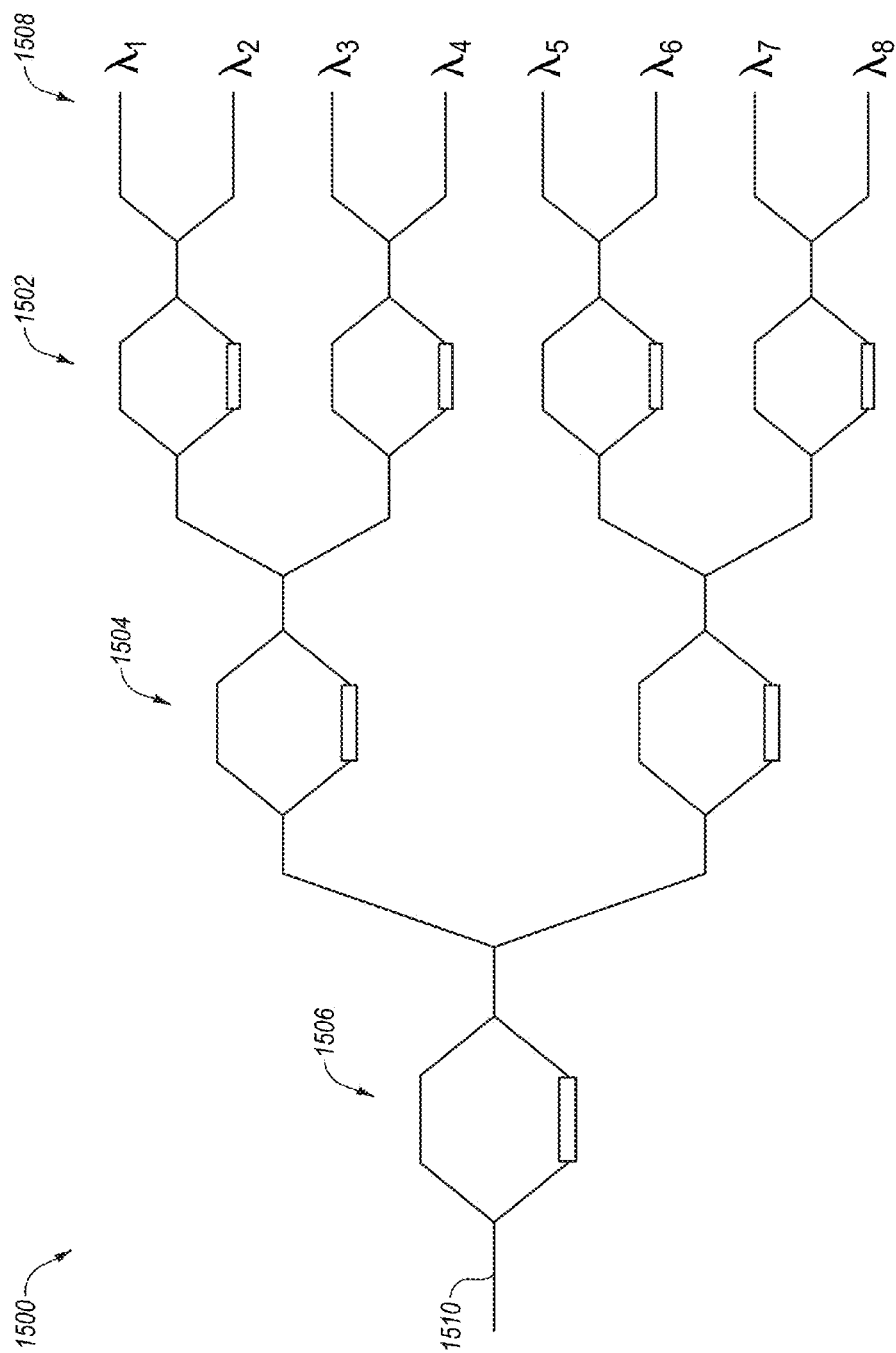
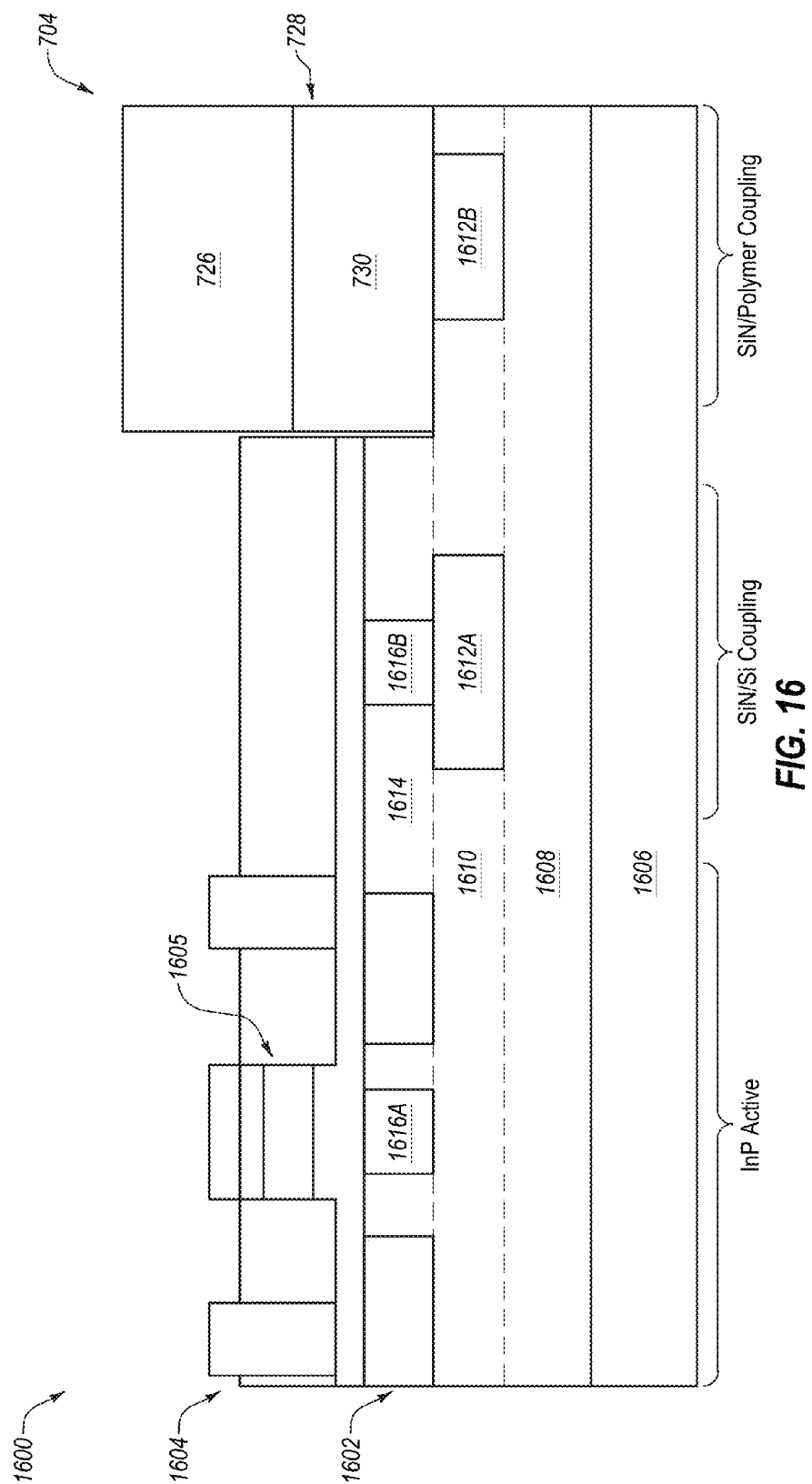


FIG. 15



**FIG. 16**

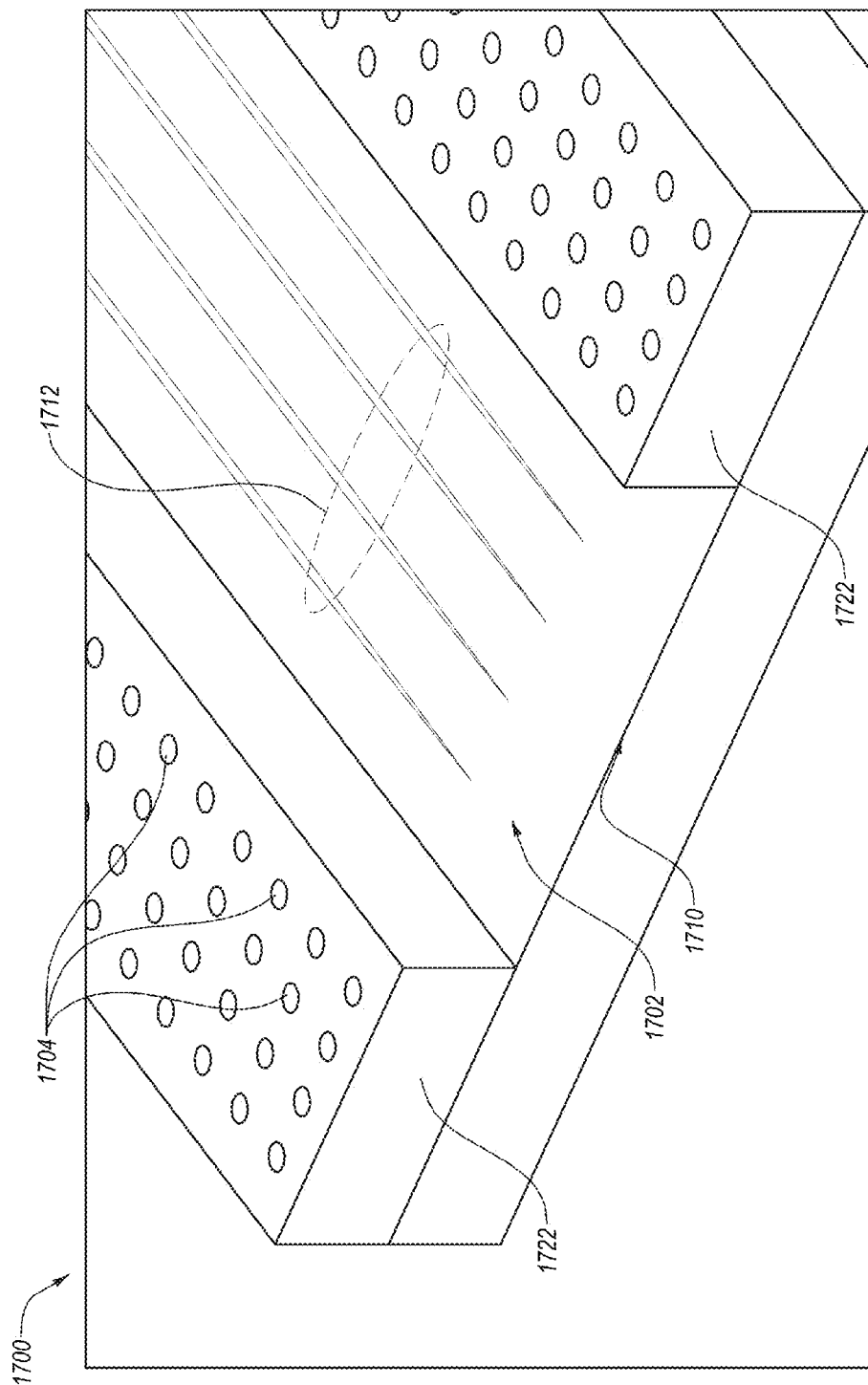
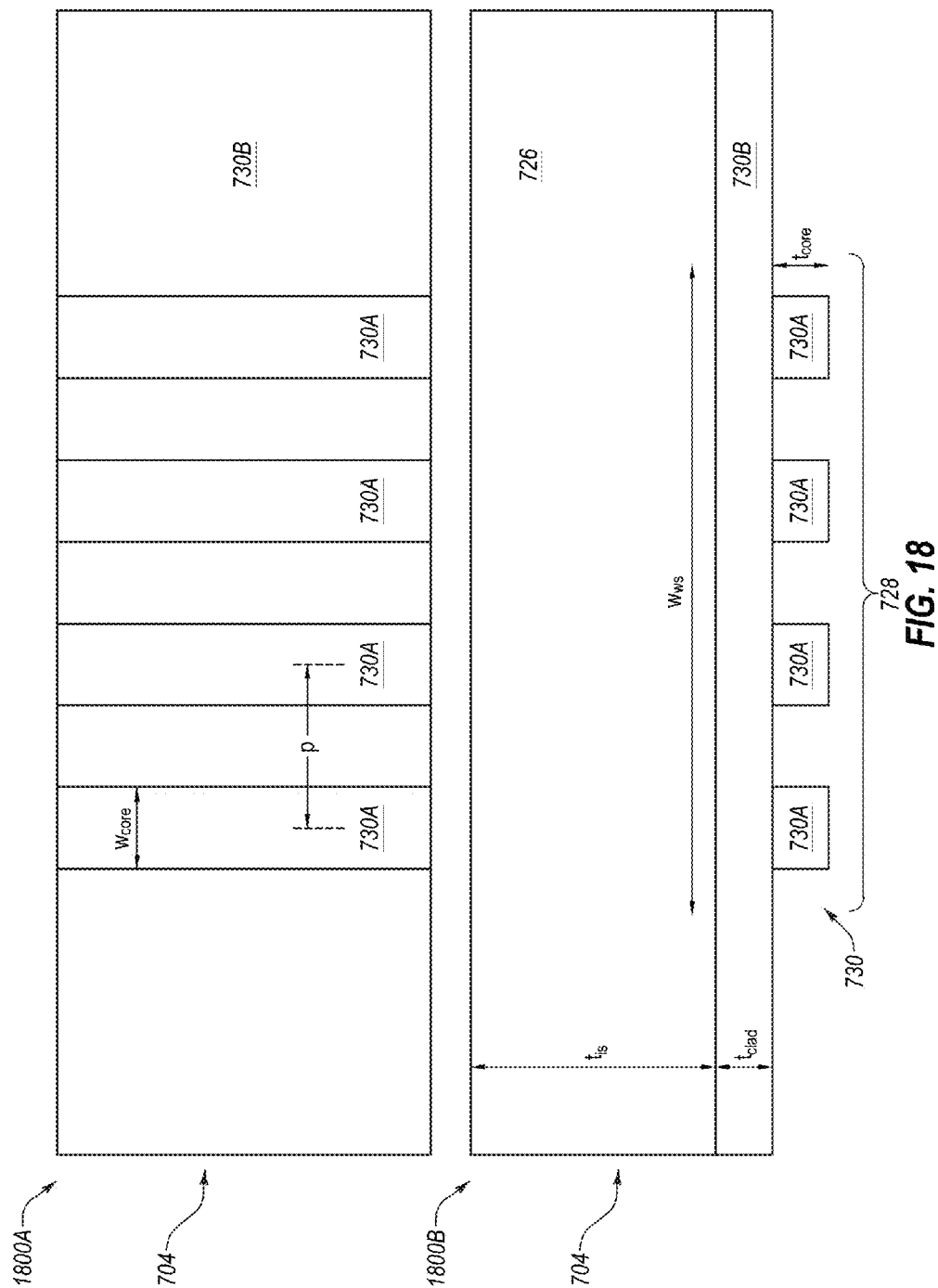


FIG. 17



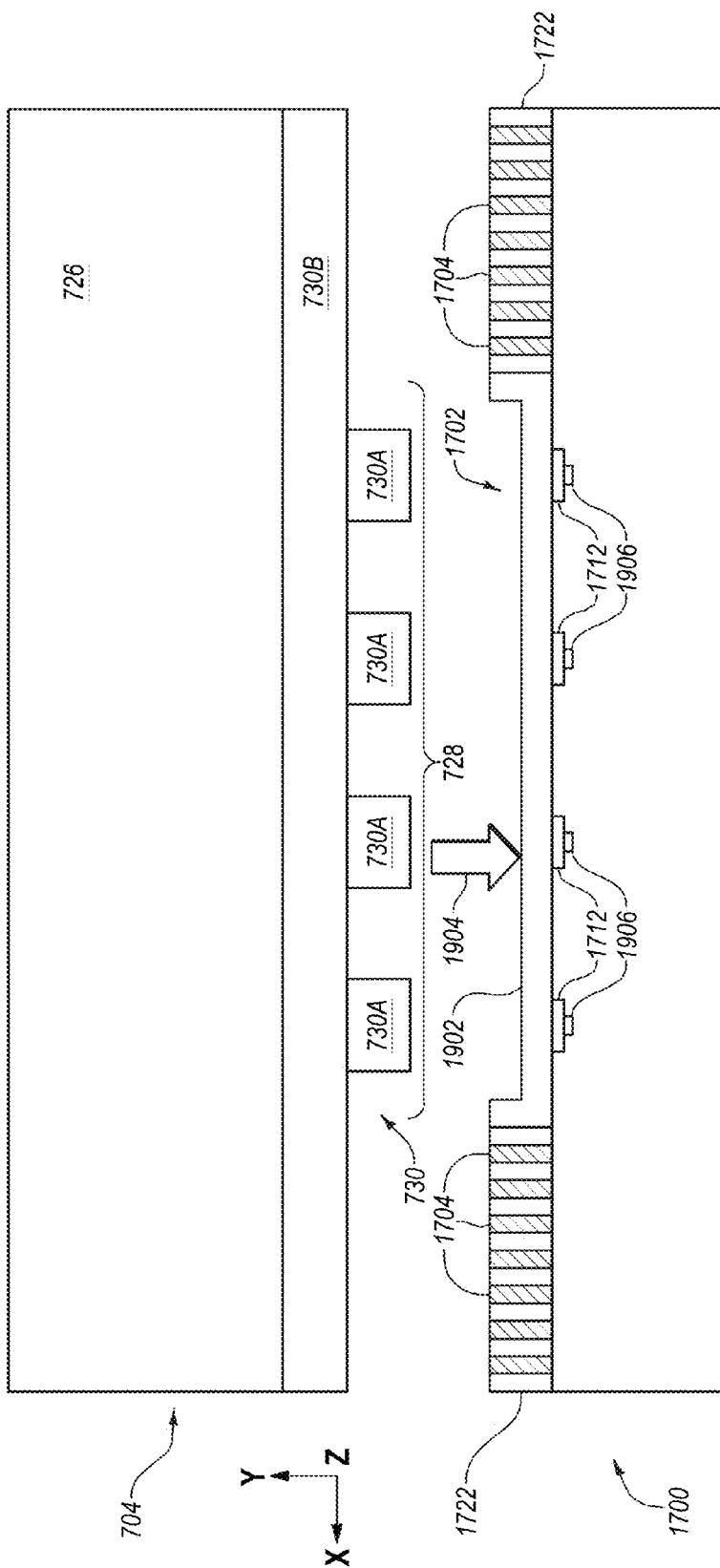


FIG. 19A

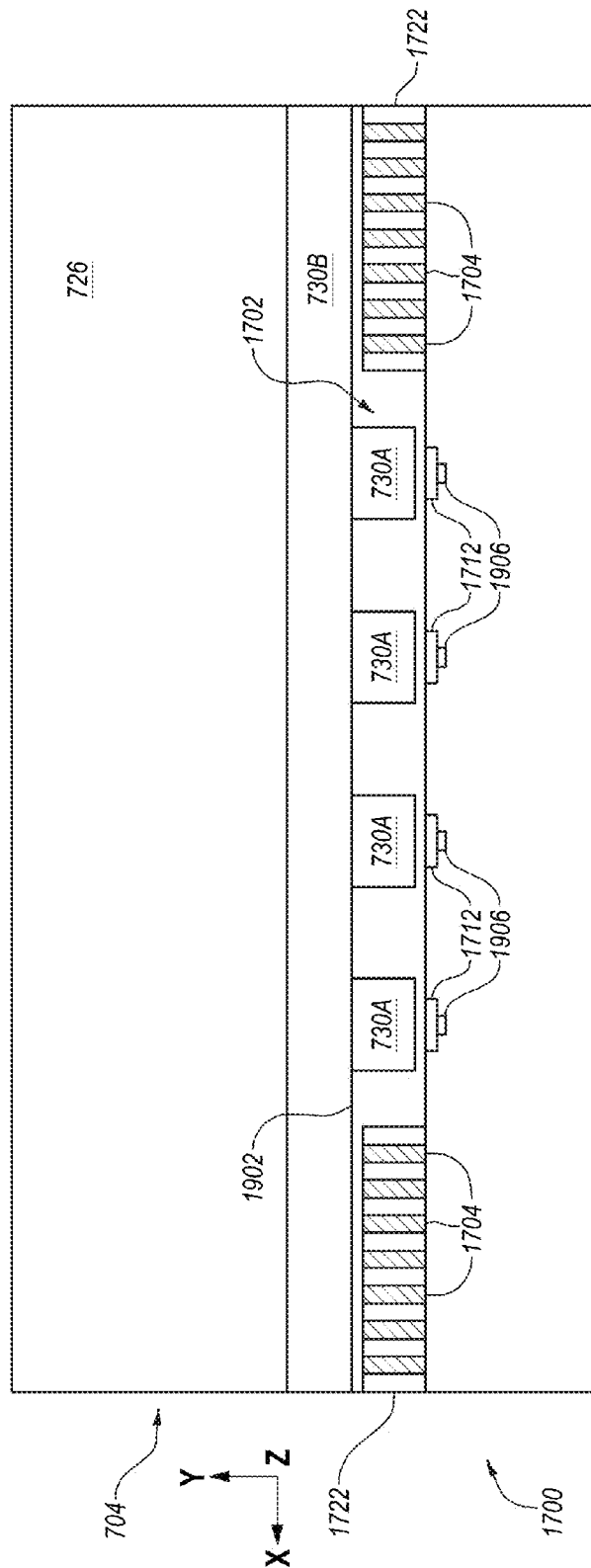


FIG. 19B



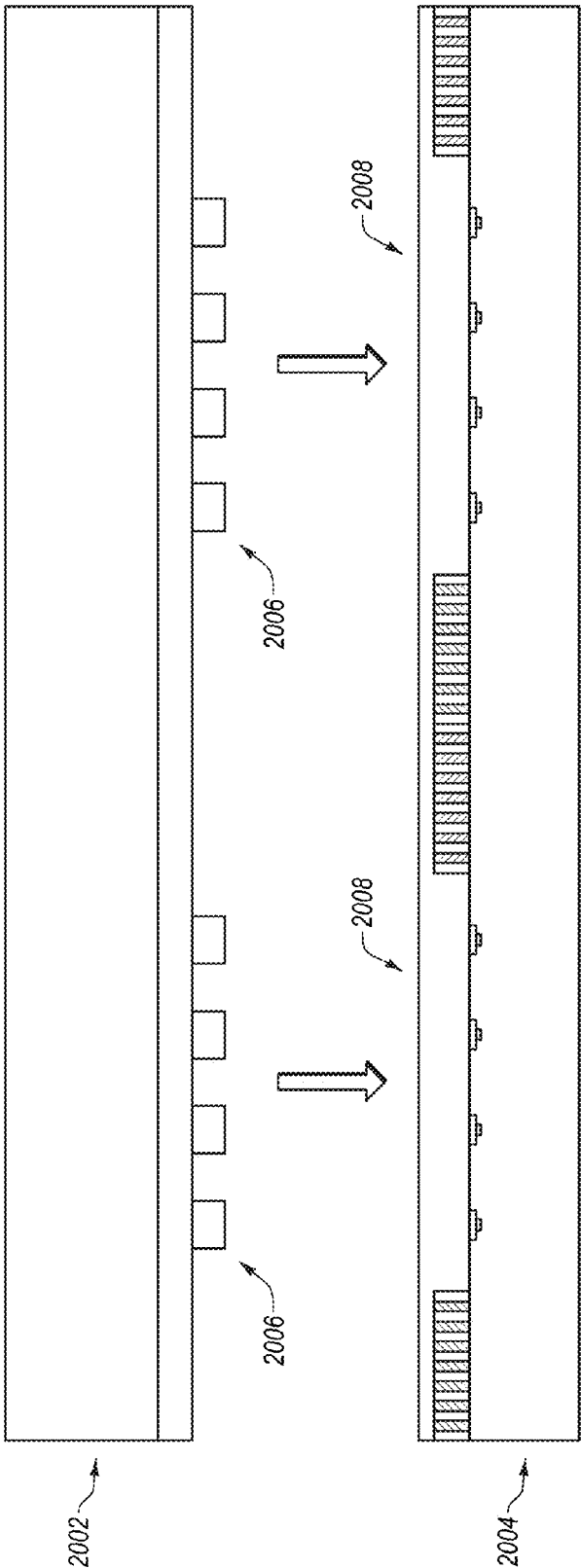
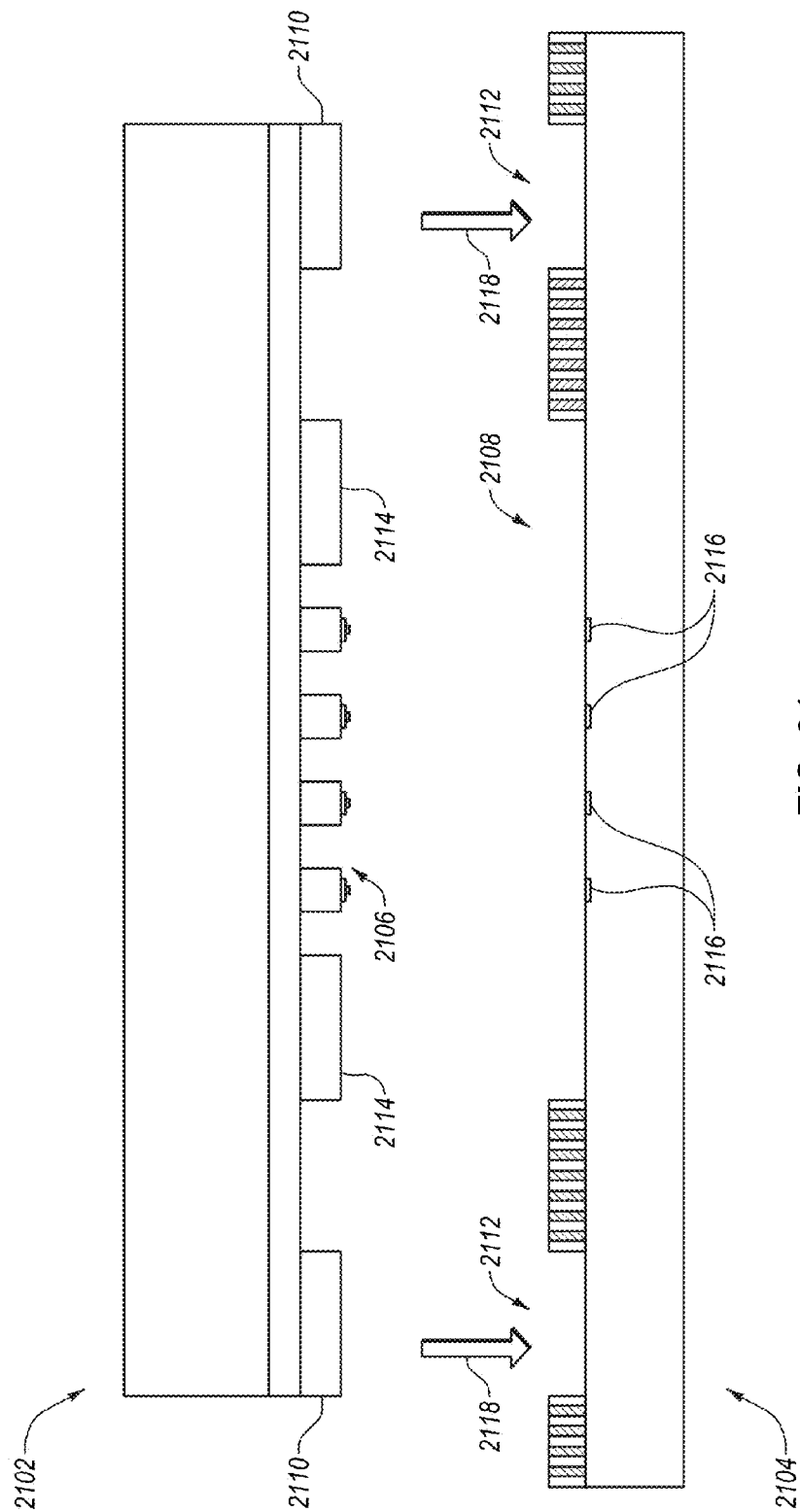


FIG. 20



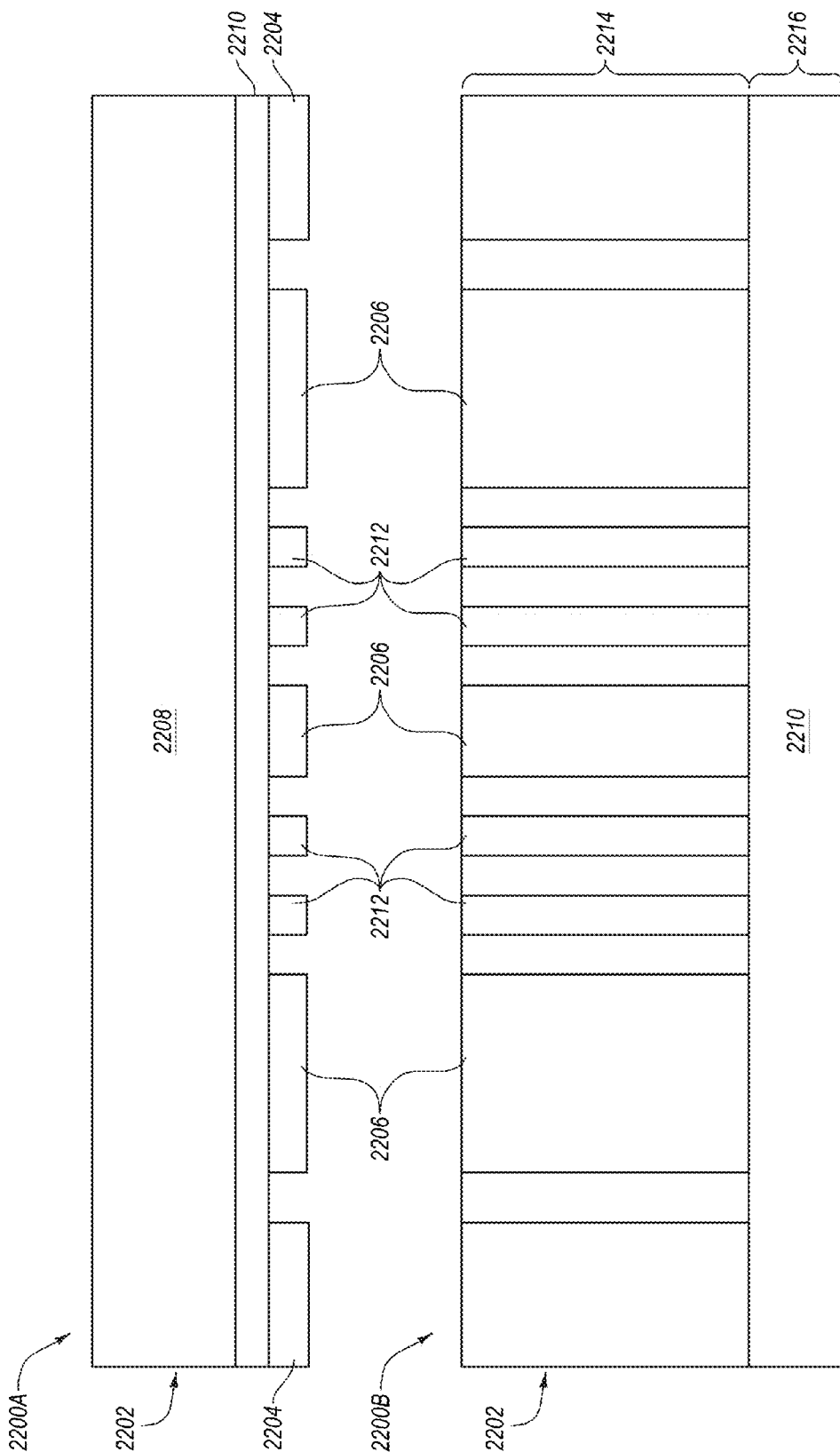


FIG. 22

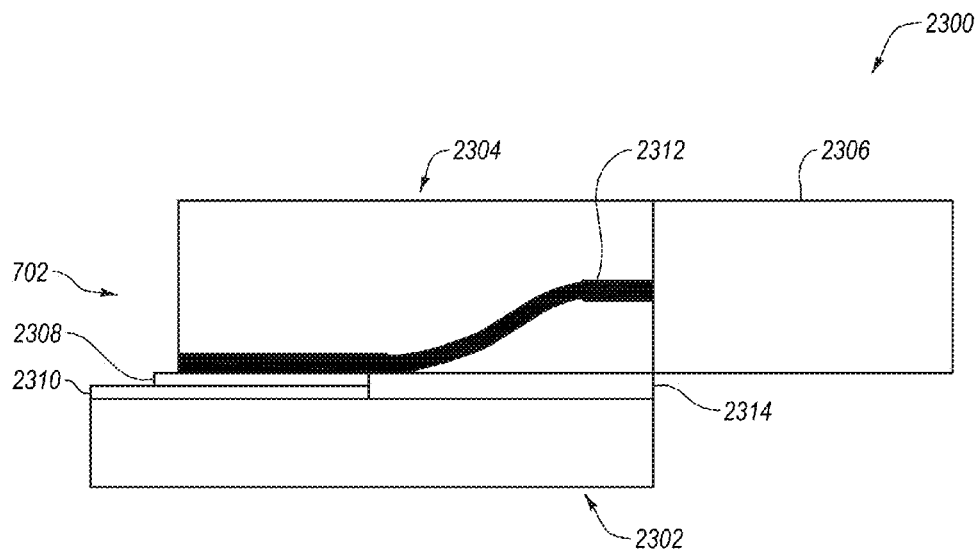


FIG. 23A

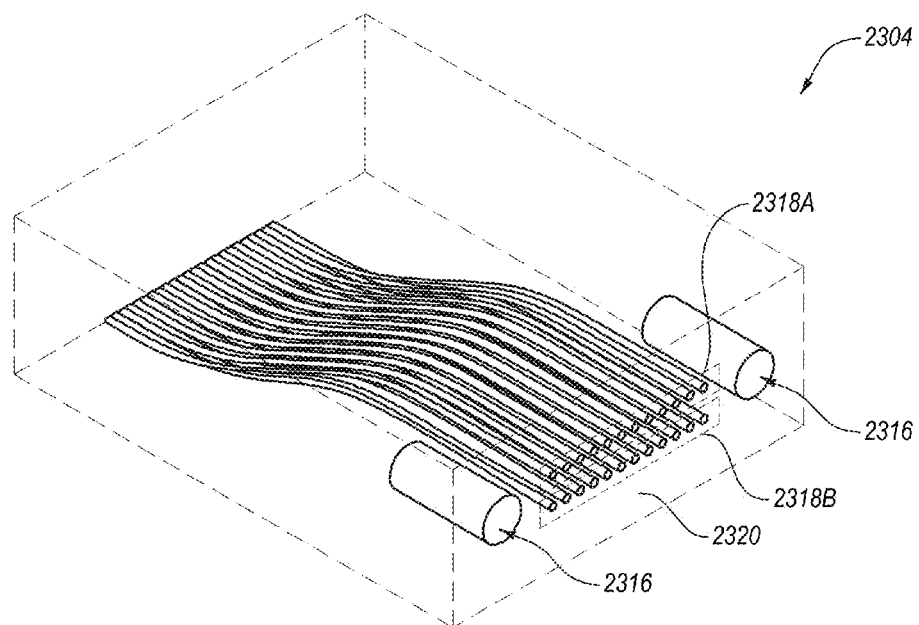
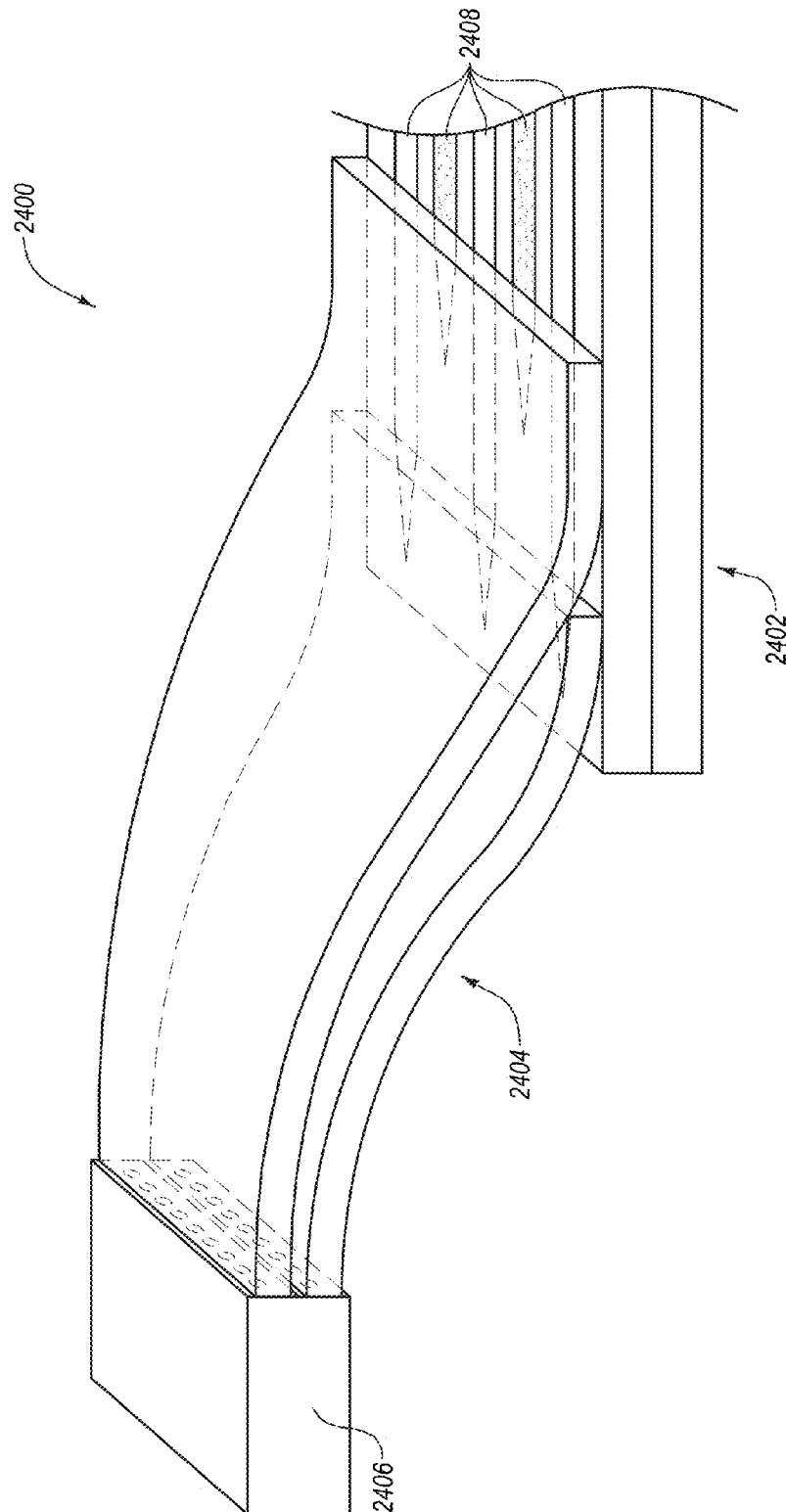


FIG. 23B



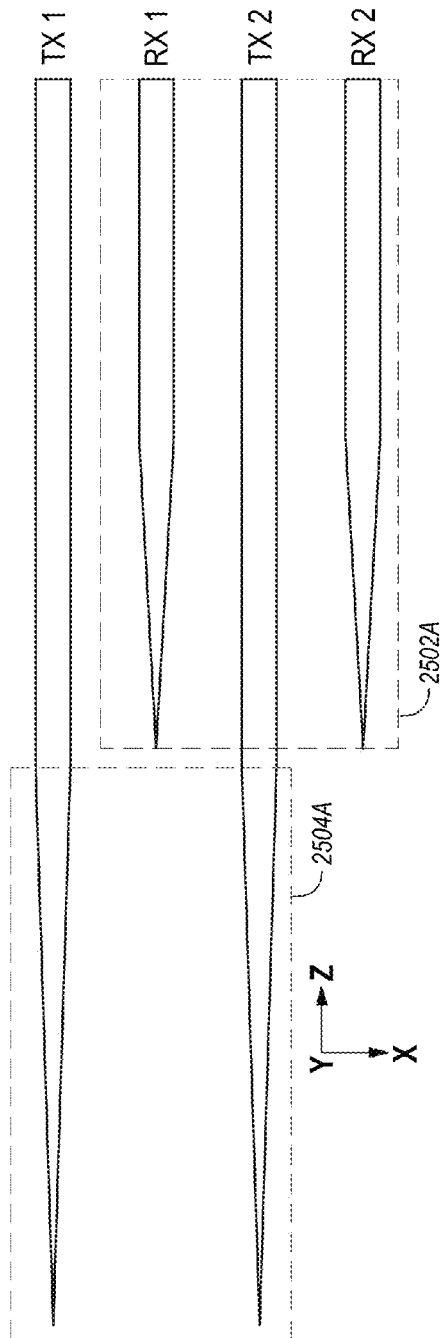


FIG. 25A

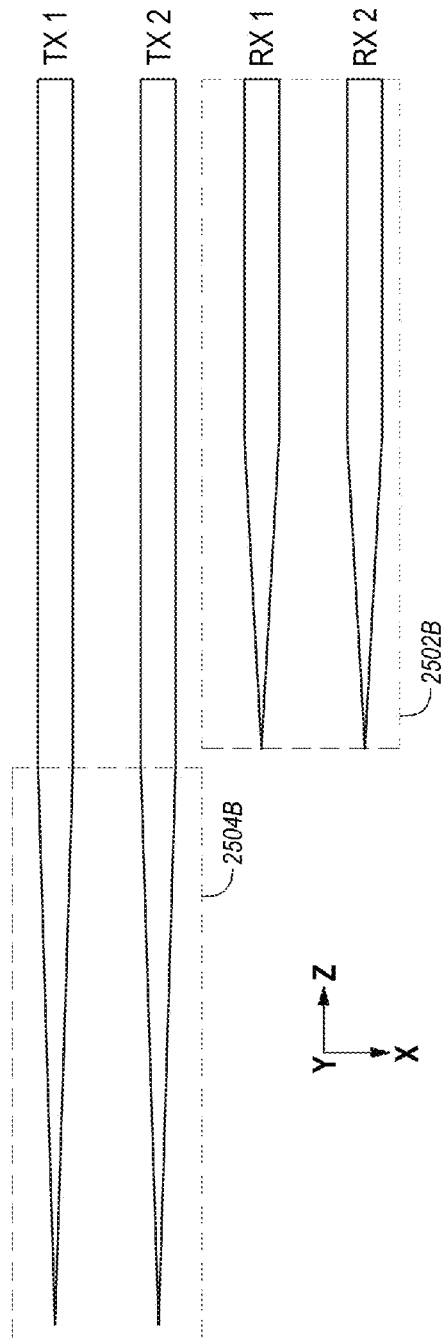


FIG. 25B

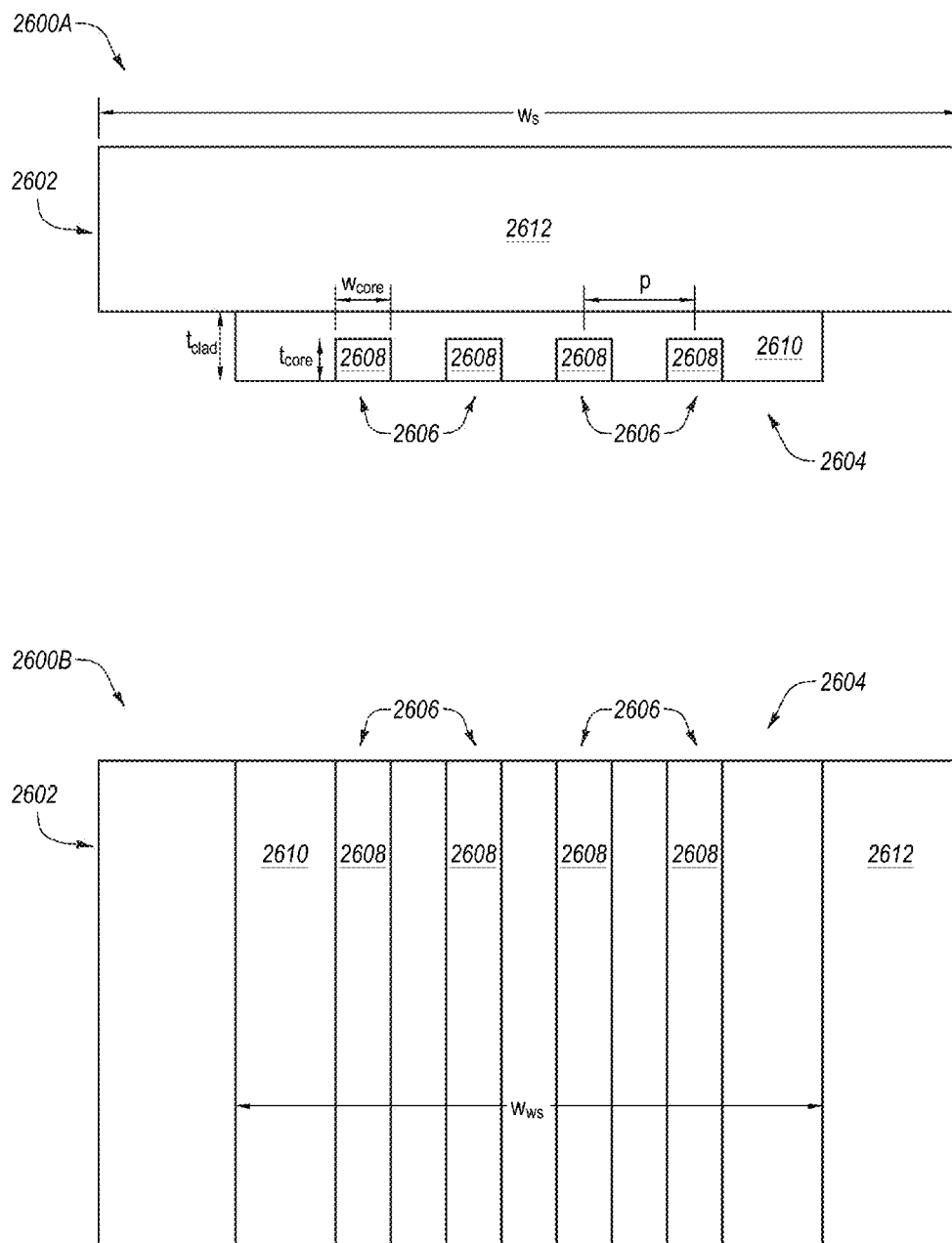


FIG. 26

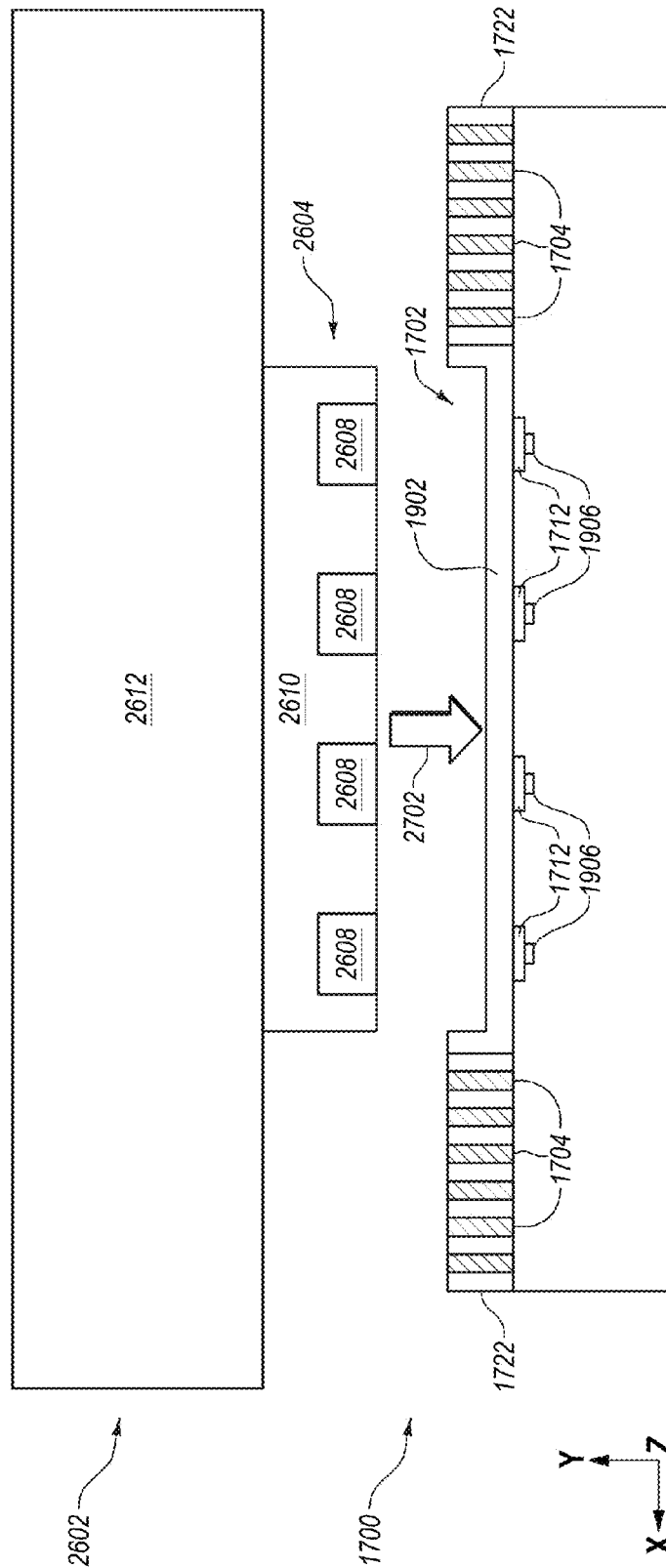


FIG. 27



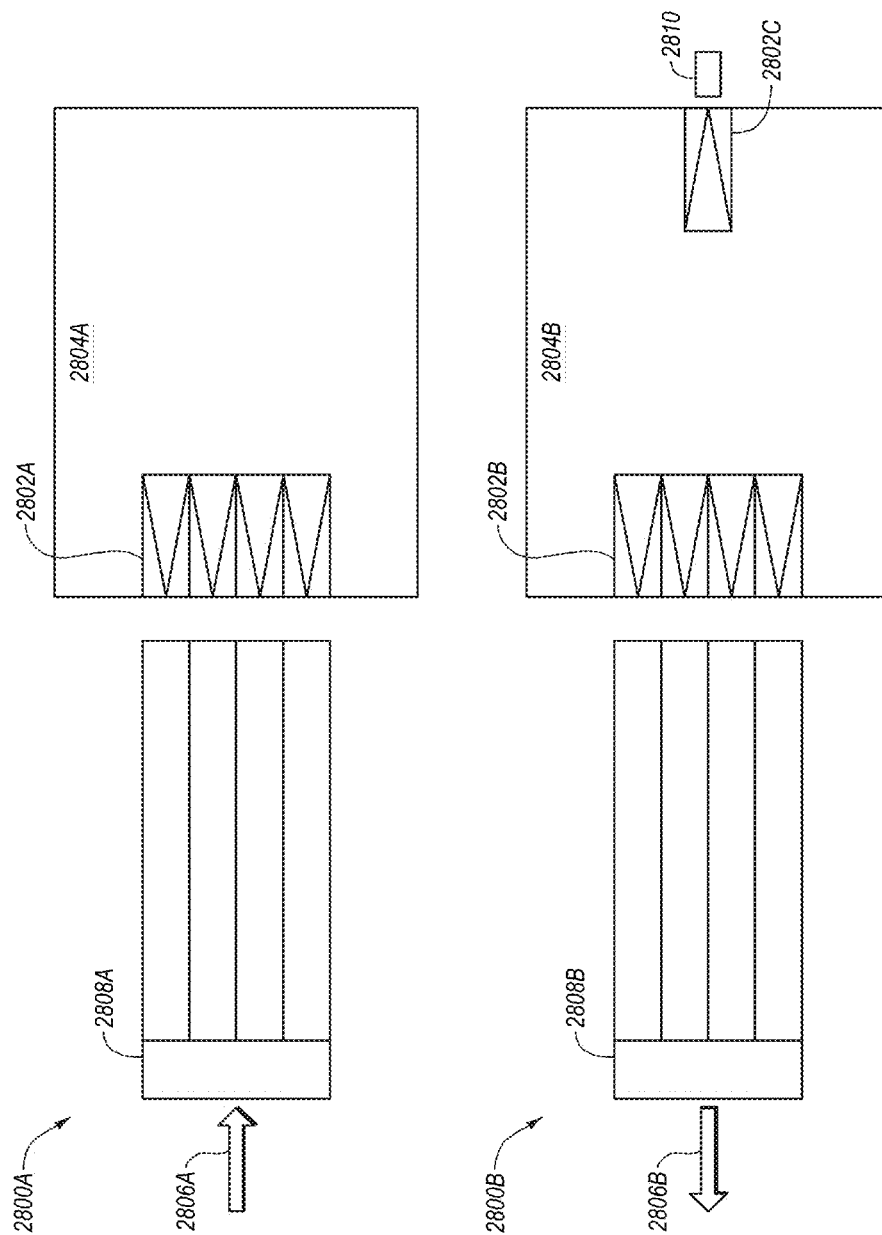


FIG. 28

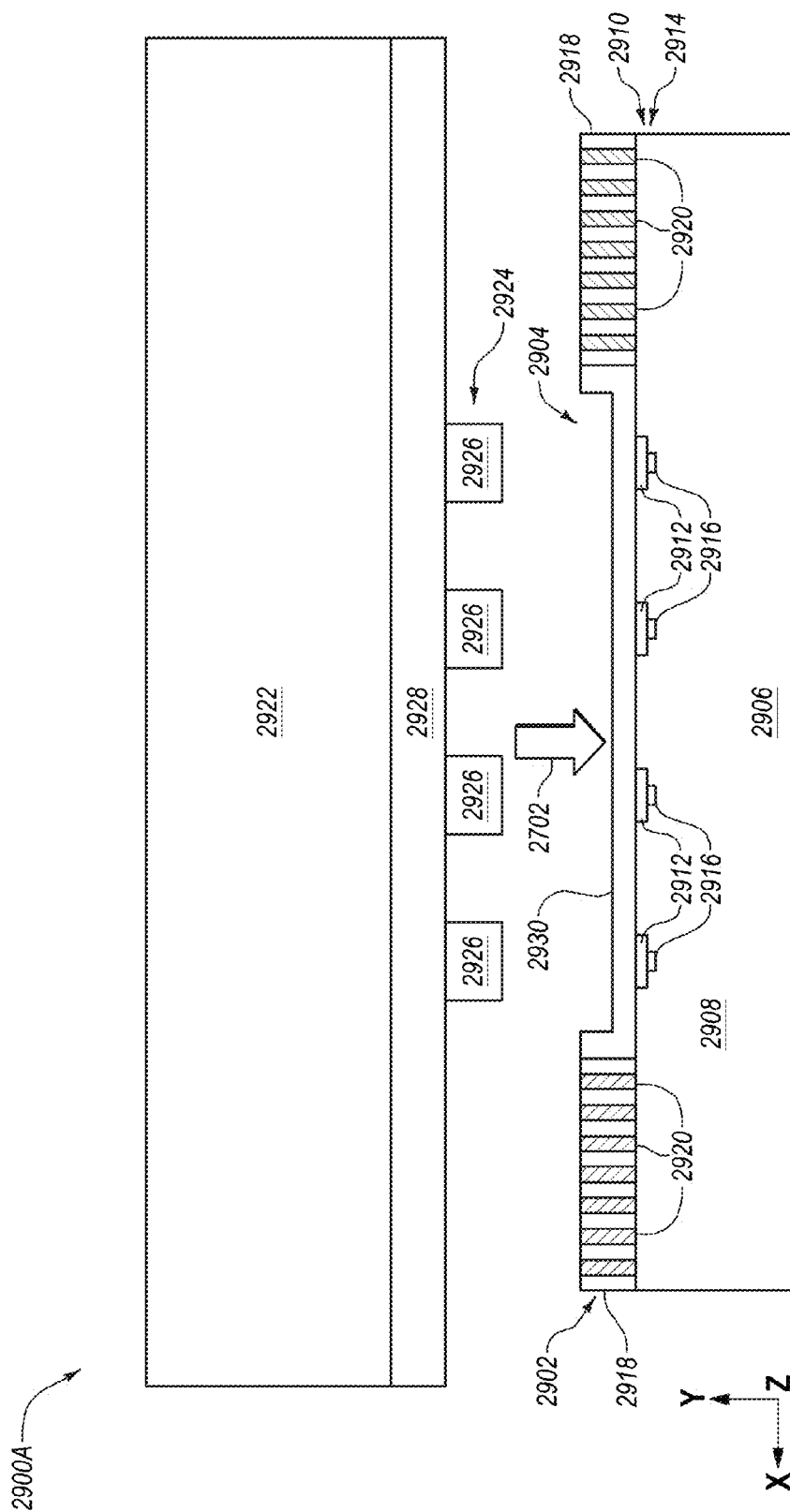


FIG. 29A

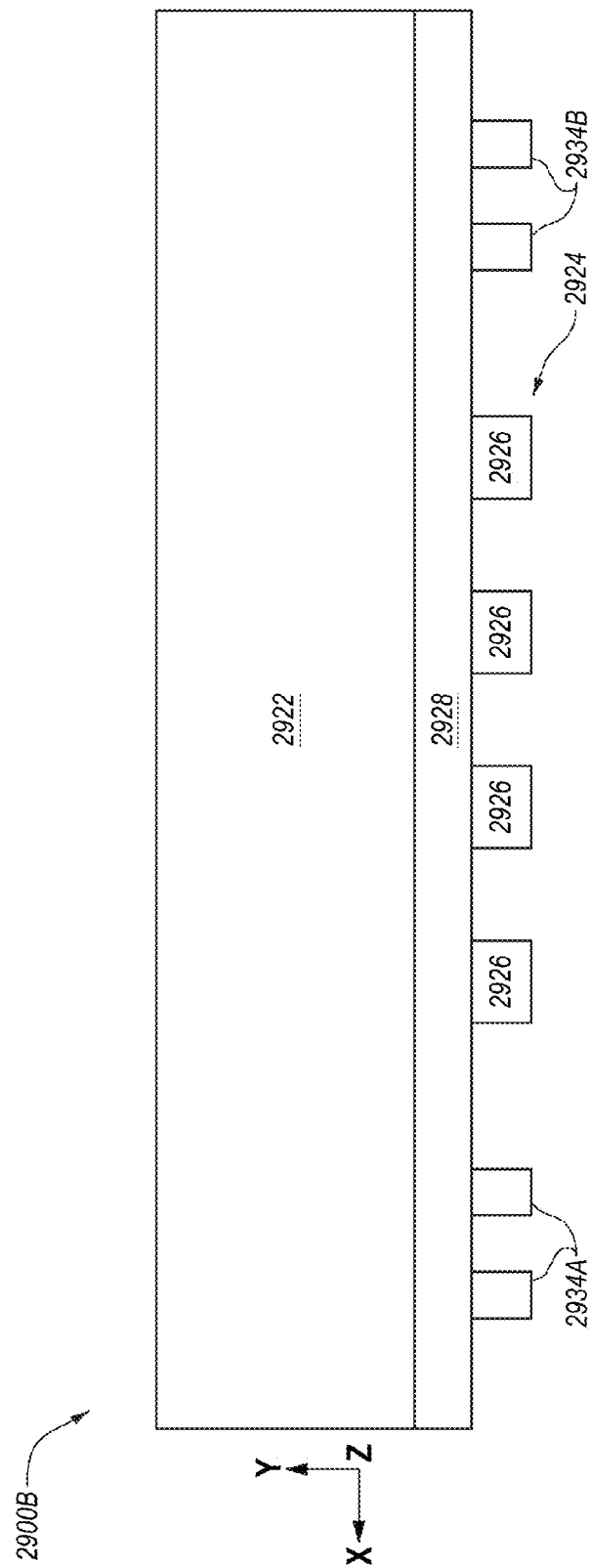


FIG. 29B

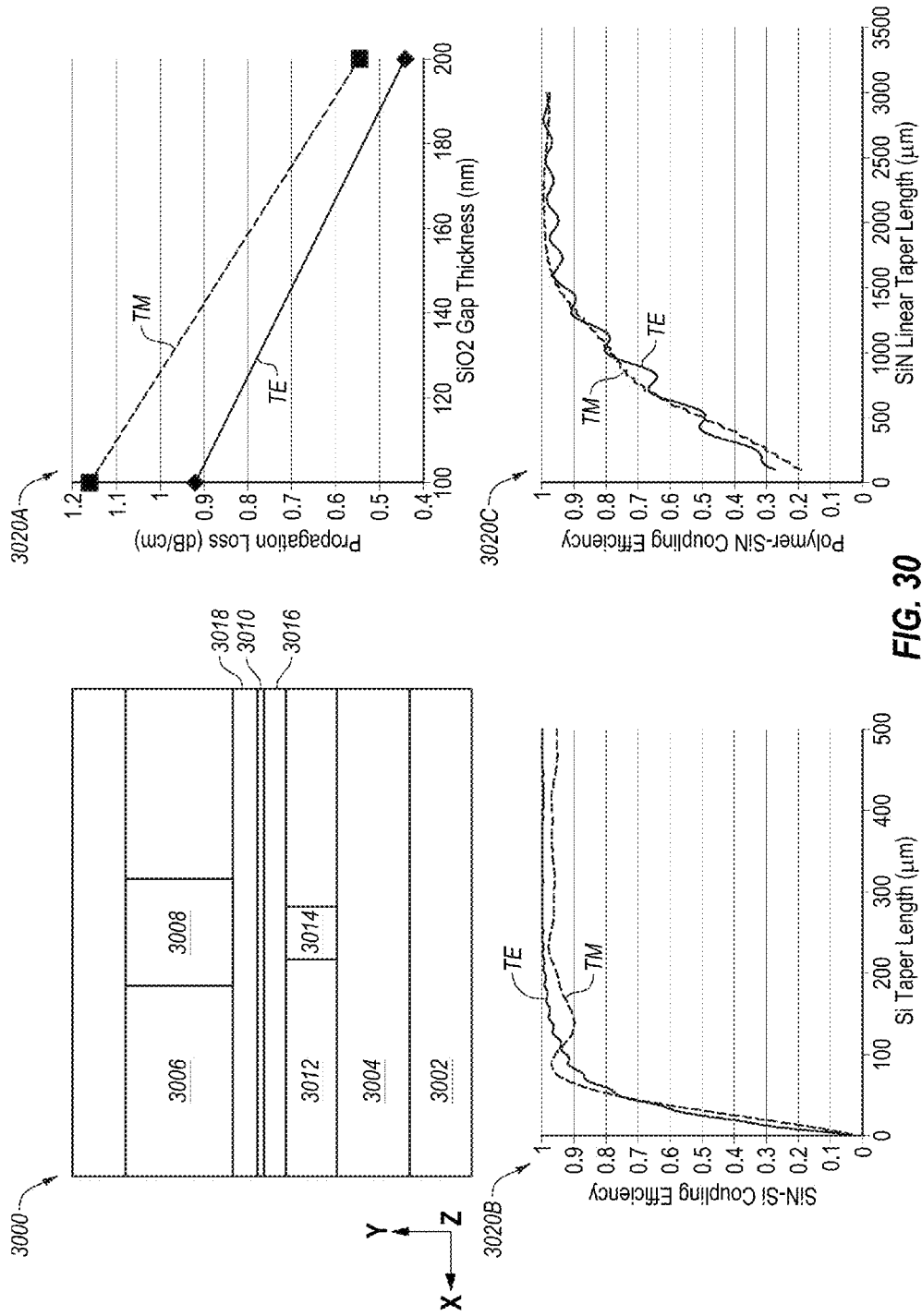


FIG. 30

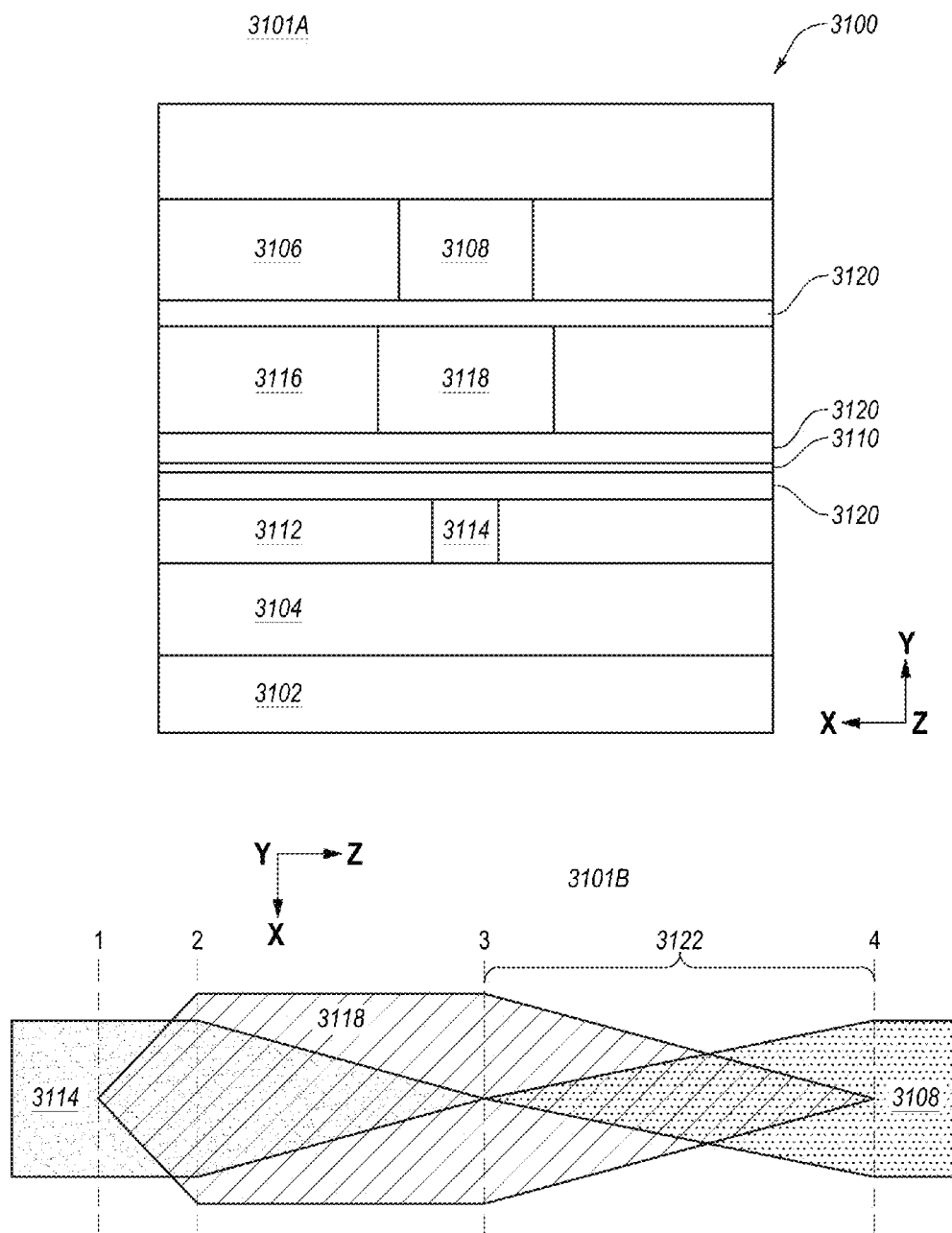


FIG. 31A

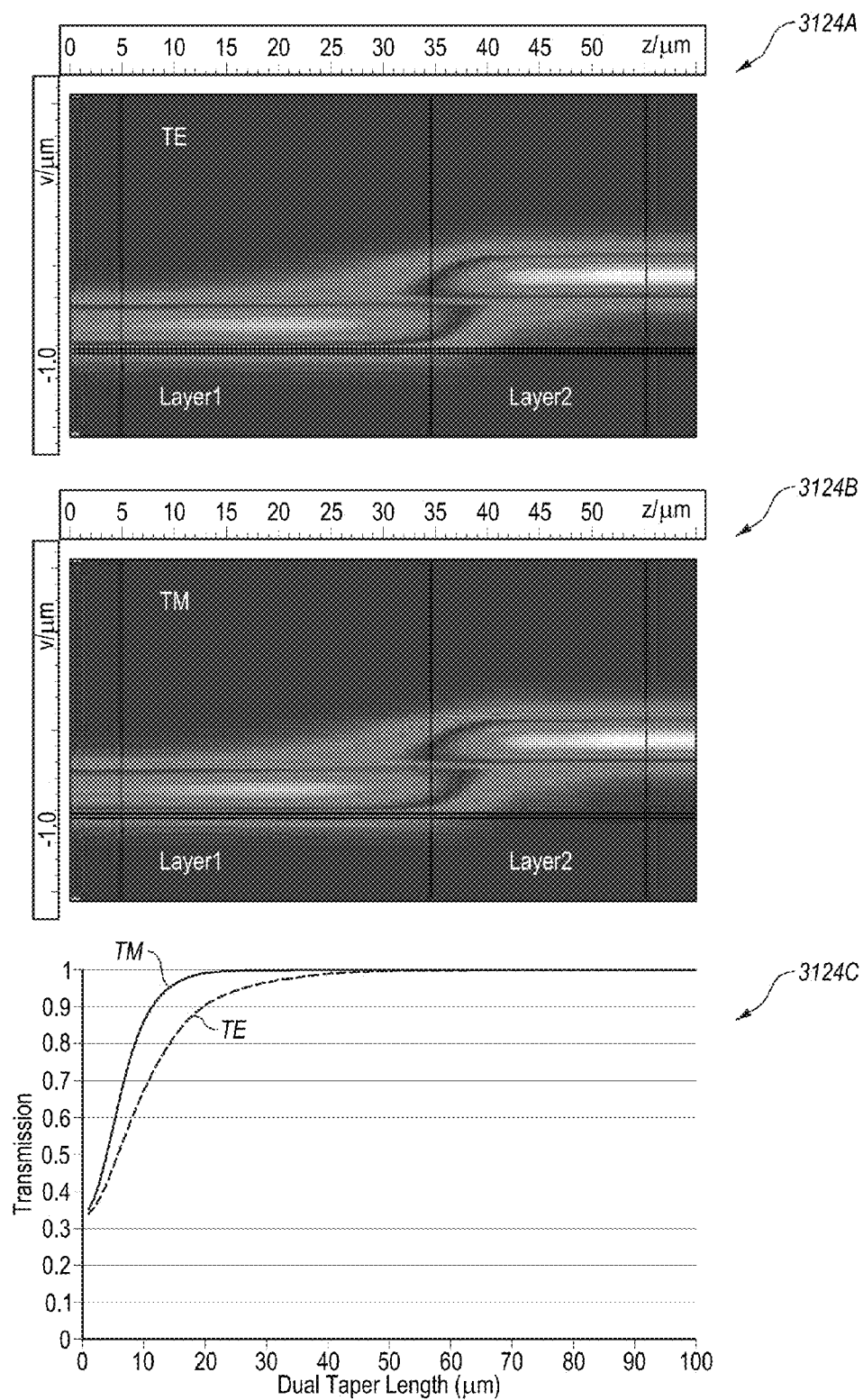


FIG. 31B

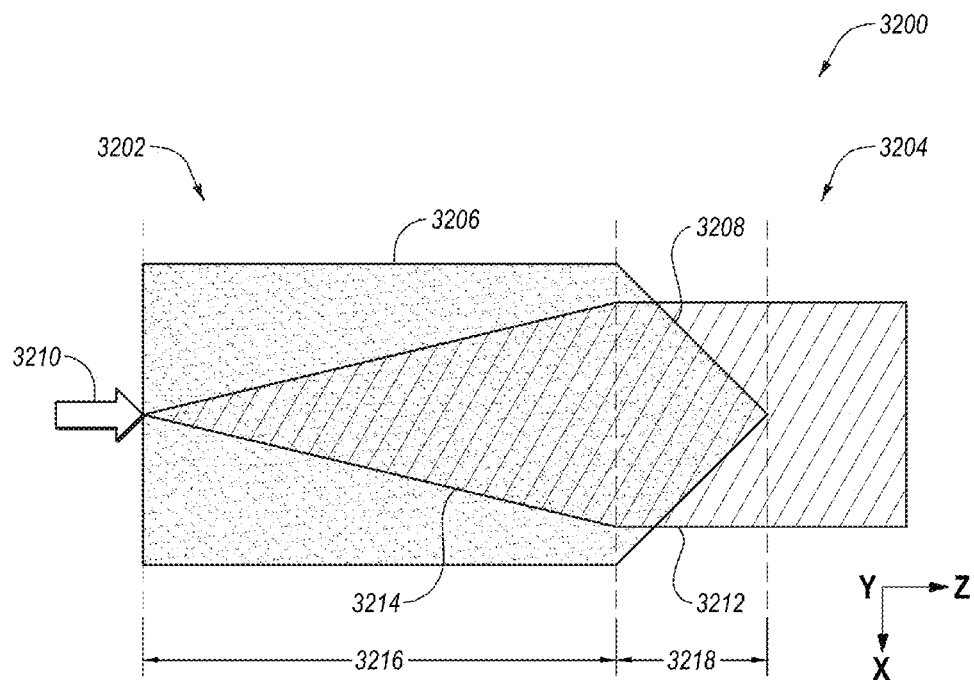


FIG. 32

3302

	First Region 3216	Second Region 3218
Length	90 $\mu\text{m}$	10 $\mu\text{m}$
Si Waveguide Width	0.08 $\mu\text{m}$ $\rightarrow$ 1.5 $\mu\text{m}$	1.5 $\mu\text{m}$
SiN Waveguide Width	2 $\mu\text{m}$	2 $\mu\text{m}$ $\rightarrow$ 0.2 $\mu\text{m}$

3304

	TE00	TM00	TE01	TM01
Transmission	0.99	0.98	0.97	0.95

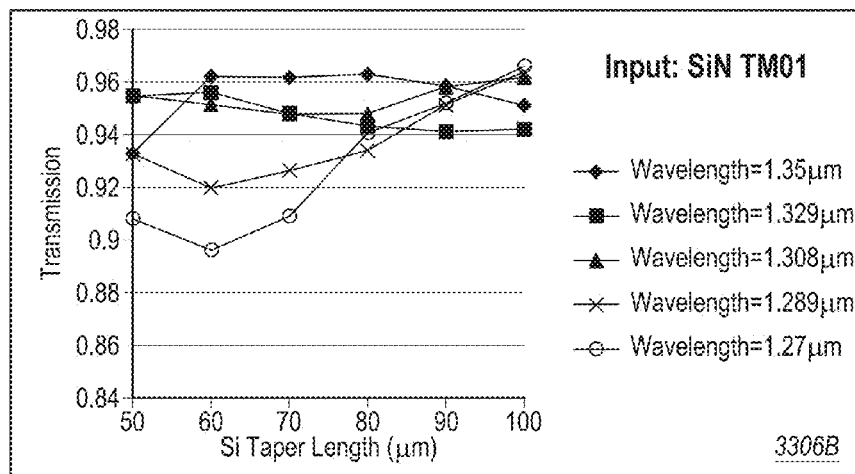
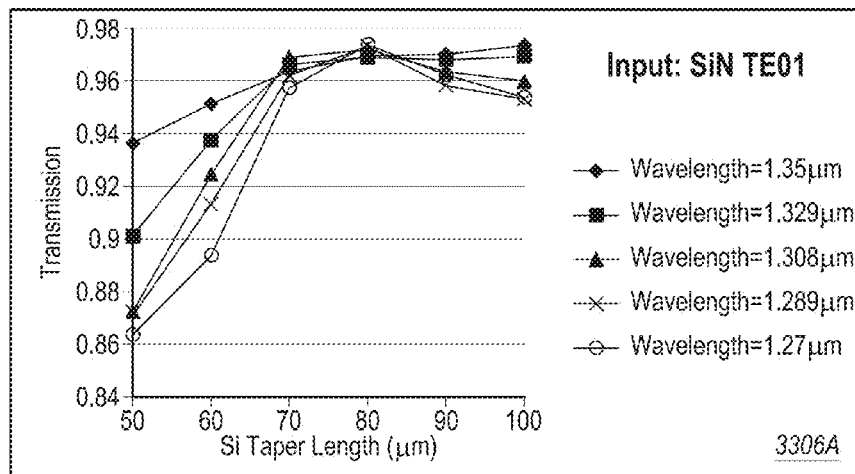
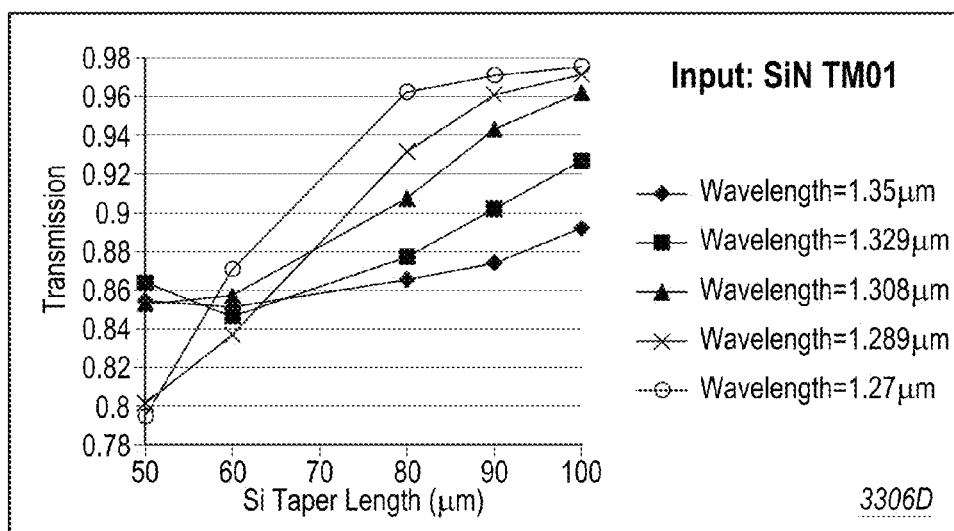
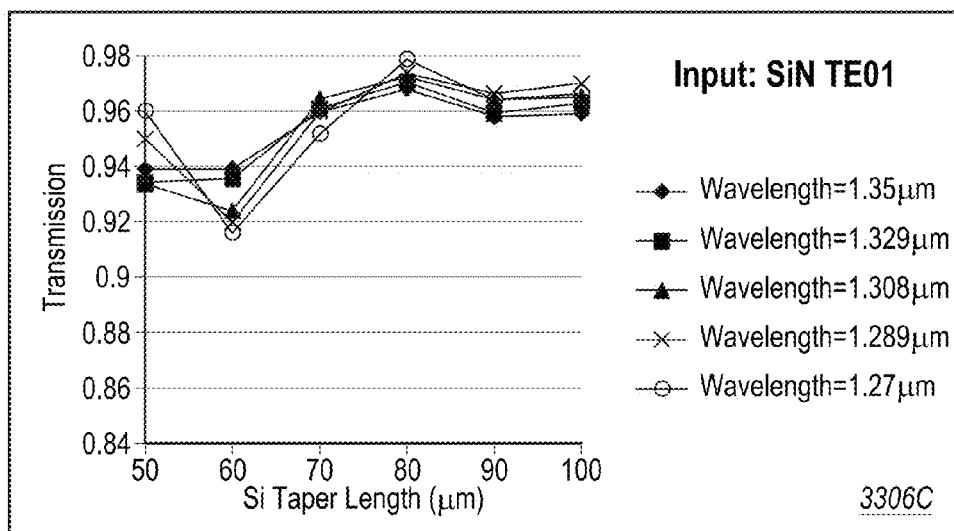
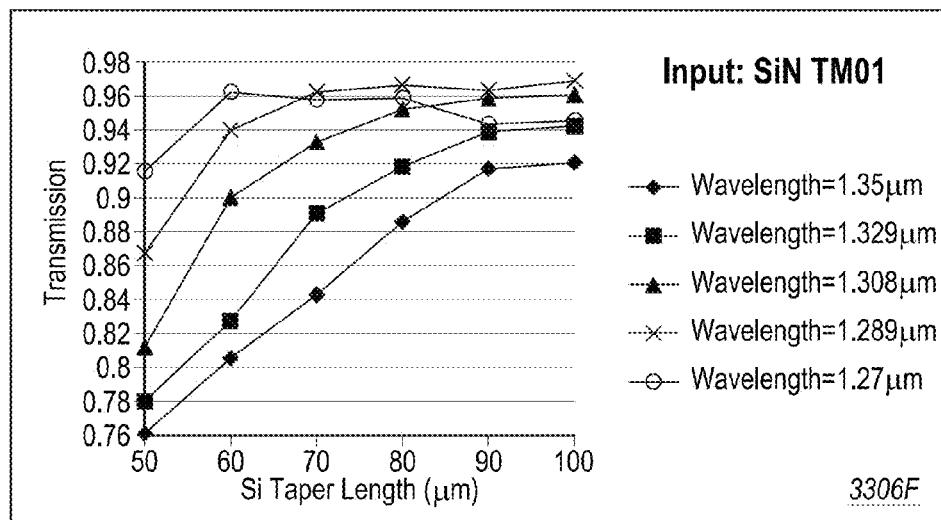
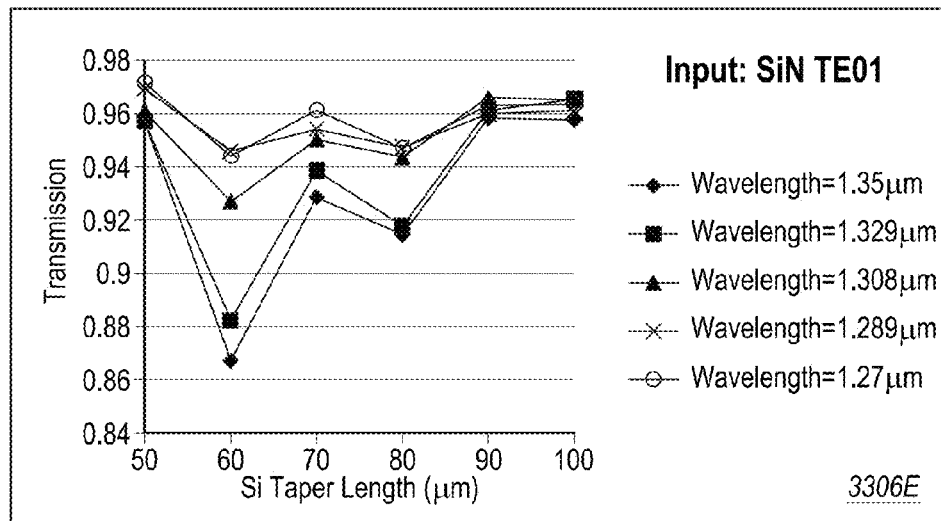


FIG. 33A



**FIG. 33B**

**FIG. 33C**

3308

	First Region 3216	Second Region 3218
Length	100 $\mu\text{m}$	10 $\mu\text{m}$
Si Waveguide Width	0.08 $\mu\text{m}$ $\rightarrow$ 1.5 $\mu\text{m}$	1.5 $\mu\text{m}$
SiN Waveguide Width	2.5 $\mu\text{m}$	2.5 $\mu\text{m}$ $\rightarrow$ 0.2 $\mu\text{m}$

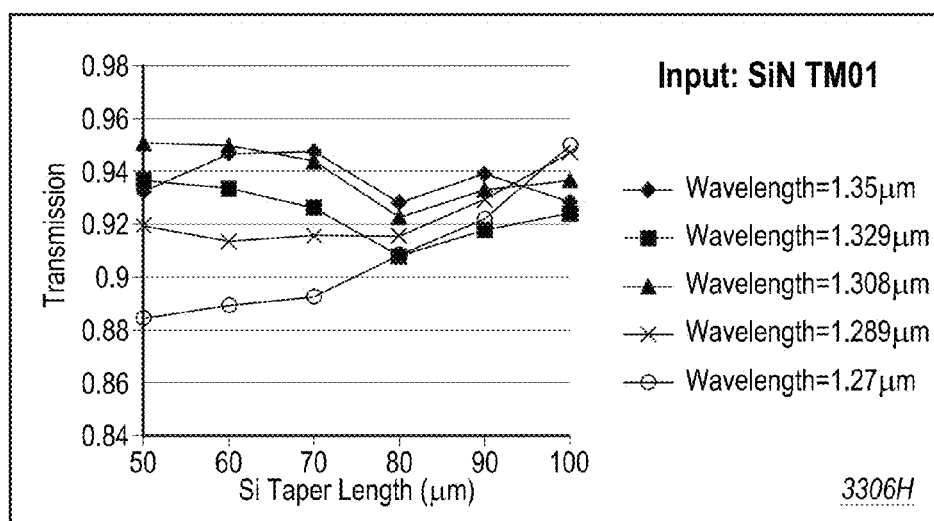
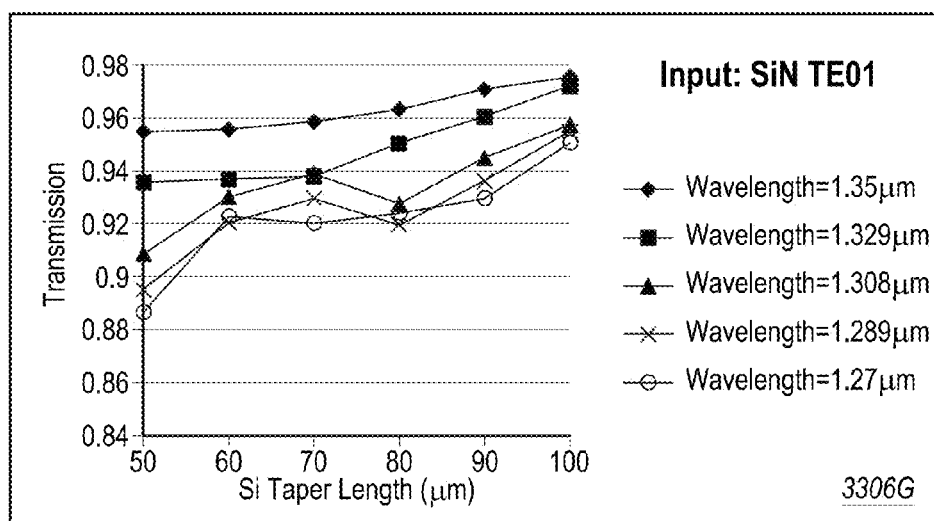
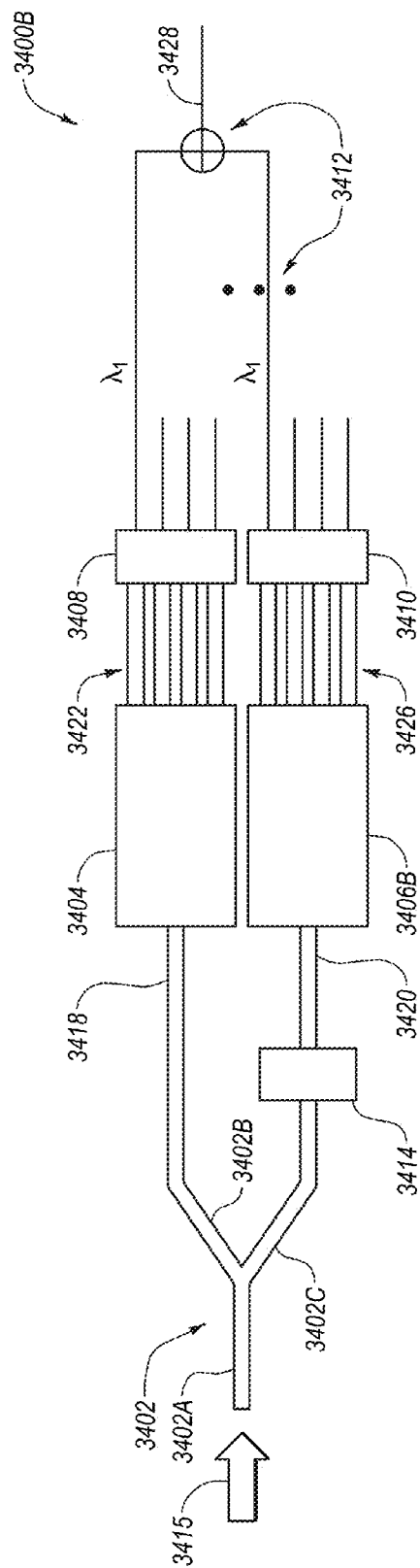
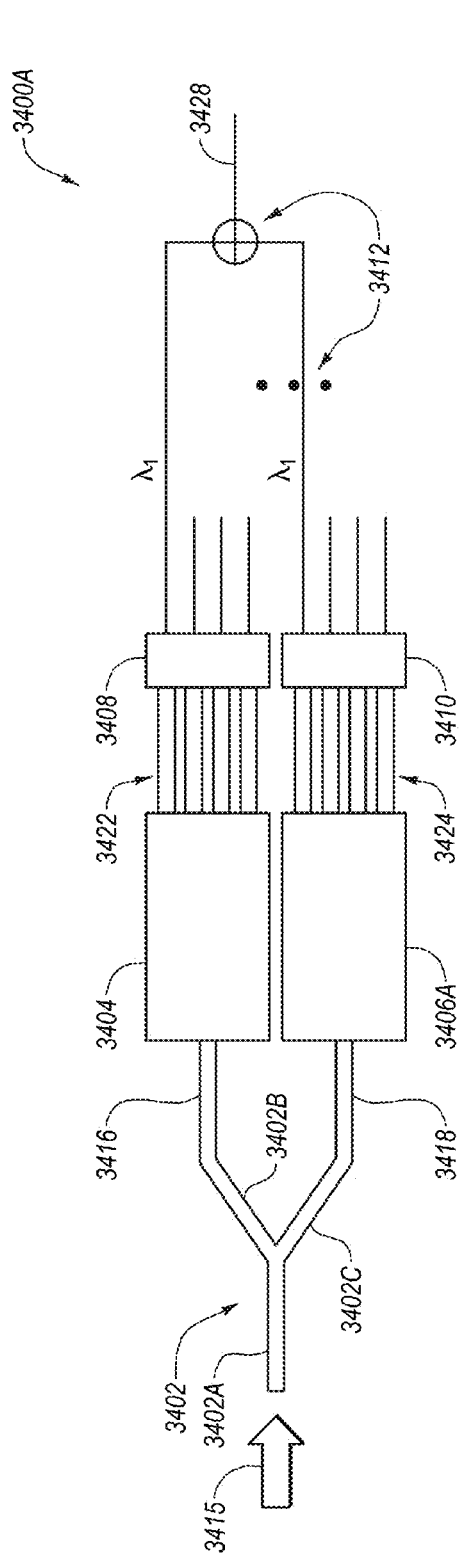


FIG. 33D



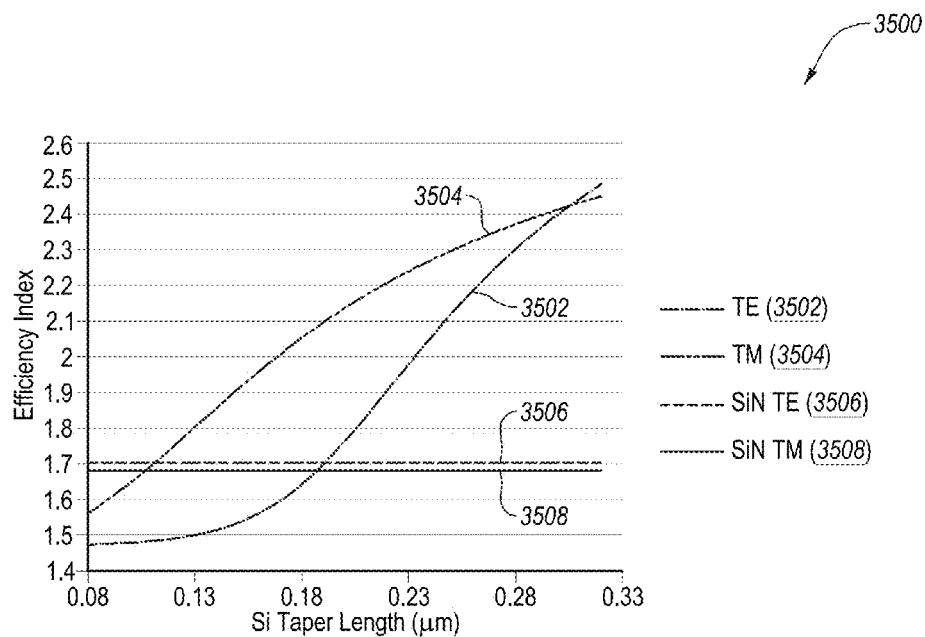


FIG. 35

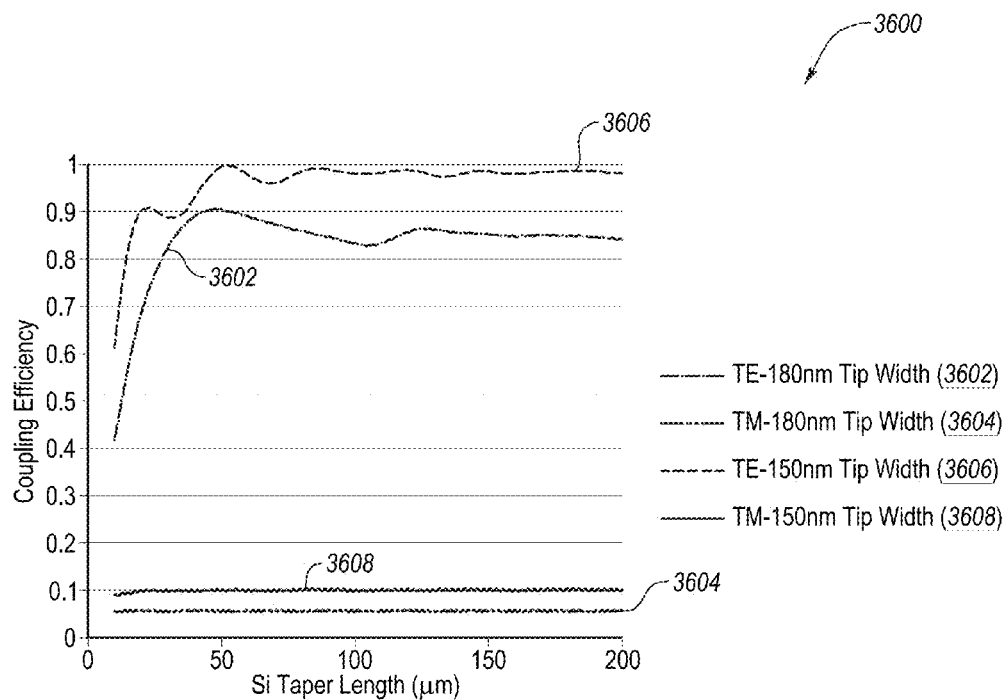
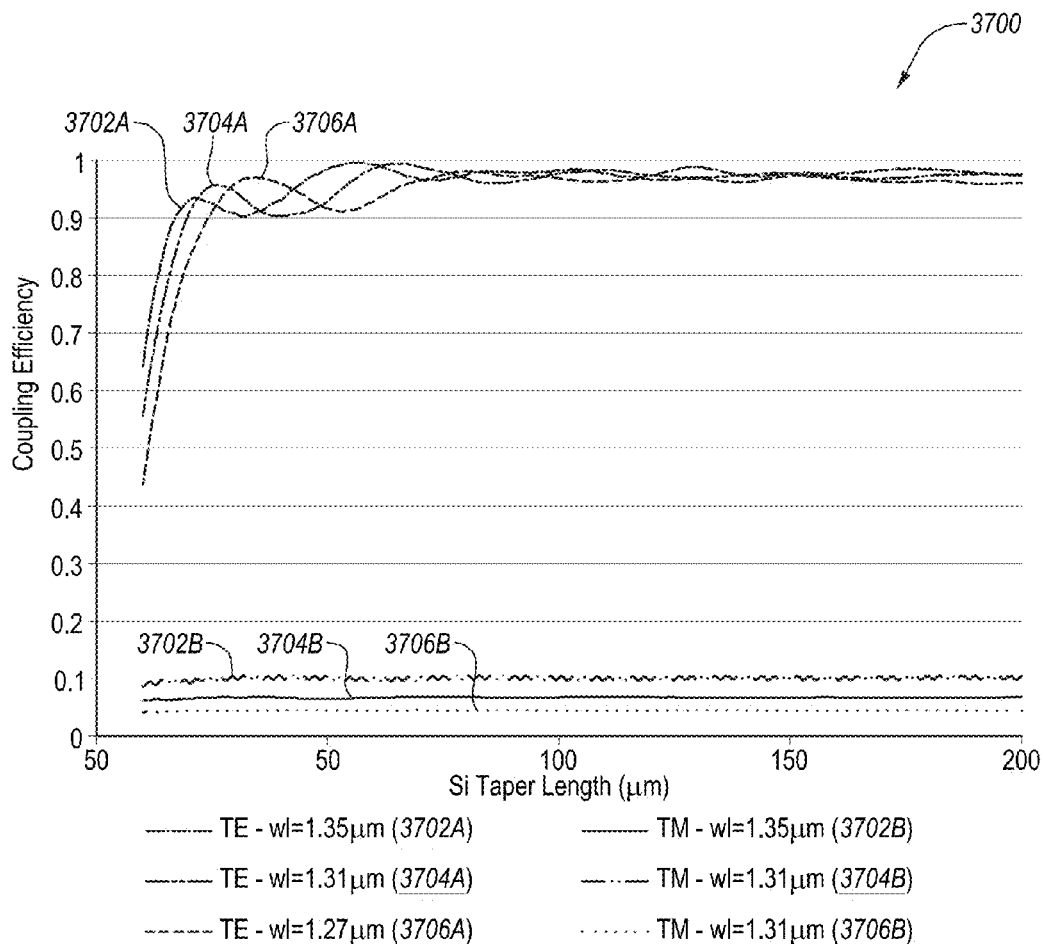


FIG. 36



3708

Wavelength( $\mu\text{m}$ )	1.35	1.31	1.27
TE	0.983	0.977	0.968
TM	0.102	0.067	0.0457
Ratio (TE/TM) (dB)	9.8	11.6	13.3

**FIG. 37**

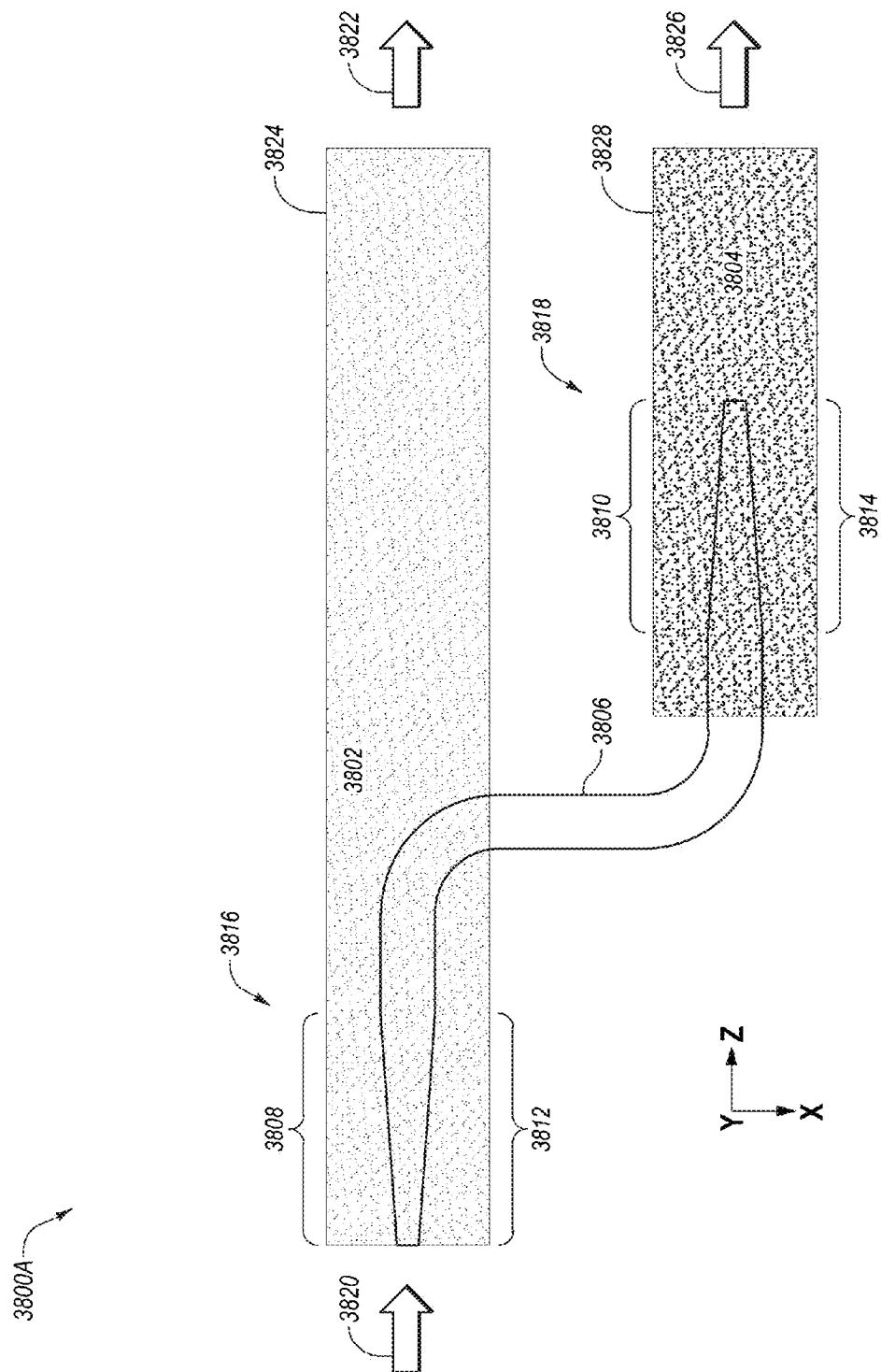


FIG. 38A

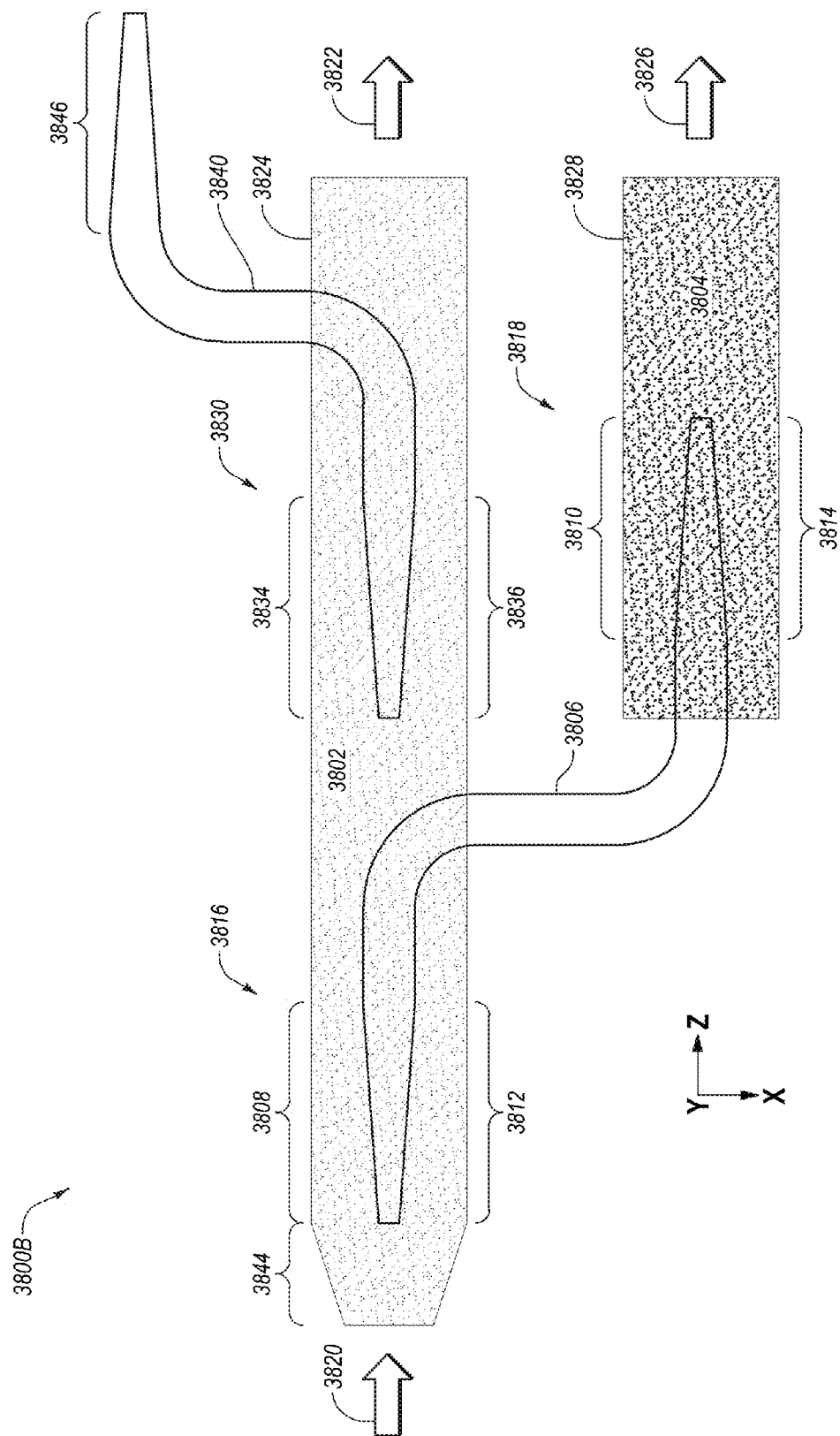


FIG. 38B



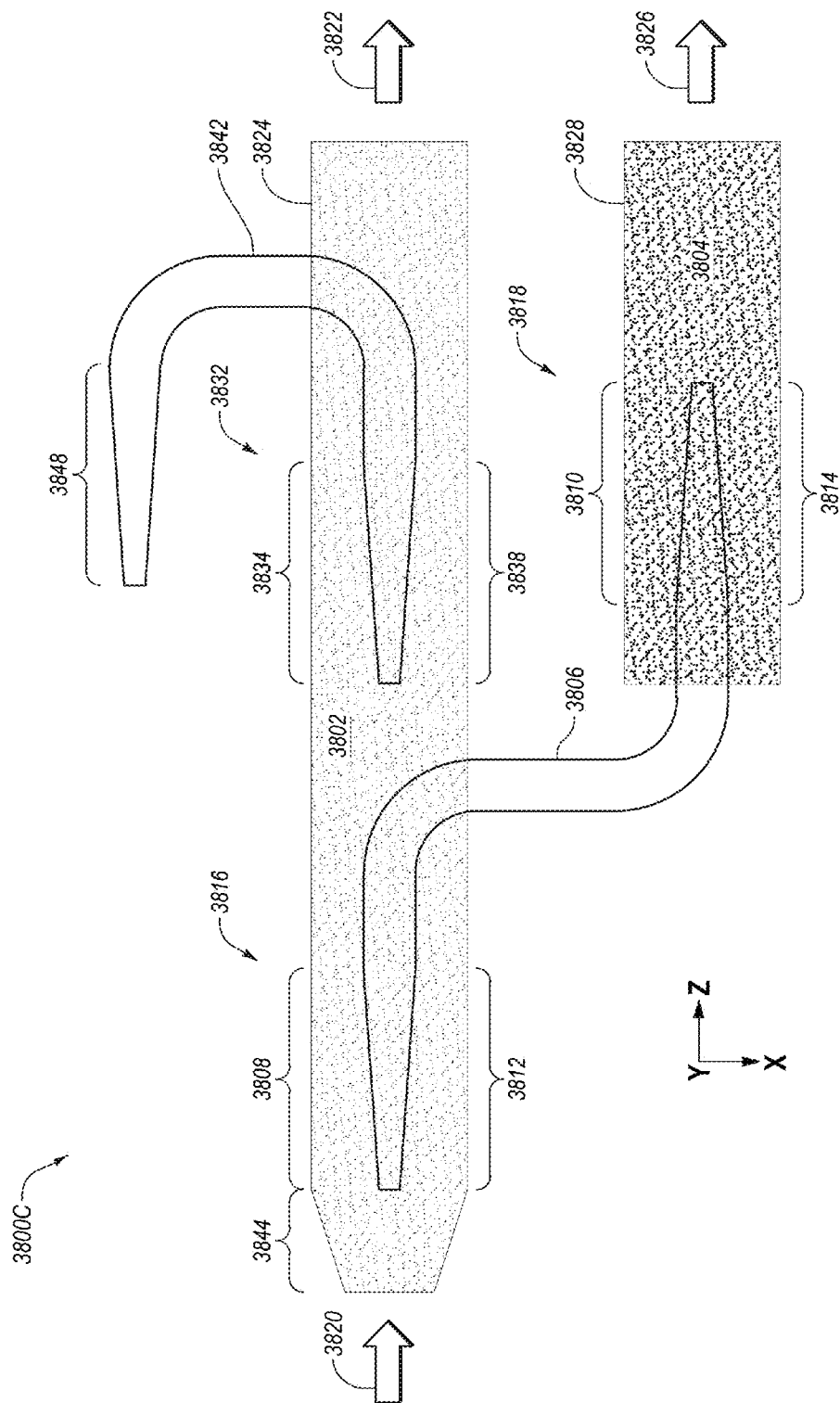


FIG. 38C

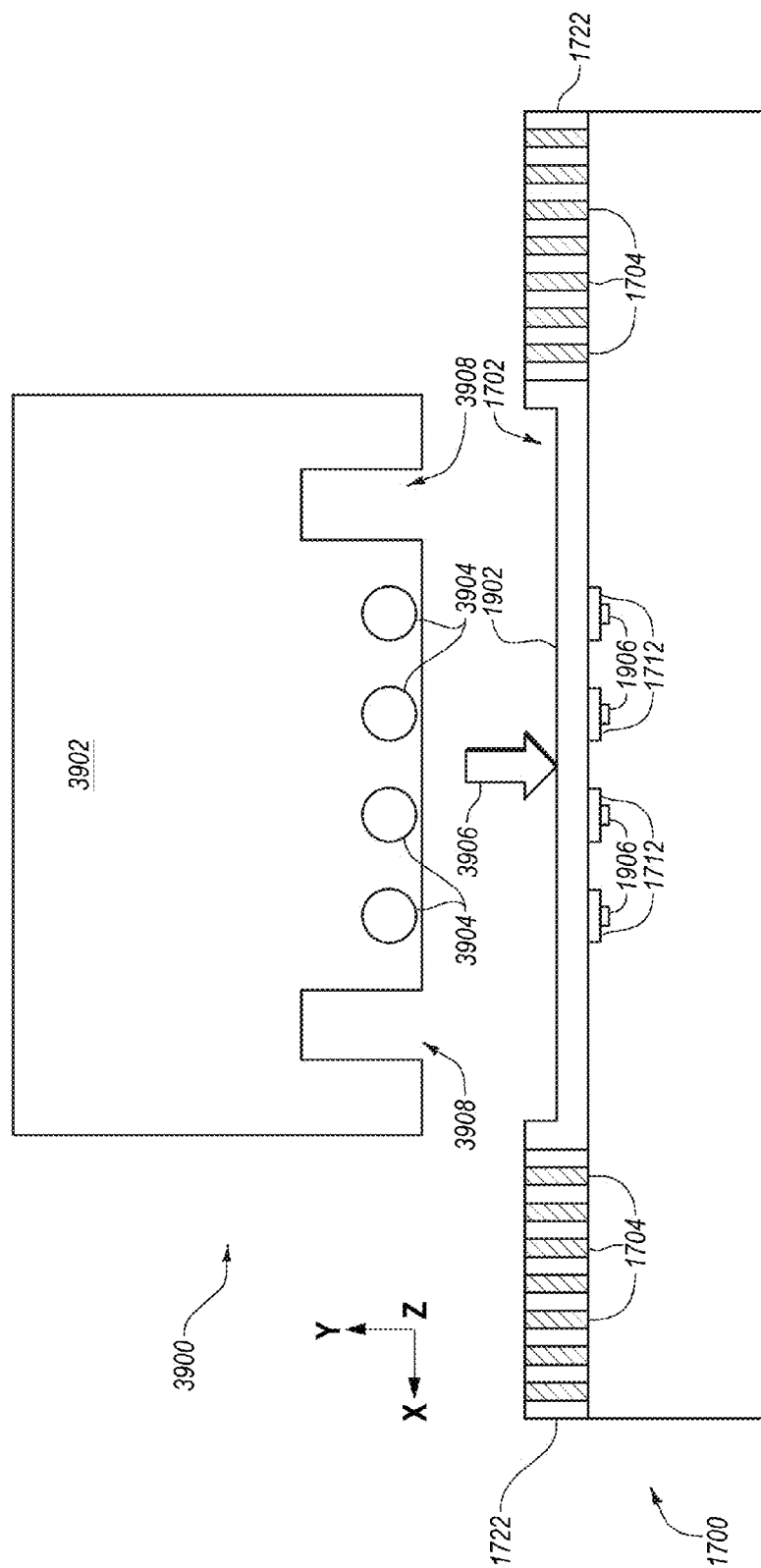


FIG. 39A

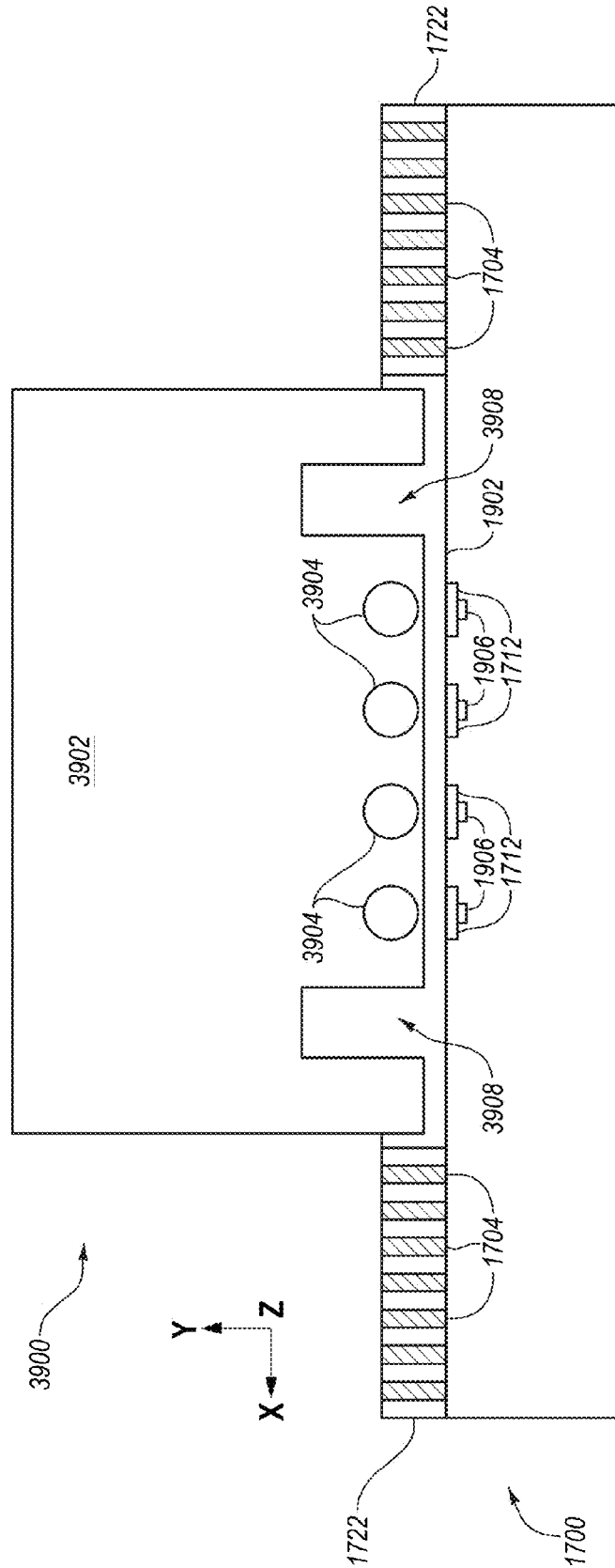


FIG. 39B

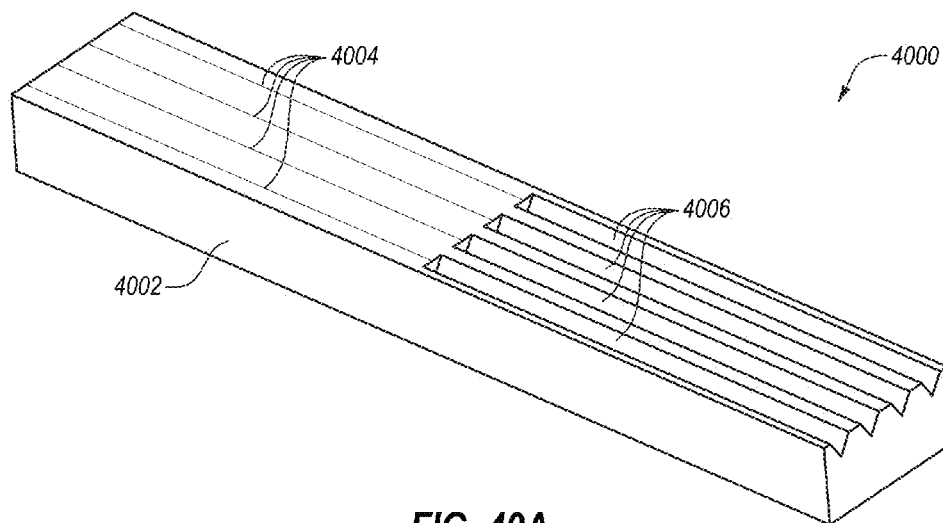


FIG. 40A

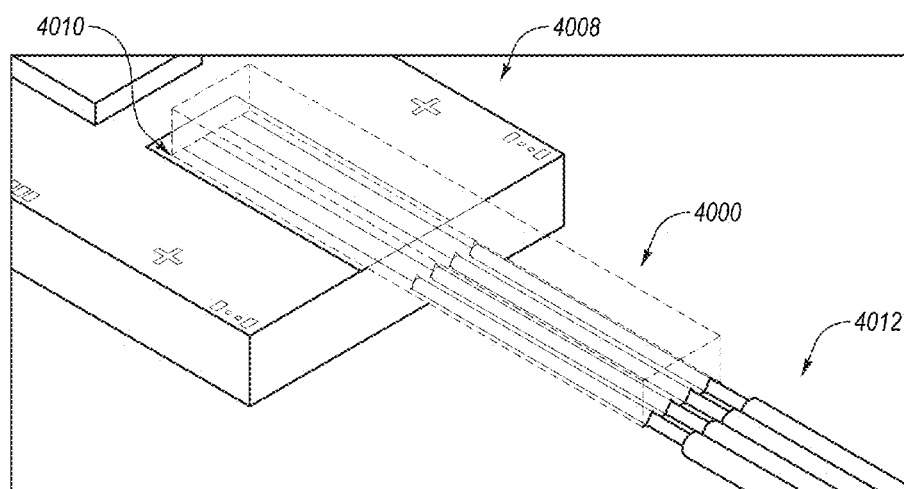


FIG. 40B

1

## TWO-STAGE ADIABATICALLY COUPLED PHOTONIC SYSTEMS

### CROSS-REFERENCE TO RELATED APPLICATIONS

The present application claims the benefit of and priority to U.S. Provisional Patent Application No. 62/078,259, filed on Nov. 11, 2014, U.S. Provisional Patent Application No. 62/120,194, filed on Feb. 24, 2015, U.S. Provisional Patent Application No. 62/181,679, filed on Jun. 18, 2015, and U.S. Provisional Patent Application No. 62/238,542, filed on Oct. 7, 2015. The foregoing applications are incorporated herein by reference.

### FIELD

The embodiments discussed herein are related to two-stage adiabatically coupled photonic systems.

### BACKGROUND

Unless otherwise indicated herein, the materials described herein are not prior art to the claims in the present application and are not admitted to be prior art by inclusion in this section.

There are two common solutions to couple light into or out of a silicon (Si) photonic integrated circuit (PIC). For example, surface grating couplers on the Si PIC can couple light into or out of the Si PIC. However, many surface grating couplers are highly wavelength dependent and may have a relatively small pass band.

As another example, edge coupling from an edge of the Si PIC may be implemented to couple light into or out of the Si PIC. However, the edge coupling may require that the Si PIC have a cleaved facet and some fabs/manufacturers may be unable or unwilling to test such a process.

The subject matter claimed herein is not limited to implementations that solve any disadvantages or that operate only in environments such as those described above. Rather, this background is only provided to illustrate one example technology area where some implementations described herein may be practiced.

### BRIEF SUMMARY OF SOME EXAMPLE EMBODIMENTS

This Summary is provided to introduce a selection of concepts in a simplified form that are further described below in the Detailed Description. This Summary is not intended to identify key features or essential characteristics of the claimed subject matter, nor is it intended to be used as an aid in determining the scope of the claimed subject matter.

Some example embodiments described herein generally relate to two-stage adiabatically coupled photonic systems.

In an example embodiment, a coupled system may include a first waveguide, at least one second waveguide, and an interposer. The first waveguide may have a first refractive index  $n_1$  and a tapered end. The at least one second waveguide may each have a second refractive index  $n_2$ . The interposer may include a third waveguide having a third refractive index  $n_3$  and a coupler portion. The tapered end of the first waveguide may be adiabatically coupled to a coupler portion of one of the at least one second waveguide. A tapered end of one of the at least one second waveguide may be adiabatically coupled to the coupler portion of the third waveguide of the interposer. The first refractive index  $n_1$  may be greater than the second refractive index  $n_2$ , both of which may be greater

2

than the third refractive index  $n_3$ . The coupled system may be configured to adiabatically couple light between the first waveguide and the at least one second waveguide and between the at least one second waveguide and the third waveguide.

Additional features and advantages of the invention will be set forth in the description which follows, and in part will be obvious from the description, or may be learned by the practice of the invention. The features and advantages of the invention may be realized and obtained by means of the instruments and combinations particularly pointed out in the appended claims. These and other features of the present invention will become more fully apparent from the following description and appended claims, or may be learned by the practice of the invention as set forth hereinafter.

### BRIEF DESCRIPTION OF THE DRAWINGS

To further clarify the above and other advantages and features of the present invention, a more particular description of the invention will be rendered by reference to specific embodiments thereof which are illustrated in the appended drawings. It is appreciated that these drawings depict only typical embodiments of the invention and are therefore not to be considered limiting of its scope. The invention will be described and explained with additional specificity and detail through the use of the accompanying drawings in which:

FIG. 1 is a perspective view of an example optoelectronic system (hereinafter "system");

FIG. 2 is a side view of an example two-stage adiabatically coupled photonic system (hereinafter "photonic system") of FIG. 1;

FIGS. 3A-3B include various views of portions of the photonic system of FIGS. 1 and 2;

FIG. 4 includes a graphical representation of simulated coupling efficiency of TM polarized light from a Si waveguide to a SiN waveguide of FIGS. 3A-3B;

FIGS. 5A-5B include graphical representations of simulated light modes of TM and TE polarized light in the SiN waveguide of FIGS. 3A-3B at reference line 2;

FIG. 6 includes a graphical representation of simulated coupling efficiency of TM polarized light and TE polarized light from the SiN waveguide to an interposer waveguide of FIGS. 3A-3B;

FIG. 7 is a side view of another example two-stage adiabatically coupled photonic system (hereinafter "photonic system");

FIGS. 8A-8B include various views of portions of the photonic system of FIG. 7;

FIG. 9 is a side view of another example two-stage adiabatically coupled photonic system (hereinafter "photonic system");

FIG. 10 includes various simulations associated with the photonic system of FIG. 9;

FIG. 11 is a side view of another example two-stage adiabatically coupled photonic system (hereinafter "photonic system");

FIGS. 12A and 12B include an overhead view and a longitudinal cross-sectional view of another example optoelectronic system (hereinafter "system");

FIG. 13 is an overhead view of another example optoelectronic system (hereinafter "system");

FIG. 14 is an overhead view of an example arrayed waveguide grating (AWG) that may be formed as a passive optical device such as a WDM component using SiN;

3

FIG. 15 is an overhead view of an example cascade of MZ interferometers that may be formed as a passive optical device such as a WDM component using SiN;

FIG. 16 is a side view of another example two-stage adiabatically coupled photonic system (hereinafter “photonic system”);

FIG. 17 is a perspective view of an example Si PIC that defines an etched window;

FIG. 18 includes a bottom view and a side view of an implementation of a portion of an interposer that may be coupled to the Si PIC of FIG. 17 within the etched window of FIG. 17;

FIGS. 19A and 19B are side views that depict alignment and attachment of the interposer of FIG. 18 and the Si PIC of FIG. 17;

FIG. 20 is a side view that depicts alignment of another interposer and Si PIC;

FIG. 21 is a side view that depicts alignment of another interposer and Si PIC;

FIG. 22 includes a side view and a bottom view of another arrangement of an interposer with interposer alignment ridges and dummy interposer islands;

FIG. 23A is a side view of another example two-stage adiabatically coupled photonic system (hereinafter “photonic system”) that includes a Si PIC, an interposer, and an optical fiber end connector 2306 (hereinafter “connector”);

FIG. 23B is a perspective view of the interposer of FIG. 23A;

FIG. 24 is a perspective view of another example photonic system (hereinafter “photonic system”);

FIGS. 25A and 25B illustrate two different offset configurations for RX vs. TX SiN waveguides;

FIG. 26 includes a side view and a bottom view of a silicon oxynitride (SiON) interposer;

FIG. 27 is a side view that depicts alignment of the SiON interposer of FIG. 26 and the Si PIC of FIG. 17;

FIG. 28 illustrates two example optoelectronic systems (hereinafter “systems”) that each include at least one polymer on glass interposer;

FIG. 29A illustrates an example polymer on glass interposer and Si PIC;

FIG. 29B illustrates another example polymer on glass interposer;

FIG. 30 illustrates a cross-sectional view of an example Si PIC;

FIG. 31A illustrates another example Si PIC;

FIG. 31B illustrates first-third simulations for the Si PIC of FIG. 31A;

FIG. 32 illustrates a multimode SiN-to-Si adiabatic coupler region (hereinafter “coupler”);

FIGS. 33A-33D include various simulations for the coupler of FIG. 32 with various different sets of parameters;

FIGS. 34A and 34B illustrate embodiments of a demultiplexer system (collectively “demultiplexer systems”);

FIG. 35 is a graphical representation of a simulation of effective index as a function of Si waveguide width for TE and TM polarizations in Si and SiN waveguides of an adiabatic coupler region;

FIG. 36 is a graphical representation of a simulation of TE and TM polarization coupling efficiency as a function of Si waveguide taper length for a Si waveguide tip width of 180 nm and 150 nm;

FIG. 37 is a graphical representation of a simulation of TE and TM polarization coupling efficiency as a function of Si waveguide taper length for a Si waveguide tip width of 160 nm for three different wavelength channels;

4

FIGS. 38A-38C illustrate example Si PIC polarization splitters or combiners (hereinafter collectively “polarization splitters”);

FIGS. 39A and 39B include side views that depict alignment and attachment of a high index glass interposer (hereinafter “interposer”) and the Si PIC of FIG. 17;

FIG. 40A includes an upside down perspective view of another high index glass interposer (hereinafter “interposer”); and

FIG. 40B includes a perspective view of the interposer of FIG. 40A adiabatically coupled to a Si PIC 4008,

all arranged in accordance with at least one embodiment described herein.

#### DETAILED DESCRIPTION OF SOME EXAMPLE EMBODIMENTS

Some embodiments described herein generally relate to adiabatic coupling of light from a silicon (Si) waveguide to an intermediate silicon nitride ( $\text{Si}_3\text{N}_4$ , generically referred to herein as SiN) waveguide and then from the SiN waveguide to an interposer waveguide (e.g., polymer or high index glass waveguide), or vice versa. For ease of reference in the discussion that follows, the adiabatic coupling is often discussed in the context of a single Si waveguide-to-SiN waveguide-to-interposer waveguide coupling with the understanding that multiple such couplings may be included in a given system.

The Si waveguide may have a first optical mode size, the SiN waveguide may have a second optical mode size substantially larger than the first optical mode size, and the polymer or other interposer waveguide may have a third optical mode size substantially larger than the second mode size. For example, the first optical mode size may be about 0.3  $\mu\text{m}$ , or in a range between 0.25  $\mu\text{m}$  and 0.5  $\mu\text{m}$ ; the second optical mode size may be about 1  $\mu\text{m}$ , or in a range between 0.7  $\mu\text{m}$  and 3  $\mu\text{m}$ ; and the third optical mode size may be about 10  $\mu\text{m}$ , or in a range between 8  $\mu\text{m}$  and 12  $\mu\text{m}$ . The third optical mode size may be substantially similar to an optical mode size of a standard single mode optical fiber. For example, a standard single mode optical fiber may have an optical mode size of about 10  $\mu\text{m}$ , which is substantially similar to the third optical mode size.

The Si waveguide may be inverse tapered to a width of about 80 nanometers (nm) to increase a size of the light mode and bring it out into a cladding of the Si waveguide. The SiN waveguide may be fabricated on a Si photonic integrated circuit (PIC) that includes the Si waveguide. The SiN waveguide may receive the light from the Si inverse taper. Similar to the Si waveguide, the SiN waveguide may be inverse tapered to a width of 80-300 nm. The interposer waveguide with approximately a 3-8 ( $\mu\text{m}$ ) core may be placed in close optical contact with the SiN waveguide. Light from the Si waveguide inverse taper may be adiabatically coupled to the SiN waveguide and then to the interposer waveguide in steps along the direction of propagation and may be completely or substantially completely translated to it. The interposer waveguide may be processed on a separate rigid or flexible substrate and may be attached to the SiN waveguide using various techniques including thermo-mechanical attachment, or by use of index matching adhesive. The Si PIC may include modulators, waveguides, detectors, couplers, and other optical components in a Si on Insulator (e.g., silicon on silicon dioxide ( $\text{SiO}_2$ ) box layer) on Si substrate. An integrated circuit (IC) may be flip chip bonded (e.g., by copper pillar) on the Si PIC in a portion of the Si PIC away from a coupling region where the SiN waveguide and interposer waveguide may be located. The interposer waveguide may be

included in an interposer that may be transparent and/or have that may have alignment marks to allow ease in optical alignment of the SiN waveguide on the Si PIC with the interposer waveguide on the interposer. The interposer waveguide and the SiN waveguide can be aligned either passively or actively.

The SiN waveguide or waveguides may be defined in a fabrication process of the Si PIC to which a SiN/SiO<sub>2</sub> layer section is added for coupling and passive functions. A standard Si photonic stack layer has a Si substrate, SiO<sub>2</sub> oxide layer (called BOX or SiO<sub>2</sub> box), and Si waveguide layer in which Si waveguides are surrounded by SiO<sub>2</sub> cladding to confine the light. Embodiments described herein may add a SiN layer to this standard stack for two stage coupling and optionally passive optical functions. The SiN layer has regions of SiN core waveguides surrounded by SiO<sub>2</sub> cladding to confine the light. SiN has an intermediate index of refraction between indexes of refraction of Si and polymer and so allows efficient adiabatic coupling between the two layers with taper widths that are within critical dimensions of some standard complementary metal-oxide-semiconductor (CMOS) fabs. The low loss of SiN and the lower core/cladding index difference of SiN relative to SiO<sub>2</sub> cladding compared to that of Si and SiO<sub>2</sub> allows fabrication of passive components with better performance. For example wavelength division multiplexers (WDM mux) and demultiplexers (WDM demux) in SiN have higher channel isolation than in Si. In addition, passive components in SiN have a 5× smaller drift of peak wavelengths with temperature relative to the same in Si.

In some embodiments, transmit (TX) and receive (RX) Si waveguides on the Si PIC may be in one plane or accessible at one planar interface of the Si PIC whereas an MT connector for parallel single mode fibers can have configurations by multisource agreement (MSA) in which a TX array is in one row and a RX array is in a row below it. It may also be possible for both TX and RX to be in the same row but separated. Embodiments described herein include a an interposer that can connect from SiN waveguide inputs/outputs in a plane of the Si PIC and present to, e.g., an MT connector, two vertically separated rows of inputs/outputs.

In some embodiments, wavelength division multiplexing or other passive optical functions may be integrated in a same SiN/SiO<sub>2</sub> layer in which the SiN waveguide is formed. Use of the SiN/SiO<sub>2</sub> layer may be advantageous as compared to implementing such optical functions in other layers and/or materials in that it may provide lower loss, better channel isolation due to lower loss in SiN and smaller index difference between core and cladding.

Some embodiments described herein may be wavelength independent over a range of operation. For instance, some embodiments described herein may be wavelength independent over a range of operation of 1310 nm standard long reach (LR) standards, whereas surface grating couplers may have a relatively narrow 20-30 nm pass band.

The Si waveguide and the SiN waveguide are included in different layers of the Si PIC. The Si waveguide may include Si as the waveguide core surrounded by SiO<sub>2</sub> as the waveguide cladding. Similarly, the SiN waveguide may include SiN as the waveguide core surrounded by SiO<sub>2</sub> as the waveguide cladding.

In some embodiments, the layer of the Si PIC that includes the SiN waveguide is below the layer of the Si PIC that includes the Si waveguide and below the interposer waveguide. To make the fabrication of the Si/SiO<sub>2</sub> with SiN/SiO<sub>2</sub> compatible with a standard Si photonic process, which currently may not include a layer for the SiN waveguide, it may be possible to use wafer bonding to fabricate a structure

with fully processed Si (so called Front End of Line (FEOL)) and Back End of Line (BEOL) with SiN in a lower layer. Given this structure and a window that can be etched for coupling, the optical coupling between the SiN waveguide and the interposer waveguide can be achieved. As such, light propagating from the Si waveguide to the SiN waveguide to the interposer waveguide may go from the Si waveguide down to the SiN waveguide and then up into the interposer waveguide, where it may then be coupled into an optical fiber or the like, or light may travel on the reverse path. In these and other embodiments, the interposer waveguide can include polymer or a high index glass waveguide having similar cladding refractive index near 1.5.

Whether the layer of the Si PIC that includes the SiN waveguide is below or above the layer of the Si PIC that includes the Si waveguide, the SiN waveguide may be included in a region of the Si PIC that includes a wavelength division multiplexing (WDM) component within the Si PIC. Alternatively or additionally, a SiO<sub>2</sub> cladding that surrounds the SiN waveguide may be relatively thick and/or the SiN waveguide may have a square cross-sectional profile to render the SiN waveguide polarization insensitive.

In some embodiments in which the layer of the Si PIC that includes the SiN waveguide is below the layer of the Si PIC that includes the Si waveguide, a semiconductor chip with an indium phosphide (InP)-based gain element or InP-based pin detector may be wafer bonded to the Si PIC above the layer of the Si PIC that includes the Si waveguide. In the case of an InP-based gain element, light emitted by the InP-based gain element may be optically coupled into the Si waveguide, and then into the SiN waveguide, and then into the interposer waveguide, and then into, e.g., an optical fiber. In the case of an InP-based pin detector, light received into the interposer waveguide may be coupled into the SiN waveguide, then into the Si waveguide, and then into the InP-based pin detector.

In some embodiments, a top layer of the Si PIC may include metal 'dummies,' at least in a region that bounds an area to be etched as an etched window for a polymer (or other material) waveguide strip that includes the interposer waveguide, e.g., a polymer waveguide in this example. Metal 'dummies' are arrays of metal filled holes in the dielectric stack that function to produce a mechanically flat surface on average over the wafer after chemical mechanical polishing (CMP) in the BEOL process. They are so called dummies because they do not function as electrical contacts, whereas other metal in the BEOL process functions as electrical connections between various contacts and the output electrical ports of the PIC. The top layer and any intervening layers down to the layer of the Si PIC that includes the SiN waveguide may be etched through down to the layer that includes the SiN waveguide to receive in the etched window the polymer waveguide strip and allow the polymer waveguide to be optically coupled to the SiN waveguide. In some embodiments, polymer ridges, anchor windows, and/or dummy polymer islands may be provided to facilitate alignment and mechanical connection between the Si PIC and a polymer interposer that includes the polymer waveguide.

In some embodiments, WDM components included in the Si PIC may be polarization sensitive. For example, WDM components such as SiN based Echelle gratings may exhibit a polarization-dependent filter function. In particular, the filter function of such WDM components may shift one polarization of light more than another polarization of light which can lead to cross-talk for channels at a receiver. For example, a SiN based Echelle grating may shift TE polarization at a 1310 nm wavelength channel to an output guide that also

receives TM polarization at a different wavelength channel, resulting in cross-talk between the two channels.

Accordingly, the Si PIC may additionally include a polarization splitter. In general, the polarization splitter may use an SiN/Si adiabatic coupler that includes two SiN waveguides and at least one Si waveguide with two tapered ends. The tapered ends of the Si waveguide may have tip widths that favor adiabatic coupling of one of two polarizations of light over the other. For example, TM polarization may couple from SiN to Si at a much narrower Si tip width than TE polarization. The Si tip width may be selected to, in general, adiabatically couple TE polarization from the first SiN waveguide through the Si waveguide to the second SiN waveguide, while the TM polarization generally remains in the first SiN waveguide.

In the discussion that follows, numerous embodiments are disclosed. The various embodiments are not mutually exclusive unless context dictates otherwise. For instance, a portion or all of one or more embodiments may be combined with a portion or all of one or more other embodiments unless context dictates otherwise.

Reference will now be made to the drawings to describe various aspects of example embodiments of the invention. It is to be understood that the drawings are diagrammatic and schematic representations of such example embodiments, and are not limiting of the present invention, nor are they necessarily drawn to scale.

FIG. 1 is a perspective view of an example optoelectronic system **100** (hereinafter “system **100**”), arranged in accordance with at least one embodiment described herein. As illustrated, the system **100** includes a Si PIC **102**, an interposer **104**, a three-dimensional (3D) stack region **106**, and a flip chip bonded integrated circuit (IC) **108**. The Si PIC **102** and the interposer **104** together form a two-stage adiabatically coupled photonic system **200** (hereinafter “photonic system **200**”).

In general, the Si PIC **104** may include one or more optical elements, such as a modulator, waveguide, coupler, or other optical element(s) in a Si-on-insulator substrate.

In general, the 3D stack region **106** may provide electrical connections to one or more active optical components of the Si PIC **104**. Accordingly, the 3D stack region **106** may include, e.g., metallized pillars, traces, and/or contacts as well as insulative dielectric and/or other materials and elements.

In general, the flip chip bonded IC **108** may include one or more active and/or passive electrical devices that may be communicatively coupled through the 3D stack region **106** to the one or more active optical components of the Si PIC **104**.

The interposer **104** may be mechanically coupled to the Si PIC **102**. An interposer waveguide of the interposer **104** and a SiN waveguide and Si waveguide of the Si PIC **102** may be configured to adiabatically couple light into or out of the Si PIC **102**. As used herein, light may be adiabatically coupled from one optical component or device, which here we call the ‘initial state’ waveguide to another, here called the final state waveguide, in a transitional interaction region, sometimes referred to herein as an adiabatic coupler region. To transfer optical power from the initial state waveguide to the final state waveguide one or more optical properties of either or both initial and final state waveguides, such as width, height, effective refractive index, etc. are varied along the optical axis. Here the initial state and final state waveguides form one system within the transitional interaction region and light remains in a single mode of the joint system while it physically gets transferred from the initial state waveguide to the final state waveguide. The initial state and final state waveguides may respectively correspond to the Si waveguide

and the SiN waveguide, or vice versa. Alternatively or additionally, the initial and final state waveguides may respectively correspond to the SiN waveguide and the interposer waveguide, or vice versa. Alternatively or additionally, two components may be said to be adiabatically coupled together or to each other when the two components are configured as described herein to form an adiabatic coupler region.

Moreover, light is used generically herein to refer to electromagnetic radiation of any suitable wavelength, and may include light with wavelengths of, e.g., about 800-900 nm, 2200-1360 nm, 1360-1460 nm, 1530-1565 nm, or other suitable wavelengths. Light can also have TE or TM polarization.

In these and other implementations, the SiN waveguide in the Si PIC **102** may be aligned with and optically coupled to the Si waveguide in the Si PIC **102**. Additionally, the interposer waveguide in the interposer **104** may be aligned with and optically coupled to the SiN waveguide in the Si PIC **102**. The Si waveguide may have a first index of refraction  $n_1$ . The SiN waveguide may have a second index of refraction  $n_2$ . The interposer waveguide may have a third index of refraction  $n_3$ . In general, the second index of refraction  $n_2$  of the SiN waveguide may be intermediate between the first index of refraction  $n_1$  of the Si waveguide and the third index of refraction  $n_3$  of the interposer waveguide. In addition,  $n_1 > n_2 > n_3$ . In some embodiments, for a two-stage adiabatically coupled photonic system with three waveguides, each with a corresponding one of the indexes of refraction  $n_1$ ,  $n_2$ ,  $n_3$ , the first index of refraction  $n_1$  may be in a range of 3 to 3.5, the second index of refraction  $n_2$  may be in a range of 1.8 to 2.2, and the third index of refraction  $n_3$  may be in a range of 1.49 to 1.6.

The interposer waveguide in the interposer **104** may additionally be aligned with and optically coupled to an input and/or output for one or more optical signals. An example input source may include an optical signal source (e.g., a laser), an optical fiber, a fiber end connector, a lens, or other optical component or device from which incoming optical signals (e.g., signals coming toward the Si PIC **102**) are provided to the interposer **104** for input to the Si PIC **102**. An example output device to which output may be sent may include a laser, an optical receiver (e.g., a photodiode), an optical fiber, a fiber end connector, a lens, or other optical component or device to which outgoing signals (e.g., signals leaving the Si PIC **102**) may be provided through the interposer **104**. One or more of the active optical components of the Si PIC **102** may generate or otherwise be the source of outgoing signals that are outputted from the photonic system **200** through the Si waveguide, the SiN waveguide, and the interposer waveguide. Alternately or additionally, one or more of the active optical components of the Si PIC **102** may be configured to receive and process incoming signals that are inputted to the photonic system **200** through the interposer waveguide, the SiN waveguide, and the Si waveguide.

FIG. 2 is a side view of the photonic system **200** of FIG. 1, arranged in accordance with at least one embodiment described herein. The photonic system **200** includes the Si PIC **102** and the interposer **104**. FIG. 2 additionally illustrates the 3D stack region **106**.

The Si PIC **102** includes a Si substrate **202**, a SiO<sub>2</sub> box **204**, a first layer **206** that includes one or more SiN waveguides **208**, and a second layer **210** that includes one or more Si waveguides **212**. In the illustrated embodiment, the first and second layer **206** and **210** are both formed above the SiO<sub>2</sub> box **204**. In particular, the first layer **206** is formed on (or at least above) the second layer **210** and the second layer **210** is formed on (or at least above) the SiO<sub>2</sub> box **204**. Alternatively or additionally, a slab **214** of SiN may be formed between the



first layer **206** and the second layer **210** at least in a region where the Si waveguide **212** is optically coupled to the SiN waveguide **208**. In an example embodiment, the SiN waveguide **208** includes  $\text{Si}_3\text{N}_4$  as the waveguide core surrounded on at least two sides along its length by  $\text{SiO}_2$  or other suitable waveguide cladding.

Although not illustrated in FIG. 2, the Si PIC **102** may further include one or more active optical components formed in the second layer **210**. In these and other embodiments, the Si further include one or more dielectric layers **216** formed on and/or above the second layer **210**, and one or more metallized structures **218** formed in the dielectric layers **216**. The metallized structures **218** may extend from a top of the Si PIC **102** through the dielectric layers **216** to electrical contact with the active optical components formed in the second layer **210** or elsewhere in the Si PIC **102**. The dielectric layers **216** may include  $\text{SiO}_2$  or other suitable dielectric material. The dielectric layers **216** and the metallized structures **218** are collectively an example of the 3D stack region **106**.

With combined reference to FIGS. 1 and 2, the flip chip bonded IC **108** may be flip chip bonded to the 3D stack region **106**. The flip chip bonded IC may include one or more active and/or passive electrical devices that may be communicatively coupled through the 3D stack region **123** to the one or more active optical components formed in the second layer **210** of the Si PIC **102**.

The interposer **104** may include an interposer substrate **220** and a waveguide strip **222** formed on and/or coupled to the interposer substrate **220**. The waveguide strip **222** includes one or more interposer waveguides **224**. Each interposer waveguide **224** includes an interposer core **224A** and an interposer cladding **224B** of different indexes of refraction. A coupler portion of the interposer waveguide **224** may be disposed above a tapered end of the SiN waveguide **208** in the first layer **206** and is aligned with the tapered end of the SiN waveguide **208** as described in more detail below.

The Si waveguide **212** (or more particularly, the core of the Si waveguide **212**) may have the first index of refraction  $n_1$  mentioned above. The SiN waveguide **208** (or more particularly, the core of the SiN waveguide **208**) may have the second index of refraction  $n_2$  mentioned above. The interposer waveguide **224** (or more particularly, the interposer core **224A** of the interposer waveguide **224**) may have the third index of refraction  $n_3$  mentioned above, where  $n_1 > n_2 > n_3$ .

FIGS. 3A-3B include various views of portions of the photonic system **200** of FIG. 2, arranged in accordance with at least one embodiment described herein. In particular, FIG. 3A includes an overhead view **300A** and a longitudinal cross-sectional view **300B** and FIG. 3B includes transverse cross-sectional views **300C-300F** at locations respectively denoted by reference lines 1-4 in FIG. 3A.

The overhead view **300A** of FIG. 3A illustrates relative x-axis and z-axis alignment of various components with respect to each other according to an arbitrarily defined x-y-z coordinate axis provided within each of the views **300A-300B** of FIG. 3A and provided in other Figures herein. A single instance of the x-y-z coordinate axis is provided for all four views **300C-300F** of FIG. 3B since all four views **300C-300F** have the same orientation. The x direction may sometimes be referred to as a lateral or transverse direction and terms such as width, lateral, transverse, side, sideways etc. may be used to refer to, e.g., dimensions, relative position, and/or movement in the x direction unless context dictates otherwise. The y direction may sometimes be referred to as a vertical direction and terms such as height, thickness, vertical, vertically, above, below, up, down, etc. may be used to refer to, e.g., dimensions, relative position, and/or movement

in the y direction unless context dictates otherwise. The z direction may sometimes be referred to as a longitudinal or light-propagating direction and terms such as length, longitudinal, upstream, downstream, forward, backward, front, back, etc. may be used to refer to, e.g., dimensions, relative position, and/or movement in the z direction unless context dictates otherwise.

The longitudinal cross-sectional view **300B** of FIG. 3A illustrates an example material stack up for the various components. The overhead view **300A** of FIG. 3A includes outlines or footprints of the various components at different levels in the material stack up that may not necessarily be visible when viewed from above, but are shown as outlines or footprints to illustrate the x and z alignment of the various components with respect to each other.

The portion of the photonic system **200** illustrated in the view **300A** of FIG. 3A includes a tapered end of the Si waveguide **212**. The tapered end of the Si waveguide **212** is relatively wider at reference line 1 than at reference line 2. The tapered end of the Si waveguide **212** may be considered to have a taper or an inverse taper, which are structurally equivalent. As used herein, a waveguide such as the Si waveguide **212** of FIG. 3A may be considered to have a taper with respect to incoming optical signals, e.g., optical signals that enter the waveguide at a relatively narrower portion of the waveguide and propagate through the waveguide towards a relatively wider portion of the waveguide. In comparison, a waveguide such as the Si waveguide **212** of FIG. 3A may be considered to have an inverse taper with respect to outgoing optical signals, e.g., optical signals that propagate through the waveguide in the direction from wider to narrower to exit the waveguide. For simplicity in the discussion that follows, the term "taper" and its variants should be broadly construed as a variation of the waveguide width along the optical axis. In some embodiments, it may be advantageous to vary the width of the waveguide along the optical axis linearly or nonlinearly or in segments of linear and nonlinear variation. The width of the taper around the interaction region of the initial state and final state waveguides may be varied to optimize coupling or reduce the length of the coupling region to produce a physically smaller device.

The Si waveguide **212**, including the tapered end, may be formed in the second layer **210** and positioned below the first layer **206** that includes the SiN waveguide **208**. For example, the second layer **210** may be positioned below the SiN slab **214**, which in turn is positioned below the first layer **206**. Within the second layer **210**,  $\text{SiO}_2$  may generally be disposed adjacent to sides of the Si waveguide **212** (e.g., in the positive x and negative x directions), as illustrated in the views **300C** and **300D** of FIG. 3B, to form a cladding for the Si waveguide **212**, which serves as the core. In some embodiments, the Si waveguide **212** and/or other Si waveguides of the Si PIC **102** may have a thickness  $t_{\text{Si}}$  (e.g., in the y direction) of approximately 0.3  $\mu\text{m}$  and an index of refraction of about 3.4. The specific values of indexes of refraction, thickness, width, length, and other values provided herein are provided by way of example only and values other than those explicitly stated may nevertheless fall within the scope of the described embodiments.

As illustrated in FIG. 3A, the SiN slab **214** may be formed or otherwise located on the second layer **210** that includes the Si waveguide **212**. The SiN slab **214** may have a thickness (e.g., in the y direction) of approximately 0-50 nm in some embodiments.

The view **300B** of FIG. 3A further illustrates the SiN waveguide **208**. The SiN waveguide **208** includes both a coupler portion and a tapered end. The coupler portion of the

11

SiN waveguide **208** generally includes the portion of the SiN waveguide **208** between reference lines **1** and **2** and the tapered end of the SiN waveguide **208** generally includes the portion of the SiN waveguide **208** between reference lines **3** and **4**. The tapered end of the SiN waveguide **208** is relatively wider at reference line **3** than at reference line **4**. Within the first layer **206**, SiO<sub>2</sub> may generally be disposed adjacent to sides of the SiN waveguide **208** (e.g., in the positive x and negative x directions), to serve as a cladding layer for the SiN waveguide **208**, as illustrated in the views **300C-300F** of FIG. **3B**. In some embodiments, the SiN waveguide **208** and/or other SiN waveguides of the first layer **206** may have a thickness (e.g., in the z direction) of approximately 0.5-1  $\mu\text{m}$  and an index of refraction of about 1.99.

It can be seen from FIG. **3A** that, although the SiN waveguide **208** is displaced in the y direction from the Si waveguide **212**, the tapered end of the Si waveguide **212** is aligned in the x and z directions with the coupler portion of the SiN waveguide **208** such that the tapered end of the Si waveguide **212** overlaps the coupler portion of the SiN waveguide **208** (as seen in the view **300A**) in the x and z directions and is parallel thereto (as seen in the view **300B**).

FIG. **3A** additionally illustrates the interposer waveguide **224**. The interposer waveguide **224** includes the core **224A** and cladding **224B**. Additionally, the interposer waveguide **224** includes both a coupler portion and an end that extends from the coupler portion. The coupler portion of the interposer waveguide **224** generally includes the portion of the interposer waveguide **224** between reference lines **3** and **4** and the end extends away from the coupler portion (e.g., to the right in FIG. **3A**). The interposer waveguide **224** may be coupled, along with potentially one or more other interposer waveguides, to the interposer substrate **220** of FIG. **2**. In some embodiments, the interposer waveguide **224** and/or other interposer waveguides of the interposer **104** of FIG. **2** may have a thickness  $t_i$  (e.g., in the y direction) of approximately 3  $\mu\text{m}$ , a width  $w_1$  (e.g., in the x direction) of about 4  $\mu\text{m}$ , and an index of refraction of about 1.51 for the interposer core **224A** and about 1.5 for the interposer cladding **224B**. More generally, provided the index of refraction of the interposer core **224A** is greater than that of the interposer cladding **224B**, the interposer core **224A** may have an index of refraction in a range from 1.509 to 1.52. Note that the low end of the range of refractive index for the interposer is determined by the minimum taper tip width afforded by the SiN fabrication process, which here is assumed to be on the order of 200 nm. For instance, the minimum taper tip width for SiN waveguides may be 180 nm. If the process allows for a smaller tip width for the SiN, a correspondingly lower refractive index for the interposer will be allowed. This is because adiabatic coupling transition occurs when the effective indices of the SiN waveguide and interposer waveguide are substantially the same. Decreasing the SiN tip width (by using a more sophisticated process, for example) reduces the effective index of the SiN waveguide allowing a lower material index for the interposer.

It can be seen from FIG. **3A** that, although the interposer waveguide **224** is displaced in the y direction from the SiN waveguide **208**, the coupler portion of the interposer waveguide **224** is nevertheless aligned in the x and z directions with the tapered end of the SiN waveguide **208** such that the coupler portion of the interposer waveguide **224** overlaps the tapered end of the SiN waveguide **208** (as seen in the view **300A**) and is parallel thereto (as seen in the view **300B**).

The views **300C-300F** of FIG. **3B** depict widths (e.g., in the x direction) of the tapered end of each of the Si waveguide **212** and the SiN waveguide **208** at, respectively, reference lines

12

**1-4** of FIG. **3A**. For instance, from the views **300C** and **300D**, it can be seen that a width of the Si waveguide **212** tapers from a width  $w_{Si1}$  of about 0.32  $\mu\text{m}$  at reference line **1** to a width  $w_{Si2}$  of about 0.08  $\mu\text{m}$  (or 80 nm) at reference line **2**. Also, from the views **300E** and **300F**, it can be seen that a width of the SiN waveguide **208** tapers from width  $w_{SiN1}$  of about 1.0  $\mu\text{m}$  at reference line **3** to width  $w_{SiN2}$  of about 0.20  $\mu\text{m}$  (or 200 nm) at reference line **4**. As another design example, the width  $w_{SiN1}$  can be about 1.5  $\mu\text{m}$  at reference line **3** tapered to the width  $w_{SiN2}$  of about 0.08  $\mu\text{m}$  at reference line **4**.

The tapered ends of the Si waveguide **212** and the SiN waveguide **208** provide adiabatic transitions for optical signals from the Si waveguide **212** to the SiN waveguide **208** and from the SiN waveguide **208** to the interposer waveguide **224**, or adiabatic transitions for optical signals traveling in the opposite direction. An adiabatic transition may be achieved by changing the structure and/or an effective index of the tapered ends of the Si and SiN waveguides **212** and **208** in a sufficiently slow manner so light is not scattered from its mode when it is incident on the tapered ends and continues propagating in this same mode when it exits the tapered ends and enters the coupler portion of the SiN waveguide **208** or the interposer waveguide **224**. That is, the light may experience a gradual transition between the tapered end of the Si or SiN waveguide **212** or **208** and the y-axis displaced and adjacent coupler portion of the SiN or interposer waveguide **208** or **224** such that the mode does not change and no significant scattering of light takes place. Accordingly, the tapered end of the Si waveguide **212** combined with the coupler portion of the SiN waveguide **208** is an example of an adiabatic coupler region. The tapered end of the SiN waveguide **208** and the coupler portion of the interposer waveguide **224** is another example of an adiabatic coupler region.

In operation, the structure, refractive index, and/or other characteristics of an optical medium may determine an effective index of the optical medium. Effective index is somewhat analogous to energy levels in quantum mechanics. Higher effective index is analogous to lower energy level. Thus, for two adjacent optical media with different effective indexes, light tends to propagate through the medium with the higher effective index.

In the embodiments described herein, and with particular reference to FIGS. **3A** and **3B**, Si waveguides may generally have a higher effective index than SiN waveguides, and SiN waveguides may generally have a higher effective index than polymer waveguides. By tapering the end of a Si waveguide, the effective index may be reduced along the length of the tapered end until the effective index of the Si waveguide approximately matches or even becomes smaller than the effective index of a y-axis displaced SiN waveguide, such as illustrated in FIGS. **3A** and **3B**. Accordingly, light propagating through the Si waveguide **212** and exiting through its tapered end may exit the tapered end of the Si waveguide **212** and enter the SiN waveguide **208** about at a point where the effective index of the tapered end of the Si waveguide **212** matches an effective index of the SiN waveguide **208**. Analogously, the SiN waveguide **208** may be tapered at its end until its effective index approximately matches or even becomes smaller than the effective index of a y-axis displaced polymer waveguide, such as illustrated in FIGS. **3A** and **3B**. Accordingly, light propagating through the SiN waveguide **208** and exiting through its tapered end may exit the tapered end of the SiN waveguide **208** and enter the interposer waveguide **224** about at a point where the effective index of the tapered end of the SiN waveguide **208** matches an effective index of the interposer waveguide **224**.

Some other adiabatic coupling systems include a single adiabatic coupler region or stage in which a polymer or high index glass (or other interposer) waveguide receives light directly from a tapered end of a Si waveguide. Such systems generally require a Si waveguide that is very thin (e.g., 190-200 nm thick in the y direction of FIGS. 3A-3B) and/or tapering the Si waveguide to a very thin width (e.g., 40 nm wide in the x direction) to reach an effective index small enough to match the effective index of the polymer or high index glass waveguide. Such fine dimensions may not be achievable for some fabs/manufacturers and/or may be inconsistent with existing processes of these fabs/manufacturers. In addition, smaller Si waveguides generally have higher insertion loss than relatively larger Si waveguides, making them disadvantageous. The adiabatic coupling length between Si and Polymer waveguides may be on the order of 2 mm, over which such a narrow Si waveguide would introduce unwanted optical loss. In comparison, some embodiments described herein implement a two-stage adiabatic coupling where the SiN waveguide has an intermediate index of refraction between that of the Si waveguide and of the interposer waveguide, such that the effective index of the Si waveguide may be matched to the effective index of the SiN waveguide by fabricating the SiN waveguide and/or its tapered end with larger dimensions that are achievable by the fabs/manufacturers and that allow the use of a larger, lower loss SiN waveguide. Here, the adiabatic coupling length from the Si waveguide to the SiN waveguide may be quite small, e.g., about 50-200  $\mu\text{m}$ . In this case the higher loss of the small 80 nm wide Si waveguide does not introduce significant loss and the loss is significantly less than the narrower Si waveguide over 2 mm as described above. The adiabatic coupler region between the SiN waveguide and the interposer waveguide may be around 2 mm, where the lower loss of the SiN waveguide relative to the Si waveguide leads to less loss as compared with direct adiabatic coupling between Si and interposer waveguides.

FIG. 4 includes a graphical representation of simulated coupling efficiency of TM polarized light from the Si waveguide 212 to the SiN waveguide 208 of FIGS. 3A-3B, arranged in accordance with at least one embodiment described herein. The horizontal axis of FIG. 4 is height or thickness  $t_{\text{SiN}}$  (e.g., in the y direction of FIGS. 3A-3B) of the SiN waveguide 208 and the vertical axis is the coupling efficiency. It can be seen from FIG. 4 that the coupling efficiency increases with increasing height or thickness  $t_{\text{SiN}}$  of the SiN waveguide 208. At a height or thickness  $t_{\text{SiN}}$  of 1  $\mu\text{m}$ , the coupling efficiency is approximately 96% for the TM polarized light.

FIGS. 5A-5B include graphical representations of simulated light modes of TM and TE polarized light in the SiN waveguide 208 of FIGS. 3A-3B at reference line 2, arranged in accordance with at least one embodiment described herein. For the simulations of FIGS. 5A-5B, the SiN waveguide 208 is assumed to have a height or thickness  $t_{\text{SiN}}$  (e.g., in the y direction) of about 1  $\mu\text{m}$  and a width  $w_{\text{SiN1}}$  (e.g., in the x direction) of about 1.5  $\mu\text{m}$ .

As illustrated in FIG. 5A, at reference line 2 in FIGS. 3A-3B, most of the TM polarized light has moved into the SiN waveguide 208, although some still remains in the tip of the tapered end of the Si waveguide 212. As illustrated in FIG. 5B, at reference line 2 in FIGS. 3A-3B, virtually all of the TE polarized light has moved out of the Si waveguide 212 and into the SiN waveguide 208.

FIGS. 5A-5B further illustrate the light as a single mode of light. However, SiN waveguides 208 may in some cases support multimode light. When single mode light is coupled

adiabatically from the Si waveguide 212 to the SiN waveguide 208, only the single mode of the SiN waveguide 208 may be excited and the light may stay in the single mode in some embodiments. In other embodiments, a Si—SiN adiabatic coupler region may be configured to support transmission therebetween multimodes of light, as discussed below. In other embodiments, the SiN waveguide may be configured to support only the single mode.

FIG. 6 includes a graphical representation of simulated coupling efficiency of TM polarized light and TE polarized light (respectively labeled “TM” and “TE” in FIG. 6) from the SiN waveguide 208 to the interposer waveguide 224 of FIGS. 3A-3B, arranged in accordance with at least one embodiment described herein. The horizontal axis of FIG. 6 is length (e.g., in the z direction of FIGS. 3A-3B) of the tapered end of the SiN waveguide 208 and the vertical axis is the coupling efficiency. It can be seen from FIG. 6 that the coupling efficiency is generally better for TE polarized light and increases for both TE and TM polarized light with increasing length of the tapered end of the SiN waveguide 208.

FIG. 7 is a side view of another example two-stage adiabatically coupled photonic system 700 (hereinafter “photonic system 700”), arranged in accordance with at least one embodiment described herein. The photonic system 700 includes a Si PIC 702 and an interposer 704. Similar to the photonic system 200, the photonic system 700 may generally be configured to adiabatically couple light into and/or out of the photonic system 700.

The Si PIC 702 includes a Si substrate 706, a SiO<sub>2</sub> box 708, a first layer 710 that includes a SiN waveguide 712, and a second layer 714 that includes a Si waveguide 716. In the illustrated embodiment, the first layer 710 is formed on (or at least above) the SiO<sub>2</sub> box 708 and the second layer 714 is formed on (or at least above) the first layer 710. Alternatively or additionally, a slab 718 of SiN may be formed between the first layer 710 and the second layer 714 at least in a region where the Si waveguide 716 is optically coupled to the SiN waveguide 712. In an example embodiment, the SiN waveguide 712 includes Si<sub>3</sub>N<sub>4</sub> as the waveguide core surrounded on at least two sides along its length by SiO<sub>2</sub> or other suitable waveguide cladding.

As illustrated in FIG. 7, the Si PIC 702 may further include one or more active optical components 720 formed in the second layer 714, one or more dielectric layers 722 formed on and/or above the second layer 714, and one or more metallized structures 724 formed in the dielectric layers 722. The metallized structures 724 may extend from a top of the Si PIC 702 through the dielectric layers 722 to electrical contact with the active optical components 720. The dielectric layers 722 may include SiO<sub>2</sub> or other suitable dielectric material. The dielectric layers 722 and the metallized structures 724 are collectively an example of a 3D stack region that may be included in Si PICs, such as the Si PIC 702 of FIG. 7. Alternatively or additionally, the region of the Si PIC 702 that includes the active optical components 720 may be referred to as an active region of the Si PIC 702 (labeled “Actives” in FIG. 7), whereas a region or regions of the Si PIC 702 that lack such active optical components 720 may be referred to as a passive region of the Si PIC 702 (labeled “Passives” in FIG. 7).

The Si PIC 702 may define an etched window 725 through the layers of the Si PIC 702 down to the first layer 710, including through the dielectric layers 722, the second layer 714, and the SiN slab 718 in the example of FIG. 7.

The interposer 704 may include an interposer substrate 726 and a waveguide strip 728 formed on and/or coupled to the polymer substrate. The waveguide strip 728 includes one or

15

more interposer waveguides **730**. Each of the interposer waveguides **730** includes an interposer core and interposer cladding of different indices of refraction. A coupler portion of each interposer waveguide **730** is disposed above a tapered end of each SiN waveguide **712** within the etched window **725** of the Si PIC **702** and is aligned with the tapered end of the corresponding SiN waveguide **712** as described in more detail below.

Each of the Si PIC **702**, the interposer **704**, the Si substrate **706**, the SiO<sub>2</sub> box **708**, the first layer **710**, the SiN waveguide **712**, the second layer **714**, the Si waveguide **716**, the SiN slab **718**, the active optical components **720**, the dielectric layers **722**, the metallized structures **724**, the interposer substrate **726**, the waveguide strip **728**, and the interposer waveguide **730** of FIG. 7 may generally be similar or identical to, respectively, any of the other Si PICs, interposers, Si substrates, SiO<sub>2</sub> boxes, first layers, SiN waveguides, second layers, Si waveguides, SiN slabs, active optical components, dielectric layers, metallized structures, interposer substrates, waveguide strips, and interposer waveguides disclosed herein, excepted as otherwise indicated herein.

FIGS. 8A-8B include various views of portions of the photonic system **700** of FIG. 7, arranged in accordance with at least one embodiment described herein. In particular, FIG. 8A includes an overhead view **800A** and a longitudinal cross-sectional view **800B** and FIG. 8B includes transverse cross-sectional views **800C-800F** at locations respectively denoted by reference lines 1-4 in FIG. 8A.

The overhead view **800A** of FIG. 8A illustrates relative x-axis and z-axis alignment of various components with respect to each other. The longitudinal cross-sectional view **800B** of FIG. 8A illustrates an example material stackup for the various components. The overhead view **800A** of FIG. 8A includes outlines or footprints of the various components at different levels in the material stackup that may not necessarily be visible when viewed from above, but are shown as outlines or footprints to illustrate the x and z alignment of the various components with respect to each other.

The portion of the photonic system **700** illustrated in the view **800A** of FIG. 8A includes a tapered end of the Si waveguide **716**. The tapered end of the Si waveguide **716** is relatively wider at reference line **1** than at reference line **2**. The Si waveguide **716**, including the tapered end, may be formed in the second layer **714** (FIG. 7) on or above the first layer **710** (FIG. 7) that includes the SiN waveguide **712**. For example, the second layer **714** may be formed on the SiN slab **718** above the first layer **710**. Within the second layer **714**, SiO<sub>2</sub> may generally be disposed adjacent to sides of the Si waveguide **716** (e.g., in the positive x and negative x directions), as illustrated in the views **800C** and **800D** of FIG. 8B, to form a cladding for the Si waveguide **716**, which serves as the core. The thickness and/or index of refraction of the Si waveguide **716** may be the same as or different than the thickness and/or index of refraction of the Si waveguide **212** described above.

As illustrated in FIG. 8A, the SiN slab **718** may be formed or otherwise located on the first layer **710** (FIG. 7) that includes the SiN waveguide **712**. The SiN slab **718** may have a thickness that is the same as or different than the thickness of the SiN slab **214** described above.

The view **800B** of FIG. 8A further illustrates the SiN waveguide **712**. The SiN waveguide **712** includes both a coupler portion and a tapered end. The coupler portion of the SiN waveguide **712** generally includes the portion of the SiN waveguide **712** between reference lines **1** and **2** and the tapered end of the SiN waveguide **712** generally includes the portion of the SiN waveguide **712** between reference lines **3**

16

and **4**. The tapered end of the SiN waveguide **712** is relatively wider at reference line **3** than at reference line **4**. Within the first layer **710** (FIG. 7), SiO<sub>2</sub> may generally be disposed adjacent to sides of the SiN waveguide **712**, to serve as a cladding layer for the SiN waveguide **712** (e.g., in the positive x and negative x directions), as illustrated in the views **800C-800F** of FIG. 8B. The SiN waveguide **712** and/or other SiN waveguides of the first layer **710** may have a thickness (e.g., in the y direction) and/or index of refraction that is the same as or different than the thickness and/or index of refraction of the SiN waveguide **208** described above.

It can be seen from FIG. 8A that, although the SiN waveguide **712** is displaced in the y direction from the Si waveguide **716**, the tapered end of the Si waveguide **716** is aligned in the x and z directions with the coupler portion of the SiN waveguide **712** such that the tapered end of the Si waveguide **716** overlaps the coupler portion of the SiN waveguide **712** (as seen in the view **800A**) in the x and z directions and is parallel thereto (as seen in the view **800B**).

FIG. 8A additionally illustrates the interposer waveguide **730**. The interposer waveguide **730** includes an interposer core **730A** and an interposer cladding **730B**. Additionally, the interposer waveguide **730** includes both a coupler portion and an end that extends from the coupler portion. The coupler portion of the interposer waveguide **730** generally includes the portion of the interposer waveguide **730** between reference lines **3** and **4** and the end extends away from the coupler portion (e.g., to the right in FIG. 8A). The interposer waveguide **730** may be coupled, along with potentially one or more other interposer waveguides, to the interposer substrate **726** of FIG. 7. In some embodiments, the interposer waveguide **730** and/or other interposer waveguides of the interposer **704** of FIG. 7 may have a thickness (e.g., in the y direction), a width (e.g., in the x direction) and/or an index of refraction that is the same as or different than the thickness, width, and/or index of refraction of the interposer waveguide **224** described above.

It can be seen from FIG. 8A that, although the interposer waveguide **730** is displaced in the y direction from the SiN waveguide **712**, the coupler portion of the interposer waveguide **730** is nevertheless aligned in the x and z directions with the tapered end of the SiN waveguide **712** such that the coupler portion of the interposer waveguide **730** overlaps the tapered end of the SiN waveguide **712** (as seen in the view **800A**) and is parallel thereto (as seen in the view **800B**).

The Si waveguide **716**, the SiN waveguide **712**, tapered ends thereof, and/or the interposer waveguide **730** may have widths (e.g., in the x direction) and/or lengths (e.g., in the z direction) that are the same as or different than the widths and/or lengths of the Si waveguide **212**, the SiN waveguide **208**, tapered ends thereof, and/or the interposer waveguide **224** described above. Alternatively or additionally, the tapered ends of the Si waveguide **716** and the SiN waveguide **712** may provide adiabatic transitions for optical signals from the Si waveguide **716** to the SiN waveguide **712** and from the SiN waveguide **712** to the interposer waveguide **730**, as described above with respect to the Si waveguide **212**, the SiN waveguide **208**, and the interposer waveguide **224**.

FIG. 9 is a side view of another example two-stage adiabatically coupled photonic system **900** (hereinafter “photonic system **900**”), arranged in accordance with at least one embodiment described herein. The photonic system **900** is similar in many respects to the photonic system **700** discussed above, and includes a Si PIC **902** and the interposer **704**. The Si PIC **902** is similar in many respects to the Si PIC **702** discussed above, and includes, for example, the SiO<sub>2</sub> box **708**, the second layer **714**, the Si waveguide **716**, the active optical

components **720**, the dielectric layers **722**, and the metallized structures **724**, and the Si PIC **902** additionally defines an etched window **925**.

The Si PIC **902** additionally includes a first layer **910** that is similar to the first layer **710** of FIG. 7. In particular, the first layer **910** includes a first SiN waveguide **912A** with a coupler portion that is similar to the SiN waveguide **712** with coupler portion discussed above. In particular, the tapered end of the Si waveguide **716** and the coupler portion of the first SiN waveguide **912A** are aligned with each other as described with respect to the Si waveguide **716** and the SiN waveguide **712** so as to adiabatically couple light from the Si waveguide **716** to the first SiN waveguide **912A**, or vice versa.

The first layer **910** of the Si PIC **902** additionally includes a WDM component, generally designated at **914**. The WDM component **914** may function as a WDM mux or WDM demux, for instance. The WDM component **914** may include one or more cascaded Mach-Zehnders, Echelle gratings, or arrayed waveguide gratings (AWGs). The WDM component **914** optically couples the first SiN waveguide **912A** to one or more second SiN waveguides **912B**, **912C** according to the wavelength of light. Alternatively or additionally, the WDM component **914** may optically couple one or each of the second SiN waveguides **912B**, **912C** that can be carrying optical signals having different wavelength to one or more first SiN waveguides **912A** that are in turn coupled to one or more Si waveguides **716**. The second SiN waveguide **912C** may include a tapered end to adiabatically couple light into the interposer waveguide **730**, as described with respect to the SiN waveguide **712** and the interposer waveguide **730** above.

To reduce and/or eliminate polarization dependence of the WDM component **914**, one or more of the first and second SiN waveguides **912A-912C** (generically hereinafter “SiN waveguide **912**” or “SiN waveguides **912**”) may have the same effective index and group index for TE and TM polarizations of light. To configure the SiN waveguide **912** with the same effective index and group index for TE and TM polarizations of light, the SiN waveguide **912** may be provided with a symmetric square cross-section and may generally be surrounded by SiO<sub>2</sub>.

For example, in FIG. 9, at least the SiN waveguide **912B** may have a square cross-section along its length, or along at least a portion thereof. The square cross-section along at least a portion of the length of the SiN waveguide **912B** may be about 500 nm by about 500 nm. Laterally, the SiN waveguide **912B** may have SiO<sub>2</sub> adjacent thereto. In the vertical direction (e.g., the y direction), the SiN waveguide **912B** may have the SiO<sub>2</sub> box **708** or another layer of SiO<sub>2</sub> beneath and adjacent thereto, where the SiO<sub>2</sub> box **708** or other layer of SiO<sub>2</sub> has a thickness of at least 200 nm. Further, the SiN waveguide **912B** may have one or more layers of SiO<sub>2</sub> above and adjacent thereto, such as the second layer **714** and/or the dielectric layers **722**. The one or more layers of SiO<sub>2</sub> that are above and adjacent to the SiN waveguide **912B** in FIG. 9 may have an aggregate thickness greater than 330 nm.

FIG. 10 includes various simulations **1000A-1000C** associated with the embodiment of FIG. 9, arranged in accordance with at least one embodiment described herein. The simulation **1000C** depicts effective index/group index of the SiN waveguide **912B** of FIG. 9 as a function of width of the SiN waveguide **912B** where it is assumed that the SiN waveguide **912B** has a thickness of 500 nm. In the simulation **1000C**, curves **1002A** and **1002B** represent the group index of the SiN waveguide **912B** for, respectively, the TE and TM polarizations of light, while curves **1004A** and **1004B** represent the effective index of the SiN waveguide **912B** for, respectively, the TE and TM polarizations of light. It can be seen from the

simulation **1000C** that the same group index and effective index for the TE and TM polarizations of light occurs at 500 nm, e.g., where the width of the SiN waveguide **912B** is equal to the 500 nm thickness. This may result in zero birefringence operation.

FIG. 10 additionally includes a table **1006** that lists the 500 nm by 500 nm cross-sectional measurement of the SiN waveguide **912B** determined from the simulation **1000C**, as well as indexes of refraction of the SiN and SiO<sub>2</sub> used in the SiN waveguide.

The simulations **1000A** and **1000B** of FIG. 10 assume the parameters listed in the table **1004**. It can be seen from the simulations **1000A** and **1000B** that zero birefringence operation occurs for the 500 nm by 500 nm SiN waveguide **912B** surrounded by SiO<sub>2</sub> on all four sides along the length of the SiN waveguide **912B**.

FIG. 11 is a side view of another example two-stage adiabatically coupled photonic system **1100** (hereinafter “photonic system **1100**”), arranged in accordance with at least one embodiment described herein. The photonic system **1100** is similar in many respects to the photonic system **900** discussed above and includes, inter alia, the interposer **704** and an Si PIC **1102** with the SiO<sub>2</sub> box **708**, a first layer **1110** that includes one or more SiN waveguides **1112A-1112C** (hereinafter “SiN waveguide **1112**” or “SiN waveguides **1112**”) and a WDM component **1113**, a second layer **1114** that includes one or more Si waveguides **1116**, one or more dielectric layers **1122**, and metallization structures **1124**. The first layer **1110**, SiN waveguide **1112**, WDM component **1113**, second layer **1114**, Si waveguide **1116**, dielectric layers **1122**, and metallization structures **1124** may generally be similar or identical to, respectively, any of the other first layers, SiN waveguides, WDM components, second layers, Si waveguides, dielectric layers, and metallization structures disclosed herein except as otherwise indicated herein.

One difference between the photonic system **1100** and, e.g., the photonic system **900** is that the first and second layers **1110** and **1114** of the Si PIC **1102** of FIG. 11 are switched compared to the first and second layers **910** and **714** of the Si PIC **902** of FIG. 9. In particular, in FIG. 11, the second layer **1114** that includes the Si waveguide **1116** is below the first layer **1110** that includes the SiN waveguides **1112**. The dielectric layers **1122** may be disposed above and in contact with the first layer **1110** and may have a thickness greater than 800 nm. The second layer **1114** may be disposed beneath and in contact with the first layer **1110** and may have a thickness greater than 330 nm.

The Si PIC **1102** may otherwise generally be similar to the Si PIC **902** of FIG. 9. For example, light may be adiabatically coupled from the Si waveguide **1116** to the SiN waveguide **1112A**, or vice versa, and from the SiN waveguide **1112C** to the interposer waveguide **730**, or vice versa, in a similar manner as described above. Additionally, the SiN waveguide **1112B** may have the same effective index and group index for TE and TM polarizations of light.

FIGS. **12A** and **12B** include an overhead view and a longitudinal cross-sectional view of another example optoelectronic system **1200** (hereinafter “system **1200**”) that includes two adiabatic coupler regions made up of the Si waveguide **212**, the SiN waveguide **208**, and the interposer waveguide **224** of FIGS. 3A-3B, arranged in accordance with at least one embodiment described herein.

The system **1200** further includes a distributed feedback (DFB) laser **1202** or other semiconductor laser, a first lens **1204**, an optical isolator **1206**, and a second lens **1208**, all mounted to a laser sub-mount **1210**. The first lens **1204** may be positioned in an optical path of an optical signal output

19

from the DFB laser **1202**. The optical isolator **1206** may be positioned in the optical path after the first lens **1204**. The second lens **1208** may be positioned in the optical path after the optical isolator **1206**. As illustrated, an end of the interposer waveguide **224** may be positioned in the optical path after the second lens **1208**.

FIG. **13** is an overhead view of another example optoelectronic system **1300** (hereinafter “system **1300**”), arranged in accordance with at least some embodiments described herein. The system **1300** includes  $N$  ( $N \geq 2$ ) DFB lasers **1302A-1302D** configured to emit optical signals of different wavelengths  $\lambda_1$ - $\lambda_N$ , where  $N$  is 4 in the example of FIG. **13**. Each of the DFB lasers **1302A-1302D** is optically coupled to a corresponding interposer waveguide **1304A-1304D** through a corresponding first lens **1306A-1306D**, a corresponding optical isolator **1308A-1308D**, and a corresponding second lens **1310A-1310D** as described with respect to FIGS. **12A-12B**.

The output of each of the DFB lasers **1302A-1302D** is received by a corresponding one of the interposer waveguides **1304A-1304D** (each made up of an interposer core and interposer cladding and formed on an interposer substrate) and is adiabatically coupled from the corresponding interposer waveguide **1304A-1304D** into a corresponding SiN waveguide **1312A-1312D** included in a first layer of a Si PIC included in the system **1300** of FIG. **13**. The Si PIC of the system **1300** may be similar or identical to one or more of the other Si PICs described herein. The adiabatic coupling is accomplished as described above, e.g., by providing the SiN waveguides **1312A-1312D** with tapered ends that are aligned in two orthogonal dimensions with a corresponding coupler portion of the corresponding interposer waveguides **1304A-1304D**. Rather than each of the SiN waveguides **1312A-1312D** adiabatically coupling a corresponding one of  $N$  optical signals output by the  $N$  DFB lasers **1302A-1302D** immediately into a corresponding Si waveguide in a second layer of the Si PIC that is vertically displaced above or below the first layer, the SiN waveguides **1312A-1312D** are optically coupled within the first layer of the Si PIC to a passive optical device **1314** included in the first layer of the Si PIC of FIG. **13**.

In the example of FIG. **13**, the passive optical device **1314** includes a WDM component such as a WDM mux. The WDM mux may include a cascade of Mach-Zehnder (MZ) interferometers, an arrayed waveguide grating (AWG), an Echelle grating, or other suitable WDM mux. More generally, the passive optical device **1314** may include any passive optical device suitable for formation in SiN.

The  $N$  optical signals output by the  $N$  DFB lasers **1302A-1302D** are directed by the SiN waveguides **1312A-1312D** into the passive optical device **1314**. The passive optical device **1314** multiplexes the  $N$  optical signals into a multiplexed optical signal output to a common SiN output waveguide **1316** included in the first layer of the Si PIC of FIG. **13**. The common SiN output waveguide **1316** may be configured similar or identical to other SiN waveguides described herein. The multiplexed optical signal is adiabatically coupled from the common SiN output waveguide **1316** into a Si waveguide **1318** formed in the second layer of the Si PIC. The adiabatic coupling is accomplished as described above, e.g., by providing the Si waveguide **1318** with a tapered end that is aligned in the two orthogonal dimensions with a coupler portion of the common SiN output waveguide **1316**.

FIG. **14** is an overhead view of an example AWG **1400** that may be formed as a passive optical device such as a WDM component (e.g., a WDM mux or WDM demux) using SiN in,

20

e.g., the first layers **206**, **710**, **910**, **1110** of the Si PICs **102**, **702**, **902**, **1102**, arranged in accordance with at least one embodiment described herein. The first layer of the Si PIC may include a SiN waveguide **1402**, the AWG **1400**, and SiN waveguides **1404A-1404D**. An interposer waveguide **1406** of an interposer forms an adiabatic coupler region with the SiN waveguide **1402**. A Si waveguide **1408A** formed in a second layer of the Si PIC forms an adiabatic coupler region with the SiN waveguide **1404A**. Although not illustrated in FIG. **14**, other Si waveguides formed in the second layer of the Si PIC may form adiabatic coupler regions with the other SiN waveguides **1404B-1404D**.

In some embodiments, the AWG **1400** is a WDM demux, in which case a multiplexed optical signal is adiabatically coupled from the interposer waveguide **1406** into the SiN waveguide **1402** and provided to the AWG **1400**, which demultiplexes the multiplexed optical signal into multiple output signals (e.g., separate wavelength channels) separately output to the SiN waveguides **1404A-1404D**. Each of the output signals may then be adiabatically coupled from the corresponding SiN waveguide **1404A-1404D** into a corresponding Si waveguide, such as the Si waveguide **1408A** in the case of the SiN waveguide **1404A**.

In some embodiments, the AWG **1400** is a WDM mux, in which case a different one of multiple input signals (e.g., separate wavelength channels) is adiabatically coupled from a corresponding Si waveguide, such as the Si waveguide **1408A** or other Si waveguides of the Si PIC, into a corresponding SiN waveguide **1404A-1404D**. The SiN waveguides **1404A-1404D** provide their respective input signal to the AWG **1400**, which multiplexes the various input signals into a multiplexed optical signal output to the SiN waveguide **1402**. The multiplexed optical signal may then be adiabatically coupled from the SiN waveguide **1402** to the interposer waveguide **1406**.

In FIG. **14** (and in FIG. **13**), each of the SiN waveguides **1402** and **1404A-1404D** may taper down from a relatively wide SiN waveguide to a relatively narrow SiN waveguide whose effective indexes for TE and TM are the same. Accordingly, the SiN-based AWG **1400** of FIG. **14** may be based on a zero-birefringent SiN waveguide.

FIG. **15** is an overhead view of an example cascade of MZ interferometers **1500** that may be formed as a passive optical device such as a WDM component (e.g., a WDM mux) using SiN in, e.g., the first layers **206**, **710**, **910**, **1110** of the Si PICs **102**, **702**, **902**, **1102**, arranged in accordance with at least one embodiment described herein. The cascade of MZ interferometers **1500** may include or correspond to the passive optical device **1314** of FIG. **13**. Although the cascade MZ interferometer **1500** of FIG. **15** is illustrated as a WDM mux that accepts  $N$  ( $N \geq 2$ ) input optical signals and outputs one multiplexed optical signal, the cascade MZ interferometer **1500** may instead be implemented as a WDM demux that accepts one multiplexed optical signal and outputs  $N$  individual optical signals.

The cascade of MZ interferometers **1500** may include a first stage **1502** of MZ interferometers with a delay in one arm of each of the MZ interferometers of the first stage **1502** of  $\Delta L$ , a second stage **1504** of MZ interferometers with a delay in one arm of each of the MZ interferometers of the second stage **1504** of  $2 \cdot \Delta L$ , and a third stage **1506** with one MZ interferometer with a delay in one arm of the MZ interferometer of the third stage **1506** of  $4 \cdot \Delta L$ . An input to each MZ interferometer of each stage may include a  $2 \times 2$  multimode interference (MMI) coupler and an output from each MZ interferometer of each stage may include a  $1 \times 2$  MMI coupler.

## 21

The input of each MZ interferometer of each stage may alternatively include a 50/50 directional coupler.

The first stage **1502** of MZ interferometers may have inputs coupled to SiN waveguides **1508**. Similar to the SiN waveguides **1312A** of FIG. **13**, the SiN waveguides **1508** of FIG. **15** may form adiabatic coupler regions with corresponding interposer waveguides to adiabatically couple different wavelength channels from a corresponding optical signal source, such as a corresponding one of the DFBs **1302A-1302D** of FIG. **13**, into the cascade of MZ interferometers **1500**.

The third stage **1506** of MZ interferometers may have an output coupled to an SiN waveguide **1510**. Similar to the SiN waveguide **1316** of FIG. **13**, the SiN waveguide **1510** of FIG. **15** may form an adiabatic coupler region with a Si waveguide to adiabatically couple a multiplexed output signal from the cascade of MZ interferometers **1500** into the Si waveguide.

FIG. **16** is a side view of another example two-stage adiabatically coupled photonic system **1600** (hereinafter “photonic system **1600**”), arranged in accordance with at least one embodiment described herein. The photonic system **1600** includes a Si PIC **1602**, the interposer **704**, and a semiconductor chip **1604**.

The Si PIC **1602** includes a Si substrate **1606**, a SiO<sub>2</sub> box **1608**, a first layer **1610** with one or more SiN waveguides **1612A**, **1612B**, and a second layer **1614** with one or more Si waveguides **1616A**, **1616B**. The Si substrate **1606**, the SiO<sub>2</sub> box **1608**, the first layer **1610**, the SiN waveguides **1612A**, **1612B**, the second layer **1614**, and the Si waveguides **1616A**, **1616B** may generally be similar or identical to, respectively, any of the other Si substrates, SiO<sub>2</sub> boxes, first layers, SiN waveguides, second layers, and Si waveguides disclosed herein except as otherwise indicated herein. For instance, the Si waveguide **1616B** may be adiabatically coupled to the SiN waveguide **1612A** and the SiN waveguide **1612B** may be adiabatically coupled to the interposer waveguide **730**, in a similar manner as generally described above. In some embodiments, the first layer **110** may include a WDM component and/or other features as described elsewhere herein.

The semiconductor chip **1604** may be wafer bonded to the Si PIC **1602** above the second layer **1614** of the Si PIC **1602**. The semiconductor chip **1604** may include an active optical device **1605**, such as an InP-based gain element or gain region needed to form a laser or an InP-based pin detector. The active optical device **1605** of the semiconductor chip **1604** may be optically coupled to one or both of the Si waveguide **1616A** or the Si waveguide **1616B**. Alternatively, the Si waveguides **1616A** and **1616B** may include opposite ends of the same Si waveguide. Accordingly, light may be exchanged between the active optical device **1605** and one or both of the Si waveguides **1616A** or **1616B**. In an example implementation, the Si waveguide **1616B** includes a tapered end to adiabatically couple light into (or out of) the SiN waveguide **1612A**, and an end of the Si waveguide **1616B** opposite its tapered end may include the Si waveguide **1616A** which may be optically coupled to the active optical device **1605** of the semiconductor chip **1604**. A so-called hybrid laser structure can be formed by the InP gain element and Si by adding reflective distributed Bragg reflectors (DBRs) in Si on either side of the InP gain region. The Si DBRs in either side of the InP gain region form an optical cavity with gain which hence produces a laser.

In some Si PICs described herein, the Si PIC may include metal layers and/or metallized structures for electrical contact to active optical components of the Si PIC. Such active optical components may be fabricated at the so-called Back End of Line (BEOL) process. Further, to couple light between the Si

## 22

PIC and an interposer as described herein, an etched window through one or more upper layers down to a layer that includes a SiN waveguide may be formed to expose the SiN waveguide for coupling to an interposer waveguide included in the interposer. In these and other implementations, a top layer of the Si PIC may include metal dummies to maintain flatness after CMP. The metal dummies may have to maintain a certain fill factor. The area of the etched window may be determined by the metal dummy fill factor and may be limited to a few square millimeters (mm<sup>2</sup>).

FIG. **17** is a perspective view of an example Si PIC **1700** that defines an etched window **1702**, arranged in accordance with at least one embodiment described herein. The Si PIC **1700** includes a first layer **1710** with various SiN waveguides **1712**, tapered ends of which are visible in the etched window **1702**. The Si PIC **1700**, the etched window **1702**, the first layer **1710**, and the SiN waveguides **1712** may generally be similar or identical to other Si PICs, etched windows, first layers, and SiN waveguides disclosed herein except as otherwise indicated herein. The Si PIC **1700** may additionally include one or more other components or elements similar to those described with respect to one or more of the other Si PICs disclosed herein.

The Si PIC **1700** additionally includes one or more dielectric layers **1722** above the first layer **1710**, which dielectric layers may be similar or identical to other dielectric layers disclosed herein. The etched window **1702** may be formed by etching through the dielectric layers **1722** to the first layer **1710**. Accordingly, the etched window **1702** may be bounded on three sides (two of which are visible in FIG. **17**) by the dielectric layers **1722**. At least a topmost one of the dielectric layers **1722** includes metal dummies **1704** at least in a region that bounds the etched window **1702** on the three sides. Alternatively, the metal dummies **1704** may extend from the topmost one of the dielectric layers **1722** downward through up to all of the dielectric layers **1722** or some portion thereof.

In an example embodiment, each of the tapered ends of the SiN waveguides **1712** may be about 2.2 millimeters (mm) long such that the etched window **1702** is also at least that long, the dielectric layers **1722** may be about 5-6  $\mu$ m thick such that the etched window **1702** is etched through the dielectric layers **1722** at least that deep, the SiN waveguides **1712** may have a pitch of about 50  $\mu$ m, and the etched window **1702** may have a width of 400  $\mu$ m. Other particular values are possible depending on the desired implementation.

FIG. **18** includes a bottom view **1800A** and a side view **1800B** of an implementation of a portion of the interposer **704** that may be coupled to the Si PIC **1700** of FIG. **17** within the etched window **1702**, arranged in accordance with at least one embodiment described herein. In the embodiment of FIG. **18**, the interposer **704** includes the interposer substrate **726** and the waveguide strip **728** coupled thereto. The waveguide strip **728** includes multiple interposer waveguides **730**, each of which includes interposer core **730A** and interposer cladding **730B**. In the example of FIG. **18**, the interposer **704** may include a polymer interposer such that the interposer substrate **726**, the interposer cores **730A**, and the interposer cladding **730B** respectively include a polymer substrate, polymer cores, and polymer cladding.

A thickness  $t_{is}$  of the interposer substrate **726** may be greater than or equal to about 100  $\mu$ m. A thickness  $t_{clad}$  of the interposer cladding **730B** may be about 14  $\mu$ m. A pitch  $p$  of the interposer cores **730A**, e.g., a nominal core center-to-core center spacing of the interposer cores **730A**, may be about 50  $\mu$ m, or more generally  $X \mu$ m. A width  $w_{core}$  of each of the interposer cores **730A** may be about 8  $\mu$ m. A thickness  $t_{core}$  of each of the interposer cores **730A** may be less than or equal to



a depth of a corresponding etched window of a corresponding Si PIC to which the interposer **704** is to be coupled. A width  $w_{ws}$  of the waveguide strip **728** may be about N times X, where N is a number of the interposer cores **730A** and X is the pitch p or nominal core center-to-core center spacing. A minimum width of the corresponding etched window may also be N times X. Other particular values are possible depending on the desired implementation.

In the views **1800A** and **1800B** of FIG. **18**, the interposer cores **730A** include coupler portions of the polymer waveguides **730**. The coupler portions visible in FIG. **18** may be aligned as described above with tapered ends of corresponding SiN waveguides accessible through the corresponding etched window. The coupler portions are exposed on three of four sides along their length with the interposer cladding **730B** being disposed adjacent to the remaining one of the four sides along the length of the coupler portions. Alternatively, the coupler portions may be exposed only on a bottom side, or along the bottom side and only partially on one or both vertical sides. In these and other embodiments, for a portion (not shown) of the interposer **704** that is not to be disposed inside a corresponding etched window, however, the interposer cores **730A** may generally be surrounded on all four sides along their length by the interposer cladding **730B**.

FIGS. **19A** and **19B** are side views that depict alignment and attachment of the interposer **704** of FIG. **18** and the Si PIC **1700** of FIG. **17**, arranged in accordance with at least one embodiment described herein. As illustrated in FIG. **19A**, the waveguide strip **728** of the interposer **704** is aligned to the etched window **1702** with the interposer cores **730A** generally aligned in the x and z directions with the SiN waveguides **1712** to form adiabatic coupler regions as described elsewhere herein. The etched window **1702** may be at least partially filled with an epoxy underfill **1902**. The interposer **704** may then be moved towards the Si PIC **1700** (or vice versa) as indicated by the arrow **1904** in FIG. **19A** until the interposer cores **730A** are in direct or at least close contact with the SiN waveguides **1712**, as illustrated in FIG. **19B**. As used herein, direct contact between two components or elements means the two components are actually touching each other. Close contact as used herein means the two components are sufficiently close for light to be optically coupled from one component to the other. Such components in close contact may optionally include between the two components an epoxy or other adhesive. Any descriptions herein referring to direct contact can also include close contact which may include a thin layer of, e.g., adhesive. As illustrated in FIG. **19B**, there may be sufficient underfill epoxy **1902** to overflow the etched window **1902** so as to epoxy the top of the dielectric layers **1722** to the interposer cladding **730B** of the interposer **704**.

FIGS. **19A** and **19B** additionally illustrate Si waveguides **1906** included in the Si PIC **1700** that may generally be aligned in the x and z directions with the SiN waveguides **1712** to form adiabatic coupler regions as described elsewhere herein.

FIG. **20** is a side view that depicts alignment of another interposer **2002** and Si PIC **2004**, arranged in accordance with at least one embodiment described herein. The example of FIG. **20** implements a multiple window geometry to satisfy maximum window size and metal dummy fill factor constraints and may otherwise be similarly configured to other embodiments discussed above, including implementation of two-stage adiabatic coupling as discussed herein. In this and other embodiments, the interposer **2002** may include multiple waveguide strips **2006** and the Si PIC **2004** may include multiple etched windows **2008**. Each of the waveguide strips **2006** and etched windows **2008** may generally be similar or

identical to any of the other waveguide strips and etched windows disclosed herein. In general, a lower surface of the interposer **2002**, at least in a region where the interposer **2002** couples to the Si PIC **2004**, may be complementary to an upper surface of the Si PIC **2004**, at least in a region where the Si PIC **2004** couples to the polymer interposer **2002**.

FIG. **21** is a side view that depicts alignment of another interposer **2102** and Si PIC **2104**, arranged in accordance with at least one embodiment described herein. The interposer **2102** includes one or more waveguide strips **2106** while the Si PIC **2104** includes one or more etched windows **2108**. In addition, the example of FIG. **21** implements one or more interposer alignment ridges **2110** and corresponding Si PIC anchor windows **2112** and/or one or more dummy interposer islands **2114** and is otherwise similarly configured to other embodiments discussed above, including implementation of two-stage adiabatic coupling as discussed herein.

The interposer alignment ridges **2110** in some embodiments may be formed from the same material as the interposer cores, interposer cladding, or interposer substrate of the interposer **2102**. Alternately or additionally, each of the interposer alignment ridges **2110** may be about 100 to 200  $\mu\text{m}$  wide and the same or a different thickness as the interposer cores.

The anchor windows **2112** may be etched through one or more dielectric layers of the Si PIC **2104** that are above a corresponding first layer of the Si PIC **2104** that includes SiN waveguides **2116** that are to be optically coupled to interposer waveguides included in the waveguide strip **2106**. The shapes and locations of the anchor windows **2112** may be complementary to the shapes and locations of the interposer alignment ridges **2110**. When attaching the polymer interposer **2102** to the Si PIC **2104**, the interposer alignment ridges **2110** may be aligned to the anchor windows **2104**, which may in turn align exposed coupler portions of the interposer waveguides of the waveguide strip **2106** to the SiN waveguides **2116**. The interposer **2102** may then be moved towards the Si PIC **2104** (or vice versa) as indicated by the arrows **2118** in FIG. **21** until the interposer cores are in direct or at least close contact with the SiN waveguides **2116** to form corresponding adiabatic coupler regions.

The dummy interposer islands **2114** in some embodiments may be formed from the same material as the interposer cores, interposer cladding, or interposer substrate of the interposer **2102**. Alternately or additionally, each of the dummy interposer islands **2114** may be the same or a different width as the interposer alignment ridges **2110** and the same or a different thickness as the interposer cores. A width of the etched window **2108** may be sufficient to accommodate therein the dummy interposer islands **2114** and the waveguide strip **2106** (or more particularly the coupler portions of the interposer waveguides included therein). The dummy interposer islands **2114** may be separated from the nearest interposer waveguides by a sufficient distance to not perturb the optical mode in the nearest interposer waveguides. For example, each of the dummy interposer islands **2114** may be separated from a corresponding nearest interposer waveguide of the waveguide strip **2106** by at least 30  $\mu\text{m}$ . In general, the dummy interposer islands **2114** may provide a relatively large and flat surface to facilitate mechanical attachment process between the interposer **2102** and the Si PIC **2104**.

FIG. **22** includes a side view **2200A** and a bottom view **2200B** of another arrangement of an interposer **2202** with interposer alignment ridges **2204** and dummy interposer islands **2206**, arranged in accordance with at least one embodiment described herein. Similar to other interposers disclosed herein, the interposer **2202** may include an interposer substrate **2208**, an interposer cladding **2210**, and inter-



25

poser cores **2212**. In some embodiments, the interposer **2202** includes a polymer interposer in which each of the interposer substrate **2208**, the interposer cladding **2210**, and the interposer cores **2212** include polymer. As illustrated in the bottom view **2200B**, the interposer cladding **2210** may be removed from a bottom and/or sides of the interposer waveguides **2212** at least in a region **2214** of the interposer **2202** to be received in an etched window of an Si PIC. In a region **2216** of the interposer **2202** that is not received in the etched window, the interposer cladding **2210** may surround all sides of the interposer waveguides **2212** along their length.

FIG. **23A** is a side view of another example two-stage adiabatically coupled photonic system **2300** (hereinafter “photonic system **2300**”) that includes a Si PIC **2302**, an interposer **2304**, and an optical fiber end connector **2306** (hereinafter “connector **2306**”), arranged in accordance with at least one embodiment described herein. The Si PIC **2302** and the interposer **2304** may be similar or identical to, respectively, any of the other Si PICs and interposers disclosed herein except as otherwise indicated herein.

For example, the Si PIC **2302** may include one or more SiN waveguides **2308** formed in a first layer of the Si PIC and one or more Si waveguides **2310** formed in a second layer of the Si PIC that is below (or above in other embodiments) the first layer. Each of the Si waveguides **2310** may include a tapered end aligned in two orthogonal directions with a coupler portion of a corresponding one of the SiN waveguide **2308** to form an adiabatic coupler region. Analogously, each of the SiN waveguides **2308** may include a tapered end aligned in the two orthogonal directions with a coupler portion of a corresponding one of one or more interposer waveguides **2312** included in the interposer **2304** to form another adiabatic coupler region.

The interposer **2304** may include a high index glass waveguide block or high index glass waveguide interposer. Accordingly, in this example, the interposer waveguides **2312** may include high index glass waveguides that may be written into the high index glass waveguide block, e.g., by ion exchange method, ultraviolet (UV) radiation laser writing, or other suitable index altering radiation or process.

Each of the interposer waveguides **2312** may generally be aligned relative to a corresponding one of the SiN waveguides **2308** actively or passively to form adiabatic coupler regions. The alignment of each of the SiN waveguides **2308** to the corresponding Si waveguide **2310** may be achieved in the fabrication process to form adiabatic coupler regions.

An epoxy underfill **2314** may be provided between the interposer **2304** and the Si PIC **2302** to form a mechanical attachment therebetween.

The connector **2306** may include a multi-fiber push on (MPO) connector or other suitable optical fiber end connector.

The interposer **2304** may be coupled to the connector **2306**, which in turn may be coupled to one or more optical fibers (not shown). Light may be coupled from the optical fibers into the interposer waveguides **2312** of the interposer **2304**, and/or from the interposer waveguides **2312** of the interposer **2304** into the optical fibers.

FIG. **23B** is a perspective view of the interposer **2304** of FIG. **23A**, arranged in accordance with at least one embodiment described herein. In these and other implementations, the interposer **2304** may include one or more alignment guides or threaded openings **2316** to receive protrusions or threaded fasteners of the connector **2306** to couple the connector **2306** to the interposer **2304** and/or to optically align the interposer waveguides **2312** of the interposer **2304** with the optical fibers.

26

In some implementations, the interposer waveguides **2312** may be divided into two or more subsets or groups. In the example of FIG. **23B**, the interposer waveguides **2312** are divided into a first subset **2318A** of interposer waveguides **2312** and a second subset **2318B** of interposer waveguides **2312**. The interposer waveguides **2312** may be divided according to their intended function. For instance, the first subset **2318A** of interposer waveguides **2312** may be used to carry incoming light from the optical fibers through the connector **2306** to the Si PIC **2302**, and thus may be referred to as receive (RX) interposer waveguides **2312**. Analogously, the second set **2318B** of interposer waveguides **2312** may be used to carry outgoing light from the Si PIC **2302** to the optical fibers through the connector **2306**, and thus may be referred to as transmit (TX) interposer waveguides **2312**. Si waveguides in the second layer of the Si PIC **2302** and/or SiN waveguides in the first layer of the Si PIC **2302** may also be described as being RX or TX waveguides depending on the function they serve.

As illustrated in FIG. **23B**, at an input/output surface **2320** of the interposer **2304**, ends of the RX interposer waveguides **2312** in the first set **2318A** may generally be arranged parallel to each other and coplanar, while ends of the TX interposer waveguides **2312** in the second set **2318B** may also generally be arranged parallel to each other and coplanar. Alternately or additionally, at the input/output surface **2320**, the ends of the RX interposer waveguides **2312** of the first set **2318A** may be displaced from and parallel to the ends of the TX interposer waveguides **2312** of the second set **2318B** in a double-decker arrangement, as illustrated in FIG. **23B**.

The input/output surface **2320** of the interposer **2304** may be coupled to the connector **2306** of FIG. **23A**. The double-decker arrangement of the RX interposer waveguides **2312** of the first set **2318A** and the TX interposer waveguides **2312** of the second set **2318B** at the input/output surface **2320** may match an arrangement of RX optical fibers and TX optical fibers to which the connector **2306** of FIG. **23A** may be coupled. Other arrangements of the RX and TX interposer waveguides **2312** may be implemented to match other arrangements of the RX and TX optical fibers through the connector **2306**.

FIG. **24** is a perspective view of another example photonic system **2400** (hereinafter “photonic system **2400**”) that includes a Si PIC **2402**, an interposer **2404**, and an optical fiber end connector **2406**, arranged in accordance with at least one embodiment described herein. The photonic system **2400** additionally includes a Si PIC **2402** and an optical fiber end connector **2406**. The Si PIC **2402**, the interposer **2404**, and the connector **2406** may be similar or identical to, respectively, any of the other Si PICs, interposers, and connectors disclosed herein except as otherwise indicated herein.

For example, the Si PIC **2402** may include one or more SiN waveguides **2408** formed in a first layer of the Si PIC and one or more Si waveguides (not shown) formed in a second layer of the Si PIC that is below (or above in other embodiments) the first layer. Each of the Si waveguides may include a tapered end aligned in two orthogonal directions with a coupler portion of a corresponding one of the SiN waveguide **2408** to form an adiabatic coupler region. Analogously, each of the SiN waveguides **2408** may include a tapered end aligned in the two orthogonal directions with a coupler portion of a corresponding one of one or more interposer waveguides included in the interposer **2404** to form another adiabatic coupler region.

The interposer **2404** may include a polymer interposer with a flexible polymer substrate and one or more polymer waveguides formed thereon. The polymer waveguides of the

interposer **2404** may be divided into a first subset of RX polymer waveguides and a second subset of TX polymer waveguides, with the ends of the polymer waveguides arranged in a double decker arrangement where they connect to the connector **2406**, similar to the double decker arrangement described with respect to FIG. **23B**.

In general, light may be coupled out of or coupled into the Si PIC **2402** at a planar interface of the Si PIC **2402**, e.g., a SiN/SiO<sub>2</sub> layer of the Si PIC **2402** that includes the SiN waveguides **2408** of the Si PIC **2402**. Positions of the tapered ends of the SiN waveguides **2408** in the Si PIC **2402**, and thus of tapered ends of the Si waveguides of the Si PIC **2402** may be offset for RX Si waveguides as compared to TX Si waveguides in the light propagation direction to better isolate incoming and outgoing light from each other.

For example, FIGS. **25A** and **25B** illustrate two different offset configurations for RX vs. TX SiN waveguides, arranged in accordance with at least one embodiment described herein. In each of FIGS. **25A** and **25B**, tapered ends of RX SiN waveguides RX1 and RX2 terminate at a common z location (hereinafter “first z location”) and tapered ends of TX SiN waveguides TX1 and TX2 terminate at a different common z location (hereinafter second z location) than for RX1 and RX2. In FIG. **25A**, the tapered ends of the RX Si waveguides alternate with the tapered ends of the TX Si waveguides. In comparison, in FIG. **25B**, the tapered ends of the RX SiN waveguides as a group are located next to the tapered ends of the TX SiN waveguides as a group.

Due to the z offset in FIGS. **25A** and **25B** between the RX and TX SiN waveguides, RX and TX portions of an interposer to couple light into or out of a Si PIC that includes the RX and TX SiN waveguides of FIGS. **25A-25B** may be separated from each other. For instance, RX interposer waveguides of the interposer may be coupled to the Si PIC in a region generally denoted at **2502A** in FIG. **25A** and **2502B** in FIG. **25B**, while TX interposer waveguides of the interposer may be coupled to the Si PIC in a region generally denoted at **2504A** in FIG. **25A** and **2504B** in FIG. **25B**. Although FIGS. **25A** and **25B** are discussed in the context of SiN waveguide/interposer waveguide adiabatic coupler regions, the same principles may be applied for Si waveguide/interposer waveguide adiabatic coupler regions.

Some interposers discussed herein have been described as including polymer or high index glass. Other materials for the interposer are possible. For example FIG. **26** includes a side view **2600A** and a bottom view **2600B** of a silicon oxynitride (SiON) interposer **2602**, arranged in accordance with at least one embodiment described herein.

The SiON interposer **2602** includes a SiON waveguide strip **2604** with multiple SiON waveguides **2606**, each including a SiON core **2608** and a SiON cladding **2610**. The SiON cores **2608** may be exposed (e.g., not surrounded by SiON cladding **2610**) on at least one surface within a coupling region of the SiON interposer **2602** to be received in an etched window of a corresponding Si PIC so as to be aligned and brought into direct or at least close contact with corresponding SiN waveguides of the Si PIC.

In the illustrated embodiment, the SiON interposer **2602** includes SiON on SiO<sub>2</sub> substrate **2612** or other substrate. SiON has a refractive index that can vary between that of SiO<sub>2</sub> around 1.46 and that of SiN around 1.99 by changing the growth conditions of the fraction of O and N in the SiON portions of the SiON interposer **2602**. A refractive index of around 1.51 can be achieved to form the SiON cladding **2610** and a slightly higher index of 1.516, for example, can be achieved to form the SiON cores **2608** of the SiON waveguides **2606**.

A width  $w_s$  of the SiO<sub>2</sub> substrate **2612** may be in a range from 2 mm to 7 mm. A pitch  $H_p$  of the SiON cores **2608** may be in a range from 50  $\mu$ m to 250  $\mu$ m. A width  $w_s$  of the waveguide strip **2604** may be in a range from 400  $\mu$ m to 1.5 mm depending on number of SiON cores **2608** and the pitch  $p$ . A thickness  $t$  of the SiON cladding **2610** may be greater than or equal to 15  $\mu$ m. A thickness  $t_{core}$  and a width  $w_{core}$  of the SiON cores **2608** may each be in a range from 6  $\mu$ m to 8  $\mu$ m. Other particular values are possible depending on the desired implementation.

In the example of FIG. **26**, the SiON cladding **2610** can be flush with a top surface (in a growth direction) of the SiON cores **2608** (which is the bottom surface in the orientation of the view **2600A** of FIG. **26**). The SiON waveguides **2606** may be aligned in two orthogonal directions with corresponding SiN waveguides of a Si PIC to form adiabatic coupler regions. The SiON of the SiON interposer **2602** can be etched to form a plug to fit a corresponding etched window in a Si PIC, such as is illustrated in FIG. **27**.

FIG. **27** is a side view that depicts alignment of the SiON interposer **2602** of FIG. **26** and the Si PIC **1700** of FIG. **17**, arranged in accordance with at least one embodiment described herein. As illustrated in FIG. **27**, the SiON waveguide strip **2604** of the SiON interposer **2602** is aligned to the etched window **1702** of the Si PIC **1700** with the SiON cores **1608** generally aligned in the x and z directions with the SiN waveguides **1712** of the Si PIC **1700** in the manner described above to form adiabatic coupler regions. The etched window **1702** may be at least partially filled with the epoxy underfill **1902**. The SiON interposer **2602** may then be moved towards the Si PIC **1700** (or vice versa) as indicated by the arrow **2702** until the SiON cores **2608** are in direct or at least close contact with the SiN waveguides **1712** of the Si PIC **1700**.

FIG. **28** illustrates two example optoelectronic systems **2800A** and **2800B** (hereinafter “systems **2800**”) that each include at least one polymer on glass interposer **2802A**, **2802B**, **2802C** (collectively “polymer on glass interposers **2802**”), arranged in accordance with at least one embodiment described herein. The polymer on glass interposers **2802** may generally be similar or identical to any of the other interposers disclosed herein except as otherwise indicated herein. Each of the systems **2800** includes a multi-channel optoelectronic module (hereinafter “module”) **2804A** or **2804B**, such as a 4-channel parallel single mode **4** (PSM4) transceiver. Each of the modules **2804A** and **2804B** includes a Si PIC with one or more Si waveguides and one or more SiN waveguides that together form one or more adiabatic coupler regions.

In the photonic system **2800A**, the module **2804A** is configured to receive multiple optical signals **2806A** from an optical network through an input connector **2808A**. The optical signals **2806A** may be adiabatically coupled into the Si PIC of the module **2804A** through the polymer on glass interposer **2802A** and one or more SiN waveguides and Si waveguides of the Si PIC of the module **2804A**, in the manner generally described above.

In the photonic system **2800B**, the module **2804B** is configured to transmit multiple optical signals **2806B** to the optical network through an output connector **2808B**. One or more of the optical signals **2806B** may be adiabatically coupled from an optical transmitter **2810** of the module **2804B** and into the Si PIC of the module **2804A** through the polymer on glass interposer **2802C** (labeled “Polymer on glass plug”) and one or more SiN waveguides and Si waveguides of the Si PIC of the module **2804B**, in the manner generally described above. The optical signals may also be adiabatically coupled out of the Si PIC and into the output connector **2806B** through

one or more Si waveguides and SiN waveguides of the Si PIC of the module **2804B** and the polymer on glass interposer **2802B**, in the manner generally described above.

FIG. **29A** illustrates an example polymer on glass interposer **2900A** and Si PIC **2902**, arranged in accordance with at least one embodiment described herein. The polymer on glass interposer **2900A** may be implemented in, e.g., either or both of the systems **2800** of FIG. **28** as one or more of the polymer on glass interposers **2802A-2802C**.

In the illustrated embodiment, the Si PIC **2902** defines an etched window **2904**. The Si PIC **2902** additionally includes a Si substrate **2906**, a SiO<sub>2</sub> box **2908**, a first layer **2910** with various SiN waveguides **2912**, a second layer **2914** with various Si waveguides **2916**, and one or more dielectric layers **2918** above the first layer **2910** that includes the SiN waveguides **2912**. The Si PIC **2902**, the etched window **2904**, the Si substrate **2906**, the SiO<sub>2</sub> box **2908**, the first layer **2910**, the SiN waveguides **2912**, the second layer **2914**, the various Si waveguides **2916**, and the dielectric layers **2918** may generally be similar or identical to, respectively, any of the other Si PICs, etched windows, Si substrates, SiO<sub>2</sub> boxes, first layers, SiN waveguides, second layers, Si waveguides, and dielectric layers disclosed herein excepted as otherwise indicated herein. For example, the SiN waveguides **2912** and the Si waveguides **2916** may be arranged relative to each other to adiabatically couple light from the Si waveguides **2916** to the SiN waveguides **2912**, or vice versa, as described elsewhere herein. The Si PIC **2902** may additionally include one or more other components, layers, features, or aspects as described elsewhere herein.

The etched window **2904** may be formed by etching through the dielectric layers **2918** to the second layer **2914**. In some embodiments, the etched window **2904** is bounded on three sides (two of which are visible in FIG. **29A**) by the dielectric layers **2918**. At least a topmost one of the dielectric layers **2918** includes metal dummies **2920** at least in a region that bounds the etched window **2904** on the three sides.

The polymer on glass interposer **2900A** includes a glass substrate **2922** and a polymer waveguide strip coupled thereto. The glass substrate **2922** may include UV transparent glass and is a specific example of an interposer substrate. The polymer waveguide strip is a specific example of a waveguide strip and includes multiple polymer waveguides **2924**, each of which includes a polymer core **2926** and polymer cladding **2928**. The polymer cladding layer **2928** is coupled to the glass substrate **2922**. The polymer cores **2926** are coupled to the polymer cladding **2928**. The polymer waveguides **2924** include coupler portions as described above that are configured to be aligned in two orthogonal directions (e.g., x and z directions) with tapered ends of the SiN waveguides **2912** such that the coupler portions of the polymer waveguides **2924** overlap in the two orthogonal directions and are parallel to the tapered ends of the SiN waveguides **2912**. In this arrangement, light may be adiabatically coupled from the SiN waveguides **2912** to the polymer waveguides **2924**, or vice versa.

As illustrated, the polymer cores **2926** are parallel to each other. The polymer cores **2926** may have a pitch of 250 micrometers. Alternatively, the pitch of the polymer cores **2926** may be in a range from 290-500 micrometers, or some other value. A length of the polymer cores **2926** and/or of the polymer on glass interposer **2900A** in the z direction may be in a range from 1 millimeter to 4 millimeters, at least for a portion of the length of the polymer cores **2926** that is received within the etched window **2904**. A height or thickness in the y direction of each of the polymer cores **2926** may be less than or equal to a depth in the y direction of the etched

window **2904**. In other embodiments, the height or thickness in the y direction of each of the polymer cores **2926** may be greater than the depth in the y direction of the etched window **2904**. In an example embodiment, the height of the polymer cores **2926** is in a range from 4 μm to 7 μm. A width in the x direction of the polymer on glass interposer **2900A** may be in a range from 1 mm to 2 mm.

In some embodiments, the etched window **2904** may be at least partially filled with an epoxy underfill **2930**. To assemble the polymer on glass interposer **2900A** and the Si PIC **2902** together, the polymer on glass interposer **2900A** may be moved toward the Si PIC **2902** as indicated by arrow **2932** until the polymer cores **2926** are in direct or at least close contact with the SiN waveguides **2912**. In some embodiments, there may be sufficient epoxy underfill **2930** to overflow the etched window **2904** so as to epoxy the top of the dielectric layers **2918** to the polymer cladding **2928** of the polymer on glass interposer **2900A**.

FIG. **29B** illustrates another example polymer on glass interposer **2900B**, arranged in accordance with at least one embodiment described herein. The polymer on glass interposer **2900A** may be implemented in, e.g., either or both of the systems **2800** of FIG. **28** as one or more of the polymer on glass interposers **2802A-2802C**.

The polymer on glass interposer **2900B** includes the glass substrate **2922** and the polymer waveguides **2924**, including the polymer cores **2926** and the polymer cladding **2928**. The polymer on glass interposer **2900B** additionally includes one or more first polymer alignment ridges **2934A** disposed to a first side of the polymer waveguides **2924** and one or more second polymer alignment ridges **2934B** disposed to a second side of the polymer waveguides **2924** that is opposite the first side. The polymer alignment ridges **2934A** and **2934B** (collectively "polymer alignment ridges **2934**") may be received in one or more corresponding etched channels, windows, recesses, or other features of a corresponding Si PIC to align the polymer on glass substrate **2900B** (and more particularly, the polymer waveguides **2924**) to the Si PIC (and more particularly, SiN waveguides of the Si PIC).

The polymer on glass interposers **2900A** and **2900B** of FIGS. **29A** and **29B** and the Si PIC **2902** of FIG. **29A** may include one or more other components, layers, features, or aspects as described elsewhere herein.

For example, the polymer on glass substrate **2900B** may further include one or more dummy polymer islands, such as a first dummy polymer island between the polymer cores **2926** and the first polymer alignment ridges **2934A**, and a second dummy polymer island between the polymer cores **2926** and the second polymer alignment ridges **2934B**. In these and other embodiments, a width of the etched window of the Si PIC **2902** may be sufficient to accommodate therein the first dummy polymer island, the coupler portion of each of the polymer waveguides **2924**, and the second dummy polymer island.

Referring again to FIGS. **3A** and **3B**, and as already described, light may be coupled from the Si waveguide **212** to the SiN waveguide **208** and then from the SiN waveguide **208** to the interposer waveguide **224**. The Si substrate (not shown) on which the SiO<sub>2</sub> box **204** is formed is some distance d (e.g., in the y direction) away from the SiN waveguide **208**. Here, the distance d is about equal to the thickness of the SiO<sub>2</sub> box **204** plus the thickness of the second layer **210**. In an example embodiment, the thickness of the SiO<sub>2</sub> box **204** is 0.72 micrometers and the thickness of the second layer **210** is about 0.3 micrometers such that the distance d may be about 1.02 micrometers. For these values, some light propagating in the SiN waveguide **208** may couple into the Si substrate and

31

be lost. This loss may be referred to as substrate leakage. The substrate leakage may be significant since an optical mode in the SiN waveguide **208** may be much less confined than in the Si waveguide **212**.

Some embodiments described herein reduce the substrate leakage by increasing the distance *d* between the SiN waveguide **208** and the Si substrate. For example, the thickness of the SiO<sub>2</sub> box **204** may be increased to a thickness greater than 0.72 micrometers, such as 2 micrometers, or a thickness in a range of 2 micrometers plus or minus 10%. However, increasing the thickness of the SiO<sub>2</sub> box **204** to such an extent may be incompatible with some fabs/manufacturers.

Alternatively, one or more other modifications may be made. For instance, the thickness of the SiN waveguide **208** in the *y* direction may be increased to better confine a vertical E-field of propagating light and therefore reduce substrate leakage. Alternatively or additionally, an SiO<sub>2</sub> layer may be provided between the first layer **206** and the second layer **210** and/or the thickness of such a layer may be increased to increase the distance *d* between the SiN waveguide **208** and the Si substrate. As the distance *d* increases, Si—SiN TE coupling may decrease to decrease substrate leakage. The foregoing will be described with respect to FIG. **30**. Alternatively or additionally, a two-layer SiN structure may be implemented as described with respect to FIGS. **31A** and **31B**.

FIG. **30** illustrates a cross-sectional view of an example Si PIC **3000**, arranged in accordance with at least one embodiment described herein. The Si PIC **3000** may generally be similar or identical to any of the other Si PICs disclosed herein except as otherwise indicated herein. The cross-sectional view of FIG. **30** is taken from a similar perspective as the cross-sectional view **300C** of FIG. **3B** and illustrates an example layer stackup of the Si PIC **3000**. The Si PIC **3000**, as compared to the example of FIGS. **3A** and **3B**, increases a thickness of a SiN waveguide and increases a distance between the SiN waveguide and a corresponding Si substrate to reduce substrate leakage.

As illustrated, the Si PIC **3000** includes a Si substrate **3002**, a SiO<sub>2</sub> box **3004**, a first layer **3006** that includes a SiN waveguide **3008**, a SiN slab **3010**, and a second layer **3012** that includes a Si waveguide **3014**. The Si PIC **3000** may additionally include a first SiO<sub>2</sub> layer **3016** between the second layer **3012** and the SiN slab **3010** and a second SiO<sub>2</sub> layer **3018** between the SiN slab **3010** and the first layer **3006**. The Si waveguide **3014** and the SiN waveguide **3008** may be arranged to form an adiabatic coupler region as described elsewhere herein.

In some embodiments, a total thickness of all layers of the Si PIC **3000** between a top of the Si substrate **3002** and a bottom of the first layer **3006** that includes the SiN waveguide **3008** may be at least 1.2  $\mu\text{m}$ . For example, the SiO<sub>2</sub> box **3004** may have a thickness of 0.72  $\mu\text{m}$ , or a thickness in a range of 0.72  $\mu\text{m}$  plus or minus 10%, or some other thickness. The SiN waveguide **3008**, and thus the first layer **3006**, may have a thickness of 0.7  $\mu\text{m}$ , or a thickness in a range of 0.7  $\mu\text{m}$  plus or minus 10%, or some other thickness. The second SiO<sub>2</sub> layer **3018** immediately beneath the SiN waveguide **3008** may have a thickness of at least 0.1  $\mu\text{m}$ , or a thickness in a range of 0.1  $\mu\text{m}$  to 0.2  $\mu\text{m}$  or more, or some other thickness. The Si waveguide **3014**, and thus the second layer **3012**, may have a thickness of 0.3  $\mu\text{m}$ , or a thickness in a range of 0.3  $\mu\text{m}$  plus or minus 10%, or some other thickness. The first SiO<sub>2</sub> layer **3016** may be omitted altogether, or may have a thickness in a range from 10 nm-290 nm. The SiN slab **3010** may be omitted altogether or may have a thickness in a range of 0.04  $\mu\text{m}$  to 0.07  $\mu\text{m}$ , or some other thickness. Accordingly, in some

32

embodiments, all the layers between the Si substrate **3002** and the first layer **3006** may have a total thickness of at least 1.2  $\mu\text{m}$  (e.g.,  $0.72+0.2+0.3=1.22 \mu\text{m}$ ) in the example of FIG. **30**, as compared to about 1  $\mu\text{m}$  in the example of FIGS. **3A** and **3B**.

As compared to the example of FIGS. **3A** and **3B**, the optical mode may be more confined in the relatively larger SiN waveguide **3008**. Additionally, the increased distance between the Si substrate **3002** and the SiN waveguide **3008** as compared to FIGS. **3A** and **3B** may further optically isolate the Si substrate **3002** from the SiN waveguide **3008** to reduce substrate leakage.

FIG. **30** additionally illustrates first-third simulations **3020A-3020C** for the Si PIC **3000** of FIG. **30** in which SiN propagation loss through the SiN waveguide **3008** has been ignored. The first simulation **3020A** includes a graph of propagation loss or substrate leakage along the vertical axis in units of decibels (dB) per centimeter (cm) as a function of SiO<sub>2</sub> gap thickness along the horizontal axis in units of nanometers. The SiO<sub>2</sub> gap thickness in the first simulation **3020A** refers to the thickness of the second SiO<sub>2</sub> layer **3018** in the Si PIC **3000**. As illustrated in the first simulation **3020A**, propagation loss of TM and TE optical modes (labeled “TM” and “TE” throughout FIG. **30**) decreases with increasing SiO<sub>2</sub> gap thickness. For instance, from a SiO<sub>2</sub> gap thickness of 0.1  $\mu\text{m}$  to 0.2  $\mu\text{m}$ , the propagation loss for the TM optical mode decreases from about 1.16 dB/cm to about 0.55 dB/cm and the propagation loss for the TE optical mode decreases from about 0.91 dB/cm to about 0.45 dB/cm.

The second simulation **3020B** includes a graph of SiN-to-Si coupling efficiency along the vertical axis as a function of Si taper length along the horizontal axis in units of  $\mu\text{m}$ . The Si taper length refers to a length of a tapered end of the Si waveguide **3014**. As illustrated in the second simulation **3020B**, the SiN-to-Si coupling efficiency generally increases with increasing Si taper length and is about 97% or higher for both TE and TM optical modes at a Si taper length of about 250  $\mu\text{m}$ .

The third simulation **3020C** includes a graph of polymer-to-SiN coupling efficiency along the vertical axis as a function of SiN linear taper length along the horizontal axis in units of  $\mu\text{m}$ . The SiN linear taper length refers to a length of the tapered end of the SiN waveguide **3008**. As illustrated in the third simulation **3020C**, the polymer-to-SiN coupling efficiency generally increases with increasing SiN linear taper length and is about 95% or higher for both TE and TM optical modes at a SiN linear taper length of about 2 millimeters (or 2000  $\mu\text{m}$ ).

The Si PIC **3000** may include one or more other components, layers, features, or aspects as described elsewhere herein.

FIG. **31A** illustrates another example Si PIC **3100**, arranged in accordance with at least one embodiment described herein. The Si PIC **3100** may generally be similar or identical to any of the other Si PICs disclosed herein except as otherwise indicated herein. FIG. **31A** includes a cross-sectional view **3101A** and an overhead view **3101B** of the Si PIC **3100**. The cross-sectional view of FIG. **31A** is taken from a similar perspective as the cross-sectional view **300C** of FIG. **3B** and illustrates an example layer stackup of the Si PIC **3100**. The Si PIC **3100** implements a two-layer SiN structure to reduce substrate leakage.

As illustrated, the Si PIC **3100** includes a Si substrate **3102**, a SiO<sub>2</sub> box **3104**, a first layer **3106** that includes a SiN waveguide **3108**, a SiN slab **3110**, a second layer **3112** that includes a Si waveguide **3114**, and a third layer **3116** that includes a SiN transition waveguide **3118**. The Si PIC **3100**

may additionally include one or more SiO<sub>2</sub> layers **3120** between the second layer **3112** and the SiN slab **3110**, between the SiN slab **3110** and the third layer **3116**, and/or between the third layer **3116** and the first layer **3106**.

In some embodiments, a total thickness of all layers of the Si PIC **3100** between a top of the Si substrate **3102** and a bottom of the first layer **3106** that includes the SiN waveguide **3108** may be at least 1.2 μm, such as 1.6 μm or 1.6 μm plus or minus 10%. In more detail, the SiO<sub>2</sub> box **3104** may have a thickness of 0.72 μm, or a thickness in a range of 0.72 μm plus or minus 10%, or some other thickness. The Si waveguide **3114**, and thus the second layer **3112**, may have a thickness of 0.3 μm, or a thickness in a range of 0.3 μm plus or minus 10%, or some other thickness. The SiO<sub>2</sub> layer **3120** immediately above the second layer **3112** may be omitted altogether, or may have a thickness in a range from 10-290 nm, or some other thickness. The SiN slab **3110** may have a thickness in a range from 0.04 to 0.07 μm, or some other thickness. The SiN transition waveguide **3118**, and thus the third layer **3116**, may have a thickness of 0.5 μm, or a thickness in a range of 0.5 μm plus or minus 10%, or some other thickness. The SiN transition waveguide **3118** may have a width in the x direction other than at one or more tapered ends thereof in a range from 1-2 μm, or some other width. The SiO<sub>2</sub> layer **3120** immediately beneath the SiN transition waveguide **3118** may have a thickness in a range from 0.04-0.07 μm, or some other thickness. The SiN waveguide **3108**, and thus the first layer **3106**, may have a thickness in a range from 0.04-0.07 μm, or some other thickness. The SiN waveguide **3108** may have a width in the x direction other than at one or more tapered ends thereof of 0.6-1 μm, or some other width. The SiO<sub>2</sub> layer **3120** immediately beneath the SiN waveguide **3108** may have a thickness in a range from 0.05-0.2 μm, or some other thickness.

The overhead view **3101B** illustrates relative x-axis and z-axis alignment of various w components of the Si PIC **3100** with respect to each other and includes reference lines **1**, **2**, **3**, and **4**. The relative x-axis and z-axis alignment between the Si waveguide **3114**, the SiN transition waveguide **3118**, and the SiN waveguide **3108** and aspects of each of the foregoing waveguides will now be described. As illustrated, the SiN waveguide **3108** includes a tapered end between reference lines **3** and **4**. Although not illustrated in FIG. **31A**, the SiN waveguide **3108** may include another tapered end opposite the tapered end illustrated in FIG. **31A** to adiabatically couple light into a corresponding interposer waveguide or to adiabatically receive light from the interposer waveguide.

The SiN transition waveguide **3118** includes a coupler portion between reference lines **1** and **3** at a first end of the SiN transition waveguide **3118**. The SiN transition waveguide **3118** also includes a tapered end between reference lines **3** and **4** opposite the first end. The tapered end of the SiN transition waveguide **3118** is aligned in two orthogonal directions (e.g., in the x and z directions) with the tapered end of the SiN waveguide **3108** such that the tapered end of the SiN transition waveguide **3118** overlaps in the two orthogonal directions and is parallel to the tapered end of the SiN waveguide **3108**.

The Si waveguide **3114** includes a tapered end between reference lines **2** and **3**. The tapered end of the Si waveguide **3114** is aligned in the two orthogonal direction (e.g., in the x and z directions) with the coupler portion of the SiN transition waveguide **3118** such that the tapered end of the Si waveguide **3114** overlaps in the two orthogonal directions and is parallel to the coupler portion of the SiN transition waveguide **3118**.

As illustrated in the overhead view **3101B**, the tapered end of the Si waveguide **3114** may terminate where the tapered end of the SiN waveguide **3108** begins, e.g., at reference line

**3**. Alternately or additionally, a region in which the tapered ends of the SiN waveguide **3108** and the SiN transition waveguide **3118** overlap may be referred to as a dual taper region **3122**. The dual taper region **3121** may have a length in the z direction of at least 20 μm, or at least 30 μm, or some other length.

The Si PIC **3100** may include one or more other components, layers, features, or aspects as described elsewhere herein.

FIG. **31B** illustrates first-fourth simulations **3124A-3124C** for the Si PIC **3100** of FIG. **31A**, arranged in accordance with at least one embodiment described herein. Due to the SiN transition waveguide **3118** being separated from the Si substrate **3102** by about 1.1 μm in the example of FIG. **31A**, some substrate leakage may occur for light propagating through the SiN transition waveguide **3118**. However, a total length of the SiN transition waveguide **3118** in the z direction may be relatively short, such as about 100 μm or less, such that the substrate leakage may be relatively low. On the other hand, the SiN waveguide **3108** may be separated from the Si substrate **3102** by 1.2 μm or more, or even 1.6 μm or more, such that light propagating through the SiN waveguide **3108** may experience little or no substrate leakage, such as about 0.1 dB/cm for the TE optical mode and about 0.35 dB/cm for the TM optical mode.

The first and second simulations **3124A** and **3124B** illustrate propagation of the TE and TM optical modes, respectively, from the SiN transition waveguide **3118** in the area generally labeled "Layer 1" to the Si waveguide **3118** in the area generally labeled "Layer 2". The third simulation **3124C** includes a graph of transmission efficiency from the SiN transition waveguide **3118** to the SiN waveguide **3108** along the vertical axis as a function of dual taper length along the horizontal axis in units of μm. The dual taper length refers to the length of the dual taper region **3122**. As illustrated in the third simulation **3124C**, the transmission efficiency increases with increasing dual taper length and is about 90% or higher for both TE and TM optical modes at a dual taper length of about 20 μm and is about 96% or higher for both TE and TM optical modes at a dual taper length of about 30 μm.

Some Si PICs may include a WDM mux or WDM demux as described elsewhere herein, such as an Echelle grating in a SiN layer of the Si PIC. As used herein, a SiN layer of a Si PIC refers to a layer of the Si PIC that includes SiN, which layer may additionally include other materials such as SiO<sub>2</sub> in various locations within the SiN layer. In a WDM demux configuration, incoming light received from the WDM demux may be coupled from a SiN waveguide through a Si waveguide in a Si layer of the Si PIC to a Si/germanium (Ge) based pin detector included in the Si layer of the Si PIC. As used herein, a Si layer of a Si PIC refers to a layer of the Si PIC that includes Si, which layer may additionally include other materials such as SiO<sub>2</sub> in various locations within the Si layer. Some WDM demuxes have to have a multimode output to allow a flat top shape for a filter function associated with the WDM demuxes. For example, a SiN-based WDM demux may utilize TE<sub>00</sub>, TE<sub>01</sub>, TM<sub>00</sub>, and TM<sub>01</sub> optical modes. Some of the SiN-to-Si adiabatic coupler regions described above may accommodate single mode light. Such single mode adiabatic coupler regions may reduce effective bandwidth of a WDM demux with a multimode output, since only a single mode may be coupled from the SiN waveguide to the Si waveguide.

Some embodiments described herein may include a multimode SiN-to-Si adiabatic coupler region to accept demultiplexed and/or multimode output of a WDM demux without reducing effective bandwidth of the WDM demux. In particu-

lar, FIG. 32 illustrates a multimode SiN-to-Si adiabatic coupler region 3200 (hereinafter “coupler 3200”), arranged in accordance with at least one embodiment described herein. The coupler 3200 may be implemented in any of the Si PICs described herein. Such Si PICs may generally include a SiO<sub>2</sub> box, a first layer formed above the SiO<sub>2</sub> box that includes a SiN waveguide 3202, and a second layer formed above the SiO<sub>2</sub> box and above or below the first layer and that includes a Si waveguide 3204.

The SiN waveguide 3202 includes an untapered end portion 3206 and a tapered end 3208 that begins where the untapered end portion 3206 begins, the untapered end portion 3206 and the tapered end 3208 extending in opposite directions. Although not illustrated in FIG. 32, the SiN waveguide 3202 may extend to the left of the untapered end portion 3206. The untapered end portion 3206 may receive a multimode input optical signal 3210 such as may be output by a SiN-based WDM demux.

The Si waveguide 3204 includes an untapered end portion 3212 and a tapered end 3214 that begins where the untapered end portion 3212 begins, the untapered end portion 3212 and the tapered end 3214 extending in opposite directions. The Si waveguide 3204 may extend to the right of the untapered end portion 3212. The Si waveguide 3204 may be configured to accept the multimode input optical signal 3210 from the SiN waveguide 3202.

In some embodiments, the untapered end portion 3206 of the SiN waveguide 3202 is aligned in two orthogonal directions (e.g., the x and z directions) with the tapered end 3214 of the Si waveguide 3204 such that the untapered end portion 3206 of the SiN waveguide 3202 overlaps in the two orthogonal directions and is parallel to the tapered end 3214 of the Si waveguide 3204. Additionally, the tapered end 3208 of the SiN waveguide 3202 is aligned in the two orthogonal directions with the untapered end portion 3212 of the Si waveguide 3204 such that the tapered end 3208 of the SiN waveguide 3202 overlaps in the two orthogonal directions and is parallel to the untapered end portion 3212 of the Si waveguide 3204.

A region in which the untapered end portion 3206 of the SiN waveguide 3202 and the tapered end 3214 of the Si waveguide 3204 overlap may be referred to as a first region 3216. A region in which the tapered end 3208 of the SiN waveguide 3202 and the untapered end portion 3212 of the Si waveguide 3204 overlap may be referred to as a second region 3218. Lengths of the first region 3216 and the second region 3218 and/or other parameters associated with the coupler 3200 may be adjusted to optimize the multimode coupling from the SiN waveguide 3202 to the Si waveguide 3204, as illustrated in FIGS. 33A-33D.

FIGS. 33A-33D include various simulations for the coupler 3200 of FIG. 32 with various different sets of parameters, arranged in accordance with at least one embodiment described herein.

FIG. 33A includes a first table 3302 of parameters, a second table 3304 of simulated transmission efficiency from the SiN waveguide 3202 to the Si waveguide 3204 of FIG. 32, and simulations 3306A and 3306B. With combined reference to FIGS. 32 and 33A, the parameters of FIG. 33A that are listed in the first table 3302 will now be described. In this example, the first region 3216 has a length of 90  $\mu\text{m}$  and the second region 3218 has a length of 10  $\mu\text{m}$ . In the first region 3216, the tapered end 3214 of the Si waveguide 3204 has a width that tapers along the light propagation direction from 0.08  $\mu\text{m}$  to 1.5  $\mu\text{m}$ . In the second region 3218, the untapered end portion 3212 of the Si waveguide 3204 has a width of 1.5  $\mu\text{m}$ . In the first region 3216, the untapered end portion 3206 of the SiN waveguide 3202 has a width of 2  $\mu\text{m}$ . In the second region

3218, the tapered end 3208 of the SiN waveguide 3202 has a width that tapers along the light propagation direction from 2  $\mu\text{m}$  to 0.2  $\mu\text{m}$ .

The second table 3304 includes simulated transmission efficiency for the TE<sub>00</sub>, TE<sub>01</sub>, TM<sub>00</sub>, and TM<sub>01</sub> optical modes associated with the parameters listed in the first table 3302.

The simulations 3306A and 3306B include graphs of transmission efficiency in the coupler 3200 along the vertical axis as a function of Si taper length along the horizontal axis in units of  $\mu\text{m}$  for the TE<sub>N</sub> optical mode (simulation 3306A) and the TM<sub>01</sub> optical mode (simulation 3306B) for five different wavelength channels. The Si taper length refers to the length of the first region 3216. In the simulations 3306A and 3306B, all parameters other than the length of the first region 3216 are assumed to be the parameters provided in the first table 3302.

FIG. 33B includes simulations 3306C and 3306D that use the same parameters as the simulations 3306A and 3306B of FIG. 33A except that the untapered end portion 3206 of the SiN waveguide 3202 has a width of 1.5  $\mu\text{m}$  in the first region 3216 and the tapered end 3208 of the SiN waveguide 3202 tapers from 1.5  $\mu\text{m}$  to 0.2  $\mu\text{m}$  in the second region 3218.

FIG. 33C includes simulations 3306E and 3306F that use the same parameters as the simulations 3306C and 3306D of FIG. 33B except that the tapered end 3214 of the Si waveguide 3204 tapers from 0.08  $\mu\text{m}$  to 1  $\mu\text{m}$  in the first region 3216 and the untapered end portion 3212 of the Si waveguide 3204 has a width of 1  $\mu\text{m}$  in the second region 3218. As illustrated in the simulations 3306E and 3306F, at a Si taper length (or first region 3216 length) of 90  $\mu\text{m}$ , the TE<sub>01</sub> optical mode has a transmission efficiency of about 0.96 for all five wavelength channels and the TM<sub>01</sub> optical mode has a transmission efficiency between about 0.92-0.96 depending on the wavelength channel.

FIG. 33D includes simulations 3306G and 3306H that are similar to the simulations 3306A-3306E described above, except using parameters listed in table 3308. As illustrated in the simulations 3306G and 3306H, at a Si taper length (or first region 3216 length) of 100  $\mu\text{m}$ , the TE<sub>01</sub> optical mode has a transmission efficiency of between about 0.95-0.97 depending on the wavelength channel and the TM<sub>01</sub> optical mode has a transmission efficiency between about 0.92-0.95 depending on the wavelength channel.

One or more of the WDM components described herein may have a polarization-dependent filter function. In these and other embodiments, one or more of the Si PICs described herein may further include one or more Si PIC polarization splitters or combiners (hereinafter “polarization splitter” or “polarization splitters”). The Si PIC may additionally include two polarization-specific WDM components, each of which has an input coupled to a different output of the polarization splitter. One of the polarization-specific WDM components may be optimized for TE polarization and the other may be optimized for TM polarization. Alternatively, each of the polarization-specific WDM components may be optimized for the same polarization and the Si PIC may additionally include a polarization rotator coupled between one of the two outputs of the polarization splitter and the input of one of the polarization-specific WDM components. The polarization rotator may include a Si PIC polarization rotator integrally formed in the Si PIC.

FIGS. 34A and 34B illustrate embodiments of a demultiplexer system 3400A and 3400B (collectively “demultiplexer systems 3400”), arranged in accordance with at least one embodiment described herein. Some or all of the demultiplexer systems 3400 may be implemented in a Si PIC, such as the Si PICs described above. The demultiplexer systems 3400 each include a Si PIC polarization splitter or combiner 3402

(hereinafter “polarization splitter **3402**”) a first WDM demux **3404**, a second WDM demux **3406A** or **3406B** (generically “second WDM demux **3406**”), first opto-electrical transducers **3408**, second opto-electrical transducers **3410**, and adders **3412** (only one of which is illustrated for simplicity). Additional adders **3412** are denoted by ellipses in each of FIGS. **34A** and **34B**. The demultiplexer system **3400B** of FIG. **34B** may additionally include a polarization rotator **3414**.

The polarization splitter **3402** in each of the demultiplexer systems **3400** includes an input **3402A** and first and second outputs **3402B** and **3402C** excepted when implemented as a combiner, in which case the inputs and outputs may be reversed. As described in more detail below, the polarization splitter **3402** may generally include first and second SiN waveguides formed in a corresponding layer of a Si PIC and a Si waveguide with two tapered ends formed in another layer of the Si PIC above or below the layer in which the first and second SiN waveguides are formed. In some embodiments, the first and second WDM demuxes **3404** and **3406** may be formed in the same layer of the Si PIC as the first and second SiN waveguides of the polarization splitter **3402**, as described elsewhere herein.

The input **3402A** may include a first end of the first SiN waveguide, the first output **3402B** may include a second end of the first SiN waveguide, and the second output **3402C** may include a second end of the second SiN waveguide. On the input, the polarization splitter **3402** may receive an input beam **3415** including an N-channel optical signal (e.g., a multiplexed optical signal with N wavelength channels  $\lambda_1, \lambda_2, \lambda_3, \dots, \lambda_N$ ) with two orthogonal polarizations, e.g., TE polarization and TM polarization. The input beam **3415** may be split according to polarization, with the TE polarization generally being outputted from the first output **3402B** and the TM polarization generally being outputted from the second output **3402C**.

Each of the first and second WDM demuxes **3404** and **3406** may be optimized for and/or specific to one of the two polarizations depending on the polarization of light that is input to the first or second WDM demux **3404** or **3406**. For example, the first WDM demux **3404** in FIGS. **34A** and **34B** and the second WDM demux **3406B** in FIG. **34B** may be optimized for or specific to the TE polarization. The second WDM demux **3406A** in FIG. **34A** may be optimized for or specific to the TM polarization. In these and other embodiments, each of the first and second WDM demuxes **3404** and **3406** may include an Echelle grating with a polarization-dependent filter function.

The first WDM demux **3404** includes an input **3416** optically coupled to the first output **3402B** of the polarization splitter **3402**. Analogously, the second WDM demux **3406A** or **3406B** respectively includes an input **3418** or **3420** optically coupled to the second output **3402C** or to the polarization splitter **3402**.

The first WDM demux **3404** additionally includes outputs **3422** optically coupled to the first opto-electrical transducers **3408**. Analogously, the second WDM demux **3406A** or **3406B** respectively includes outputs **3424** or **3426** optically coupled to the second opto-electrical transducers **3410**. The first opto-electrical transducers **3408** and the second opto-electrical transducers **3410** may each include at least N PN diodes, avalanche photodiodes (APDs), or other suitable optical receivers.

The adders **3412** are electrically coupled to outputs of the first and second opto-electrical transducers **3408** and **3410**, where each of the adders **3412** is electrically coupled to an output of a corresponding one of the first opto-electrical transducers **3408** and to an output of a corresponding one of

the second opto-electrical transducers **3410**. In particular, for  $i=1$  to N, an  $i$ th one of the adders **3412** may be electrically coupled to an  $i$ th one of the first opto-electrical transducers **3408** and to an  $i$ th one of the second opto-electrical transducers **3410** to sum an electrical output of the  $i$ th one of the first opto-electrical transducers **3408** with an electrical output of the  $i$ th one of the second opto-electrical transducers **3410** to generate an  $i$ th combined electrical output **3428**.

In FIGS. **34A** and **34B**, in operation, the first WDM demux **3404** receives the TE polarization of the input beam **3415** and demultiplexes it into N distinct wavelength channels  $\lambda_1, \lambda_2, \lambda_3, \dots, \lambda_N$  that are output to the first opto-electrical transducers **3408**. The first opto-electrical transducers **3408** each output an electrical signal representative of a corresponding one of the N distinct wavelength channels received at the corresponding one of the first opto-electrical transducers **3408**.

In FIG. **34A**, in operation, the second WDM demux **3406A** receives the TM polarization of the N-channel optical signal from the second output **3402C** of the polarization splitter **3402** and demultiplexes it into N distinct wavelength channels that are output to the second opto-electrical transducers **3410**. The second opto-electrical transducers **3410** each output an electrical signal representative of a corresponding one of the N distinct wavelength channels received at the corresponding one of the second opto-electrical transducers **3410**.

In FIG. **34B**, in operation, the polarization rotator **3414** rotates a polarization of the TM polarization received from the second output **3402C** of the polarization splitter **3402** from the TM polarization to the TE polarization. In this and other embodiments, the polarization rotator **3414** may include a TM-to-TE polarization rotator. More generally, the polarization rotator **3414** may rotate the polarization from a first (or second) polarization to an orthogonal second (or first) polarization. The second WDM demux **3406A** then receives the polarization-rotated signal from the polarization rotator **3414** and demultiplexes it into N distinct wavelength channels that are output to the second opto-electrical transducers **3410**. The second opto-electrical transducers **3410** each output an electrical signal representative of a corresponding one of the N distinct wavelength channels received at the corresponding one of the second opto-electrical transducers **3410**.

In both FIGS. **34A** and **34B**, the adders **3412** then combine the appropriate outputs from the first and second opto-electrical transducers **3408** and **3410** to generate an  $i$ th combined electrical signal **3428** that is representative of the  $i$ th wavelength channel from the input beam **3415** received at the input **3402A** of the polarization splitter **3402**. In particular, a first (or second, or third, or Nth) one of the  $i$ th combined electrical signals **3428** includes a sum of the electrical output of a first (or second, or third, or Nth) one of the first electro-optical transducers **3408** that is representative of a first (or second, or third, or Nth) one of the N distinct wavelength channels output by the first WDM demux **3404** and the electrical output of a first (or second, or third, or Nth) one of the second electro-optical transducers **3410** that is representative of a first (or second, or third, or Nth) one of the N distinct wavelength channels output by the second WDM demux **3406A**.

By splitting the TE polarization from the TM polarization, demultiplexing each separately from the other, and then adding corresponding channels with the adders **3412**, the demultiplexer systems **3400** of FIGS. **34A** and **34B** may eliminate or at least significantly reduce channel cross-talk that arises in WDM demuxes with polarization-dependent filter functions.

Various considerations and parameters associated with a Si PIC polarization splitter, such as the polarization splitter **3402**, will now be discussed with respect to FIGS. **35-37**,



followed by a discussion of various example Si PIC polarization splitters with respect to FIGS. 38A-38C.

FIG. 35 is a graphical representation 3500 of a simulation of effective index as a function of Si waveguide width for TE and TM polarizations in Si and SiN waveguides of an adiabatic coupler region, arranged in accordance with at least one embodiment described herein. It can be seen from curves 3506 and 3508 of FIG. 35 that the effective index for TE and TM polarizations in the SiN waveguide does not vary with Si waveguide width and has a value of about 1.7. It can be seen from curves 3502 and 3504 of FIG. 35 that the effective index for TE polarization in the Si waveguide (see curve 3502) is less than 1.7 in the region from 130 nm to 180 nm (or 0.13  $\mu$ m to 0.18  $\mu$ m) and increases across this region, and the effective index for TM polarization in the Si waveguide (see curve 3504) is greater than 1.7 in the region from 130 nm to 180 nm and increases across this region. As such, TE and TM polarizations will necessarily have different coupling efficiencies in the adiabatic coupler region if a tip width of a tapered end of the Si waveguide is between 130 nm to 180 nm. Differences between the TE and TM coupling efficiencies for various tip widths in the 130 nm to 180 nm range are illustrated in FIGS. 36 and 37.

The Si waveguide width at which the effective index for TM polarization in the Si waveguide (curve 3504) crosses over the effective index for TM polarization in the SiN waveguide (curve 3508) may be referred to herein as a "TM maximum taper width", and is about 100 nm in FIG. 35. If a tip width of a tapered end of the Si waveguide is greater than the TM maximum taper width, it can be seen from FIG. 35 that adiabatic coupling with high efficiency of the TM polarization between the Si waveguide and the SiN waveguide may be prevented relative to coupling efficiency of the TE polarization. Analogously, the Si waveguide width at which the effective index for TE polarization in the Si waveguide (curve 3502) crosses over the effective index for TE polarization in the SiN waveguide (curve 3506) may be referred to herein as a "TE maximum taper width", and is about 180 nm in FIG. 35. If a tip width of a tapered end of the Si waveguide is less than the TE maximum taper width, it can be seen from FIG. 35 that adiabatic coupling with high efficiency of the TE polarization between the Si waveguide and the SiN waveguide may be permitted relative to coupling efficiency of the TM polarization.

FIG. 36 is a graphical representation 3600 of a simulation of TE and TM polarization coupling efficiency as a function of Si waveguide taper length for a Si waveguide tip width of 180 nm and 150 nm, arranged in accordance with at least one embodiment described herein. In particular, for a tip width of 180 nm, curve 3602 represents TE coupling efficiency while curve 3604 represents TM coupling efficiency. Analogously, for a tip width of 150 nm, curve 3606 represents TE coupling efficiency while curve 3608 represents TM coupling efficiency. It can be seen from curves 3602, 3604, 3606, and 3608 that at both tip widths, the TE polarization (curves 3602 and 3606) has a much better coupling efficiency than the TM polarization (curves 3604 and 3608). Curves 3602 and 3606 tend to indicate that for tip widths equal to or greater than 180 nm, TE coupling may be below 90%. Curves 3604 and 3608 tend to indicate that for tip widths less than or equal to 150 nm, TM coupling may be greater than 10%.

FIG. 37 is a graphical representation 3700 of a simulation of TE and TM polarization coupling efficiency as a function of Si waveguide taper length for a Si waveguide tip width of 160 nm for three different wavelength channels at 1.35  $\mu$ m, 1.31  $\mu$ m, and 1.27  $\mu$ m, arranged in accordance with at least one embodiment described herein. The tip width of 160 nm is

selected as a compromise between 150 nm (below which TM coupling may be greater than 10%) and 180 nm (above which TE coupling efficiency may be less than 90%). For a tip width of 160 nm and a 1.35  $\mu$ m wavelength channel, curve 3702A represents TE coupling efficiency while curve 3702B represents TM coupling efficiency. Analogously, for a tip width of 160 nm and a 1.31  $\mu$ m wavelength channel, curve 3704A represents TE coupling efficiency while curve 3704B represents TM coupling efficiency. Analogously, for a tip width of 160 nm and a 1.27  $\mu$ m wavelength channel, curve 3706A represents TE coupling efficiency while curve 3706B represents TM coupling efficiency. It can be seen from curves 3702A, 3702B, 3704A, 3704B, 3706A, and 3706B that at all three wavelength channels, the TE polarization (curves 3702A, 3704A, and 3706A) has a much better coupling efficiency than the TM polarization (curves 3702B, 3704B, and 3706B).

FIG. 37 additionally includes a table 3708 with various TE and TM polarization coupling efficiency values for the three wavelength channels at 1.35  $\mu$ m, 1.31  $\mu$ m, and 1.27  $\mu$ m where the Si waveguide taper length is about 200  $\mu$ m. For each wavelength channel, a ratio of TE polarization coupling efficiency to TM polarization coupling efficiency is also provided in units of decibels (dB).

The simulations of FIGS. 35-37 indicate that, at least in some embodiments, an adiabatic coupler region that includes a Si waveguide with a tip width between 130 nm to 180 nm, or between 150 nm to 180 nm, or at about 160 nm, may be used to selectively couple most of the TE polarization from the Si waveguide to the SiN waveguide (or vice versa) without coupling most of the TM polarization from the Si waveguide to the SiN waveguide (or vice versa). Two or more such adiabatic coupler regions may be combined as described in more detail with respect to FIGS. 38A-38C to form a Si PIC polarization splitter or combiner, such as the polarization splitter 3402 discussed above.

FIGS. 38A-38C illustrate example Si PIC polarization splitters or combiners 3800A, 3800B, and 3800C (hereinafter collectively "polarization splitters 3800"), arranged in accordance with at least one embodiment described herein. The polarization splitters 3800 may include or correspond to the polarization splitter 3402 of FIGS. 34A and 34B and may be implemented in the demultiplexer systems 3400 of FIGS. 34A and 34B and/or in other systems or devices.

FIGS. 38A-38C each include an overhead view of the polarization splitter 3800A, 3800B, or 3800C. The overhead views of FIGS. 38A-38C include outlines or footprints of various components of the polarization splitters 3800 at different levels in a material stack up of the polarization splitters 3800 that may not necessarily be visible when viewed from above, but are shown as outlines or footprints to illustrate x and z alignment of the various components with respect to each other.

Each of the polarization splitters 3800 includes a first SiN waveguide 3802, a second SiN waveguide 3804 spaced apart from the first SiN waveguide 3802, and a Si waveguide 3806. The first and second SiN waveguides 3802 and 3804 may be formed in a first layer of a Si PIC, such as any of the first layers with SiN waveguides described herein. The Si waveguide 3806 may be formed in a second layer of the Si PIC that is above or below the first layer of the Si PIC, such as any of the second layers with Si waveguides described herein.

The first SiN waveguide 3802 includes a coupler portion 3808, the second SiN waveguide 3804 includes a coupler portion 3810, and the Si waveguide 3806 includes a first tapered end 3812 and a second tapered end 3814. The first tapered end 3812 is aligned in two orthogonal directions (e.g.,



41

x and z) with the coupler portion **3808** of the first SiN waveguide **3802** such that the first tapered end **3812** overlaps in the two orthogonal directions and is parallel to the coupler portion **3808** of the first SiN waveguide **3802**. The first tapered end **3812** and the coupler portion **3808** of the first SiN waveguide **3802** may generally form a first adiabatic coupler region **3816**. Analogously, the second tapered end **3814** is aligned in two orthogonal directions (e.g., x and z) with the coupler portion **3810** of the second SiN waveguide **3804** such that the second tapered end **3814** overlaps in the two orthogonal directions and is parallel to the coupler portion **3810** of the second SiN waveguide **3804**. The second tapered end **3814** and the coupler portion **3810** of the second SiN waveguide **3804** may generally form a second adiabatic coupler region **3818**.

Each of the first and second tapered ends **3812** and **3814** of the Si waveguide **3806** may be configured to adiabatically couple most of a first polarization (e.g., TE polarization) of an input beam **3820** between a corresponding one of the first and second tapered ends **3812** and **3814** of the Si waveguide **3806** and a corresponding one of the first and second SiN waveguides **3802** and **3804** and to prevent most of a second polarization (e.g., TM polarization) of the input beam **3820** that is orthogonal to the first polarization from being adiabatically coupled between the corresponding one of the first and second tapered ends **3812** and **3814** and the corresponding one of the first and second SiN waveguides **3802** and **3804**. The foregoing may be accomplished by providing each of the first and second tapered ends **3812** and **3814** of the Si waveguide **3806** with an appropriate tip width that generally discriminates between the first and second polarizations.

In more detail, the first tapered end **3812** of the Si waveguide **3806** may have a tip width configured to adiabatically couple most of the first polarization from the first SiN waveguide **3802** through the first tapered end **3812** to the Si waveguide **3806** and to prevent most of the second polarization from entering the Si waveguide **3806**. For example, the first tapered end **3812** may have a tip width in a range between 130 nm and 180 nm, or in a range between 150 nm and 180 nm, or a tip width of about 160 nm. Analogously, the second tapered end **3814** of the Si waveguide **3804** may have a tip width configured to adiabatically couple most of a portion of the first polarization propagating through the Si waveguide **3806** from the Si waveguide **3806** through the second tapered end **3814** to the second SiN waveguide **3804** and to prevent most of a portion of the second polarization propagating through the Si waveguide **3806** from entering the second SiN waveguide **3804**. For example, the second tapered end **3814** may have a tip width in a range between 130 nm and 180 nm, or in a range between 150 nm and 180 nm, or a tip width of about 160 nm. Accordingly, and consistent with FIGS. 35-37, a tip width of the first and second tapered ends **3812** and **3814** may be configured to selectively couple most of the first polarization of the input beam **3820** from the first SiN waveguide **3802** to the second SiN waveguide **3804** without coupling most of the second polarization from the first SiN waveguide **3802** to the second SiN waveguide **3804**.

In the example of FIG. 38A, the Si waveguide **3806** may have a taper length of 200 nm (e.g., each of the first and second tapered ends **3812** and **3814** may be 200 nm long in a light propagation direction) and each of the first and second tapered ends **3812** and **3814** may have a tip width of 150 nm. Alternatively or additionally, the first and second SiN waveguides **3802** and **3804** may each have a width of 1  $\mu$ m and each of the first and second tapered ends **3812** and **3814** may have a maximum width of 320 nm. In this example, and for a 1.31  $\mu$ m wavelength channel, each of the first and second

42

adiabatic coupler regions **3816** and **3818** may adiabatically couple about 98% of the TE polarization and about 10% of the TM polarization from one waveguide to the next (e.g., from the first SiN waveguide **3802** to the Si waveguide **3806** or from the Si waveguide **3806** to the second SiN waveguide **3804**) and may prevent about 2% of the TE polarization and about 90% of the TM polarization from being adiabatically coupled from one waveguide to the next. As a result, in FIG. 38A, an output beam **3822** from an end **3824** of the first SiN waveguide **3802** may include about 2% of the TE polarization and about 90% of the TM polarization of the input beam **3820**. Because an output beam **3826** from an end **3828** of the second SiN waveguide **3804** passes through both the first and the second adiabatic coupler regions **3816** and **3818**, the output beam **3826** may include about 96% of the TE polarization and about 1% of the TM polarization of the input beam **3820**.

In FIGS. 38B and 38C, each of the polarization splitters **3800B** and **3800C** additionally includes a third adiabatic coupler region **3830** or **3832** to improve a split ratio of the TE and TM polarizations in the output beam **3822** from the end **3824** of the first SiN waveguide **3802**. The third adiabatic coupler region **3830** or **3832** may be made up of a second coupler portion **3834** of the first SiN waveguide **3802** and a tapered end **3836** or **3838** of a second Si waveguide **3840** or **3842**. The second Si waveguide **3840** or **3842** may be formed in the same layer of the Si PIC as the Si waveguide **3806**, or in a different layer of the Si PIC than the Si waveguide **3806**.

Alternatively or additionally, the first SiN waveguide **3802** may include a tapered end **3844** upstream of the coupler portion **3808**. In an example embodiment, the tapered end **3844** of the first SiN waveguide **3802** has a taper length (e.g., a length in the z direction) of about 50  $\mu$ m. SiN waveguides in Si PICs according to some embodiments described herein may generally have a width (e.g., in the x direction) of about 0.7  $\mu$ m or less, and may be referred to as standard SiN waveguides. In comparison, SiN waveguides in Si PIC polarization splitters such as the polarization splitters **3402** and **3800** described herein may have different widths than the standard SiN waveguides, e.g., widths of about 1  $\mu$ m, and may be referred to as polarization splitter SiN waveguides. The tapered end **844** of the first SiN waveguide **3802** may serve as a transition from a standard SiN waveguide to the first SiN waveguide **3802** which is a polarization splitter SiN waveguide.

The tapered end **3836** or **3838** of the second Si waveguide **3840** or **3842** is aligned in two orthogonal directions (e.g., x and z) with the second coupler portion **3834** of the first SiN waveguide **3802** such that the tapered end **3836** or **3838** of the second Si waveguide **3840** or **3842** overlaps in the two orthogonal directions and is parallel to the second coupler portion **3834** of the first SiN waveguide **3802**. The second Si waveguide **3840** in FIG. 38B generally includes an S shape, whereas the second Si waveguide **3842** in FIG. 38C generally includes a U shape. Other shapes may alternatively be implemented. In some embodiments, each of the second Si waveguides **3840** and **3842** includes a second tapered end **3846** or **3848** opposite the tapered end **3836** or **3838**. In other embodiments, each of the second Si waveguides **3840** and **3842** terminates at a germanium (Ge) PIN detector rather than with the second tapered end **3846** or **3848**.

Each of the tapered ends **3836** or **3838** of the second Si waveguide **3840** or **3842** may have an appropriate tip width to generally discriminate between the first and second polarizations. In more detail, the tapered end **3836** or **3838** of the second Si waveguide **3840** or **3842** may have a tip width configured to adiabatically couple most of the first polarization from the first SiN waveguide **3802** through the tapered

43

end **3836** or **3838** to the second Si waveguide **3840** or **3842** and to prevent most of the second polarization from entering the second Si waveguide **3840** or **3842**. For example, the tapered end **3836** or **3838** may have a tip width in a range between 130 nm and 180 nm, or in a range between 150 nm and 180 nm, or a tip width of about 160 nm. In some embodiments, the second tapered end **3846** or **3848** of the second Si waveguide **3840** or **3842** may similarly have a tip width in a range between 130 nm and 180 nm, or in a range between 150 nm and 180 nm, or a tip width of about 160 nm.

In the example of FIGS. **38B** and **38C**, the Si waveguide **3806** may have a taper length of 200 nm and each of the first and second tapered ends **3812** and **3814** may have a tip width of 160 nm. Alternatively or additionally, the second Si waveguide **3840** or **3842** may also have a taper length of 200 nm, each of the tapered end **3836** or **3838** and the second tapered end **3846** or **3848** may have a tip width of 160 nm, and the first and second SiN waveguides **3802** and **3804** may have a width of 1  $\mu$ m. Alternatively or additionally, the first and second tapered ends **3812** and **3814** of the Si waveguide **3806**, the tapered end **3836** or **3838** of the second Si waveguide **3840** or **3842**, and/or the second tapered end **3846** or **3848** of the second Si waveguide **3840** or **3842** may have a maximum width of 320 nm. In this example, and for a 1.31  $\mu$ m wavelength channel, each of the first, second, and third adiabatic coupler regions **3816**, **3818**, and **3830** or **3832** may adiabatically couple about 97.7% of the TE polarization and about 6.7% of the TM polarization from one waveguide to the next (e.g., from the first SiN waveguide **3802** to the Si waveguide **3806**, from the Si waveguide **3806** to the second SiN waveguide **3804**, or from the first SiN waveguide **3802** to the second Si waveguide **3840** or **3842**) and may prevent about 2.3% of the TE polarization and about 93.3% of the TM polarization from being adiabatically coupled from one waveguide to the next. As a result, and because the output beam **3822** passes through both the first and third adiabatic coupler regions **3816** and **3830**, the output beam **3822** from the end **3824** of the first SiN waveguide **3802** may include about 0.05% of the TE polarization and about 87% of the TM polarization of the input beam **3820**. Also, because the output beam **3826** from the end **3828** of the second SiN waveguide **3804** passes through both the first and the second adiabatic coupler regions **3816** and **3818**, the output beam **3826** may include about 95% of the TE polarization and about 0.5% of the TM polarization of the input beam **3820**. As such, in the example of FIGS. **38B** and **38C**, the ratio of TM/TE in the output beam **3822** may be about 32 dB, and the ratio of TE/TM in the output beam **3826** may be about 23 dB. More generally, the tip widths of one or both of the first and second tapered ends **3812**, **3814** of the Si waveguide **3806** may be configured to pass at least 80% of the TM polarization through the first SiN waveguide **3802** and to adiabatically pass at least 90% of the TE polarization from the first SiN waveguide **3802** to the second SiN waveguide **3804**.

Alternatively or additionally, one or more of the polarization splitters **3800** may be implemented as a polarization combiner. In these and other embodiments, a TM input beam may be received at the end **3824** of the first SiN waveguide **3802** and a TE input beam may be received at the end **3828** of the second SiN waveguide **3804**. In this example, the second tapered end **3814** of the Si waveguide **3806** may have a tip width in a range between 130 nm and 180 nm, or even less than 130 nm. The first tapered end **3812** of the Si waveguide **3806** may have a tip width in a range between 130 nm and 180 nm, or in a range between 150 nm and 180 nm, or a tip width of about 160 nm. The TM input beam may propagate through the first SiN waveguide **3802** from right to left. The TE input

44

beam may propagate through the second SiN waveguide **3804** from right to left and may be adiabatically coupled through the adiabatic coupler region **3818** into the Si waveguide **3806** and through the adiabatic coupler region **3816** into the first SiN waveguide **3802** where it is combined with the TM input.

FIGS. **39A** and **39B** include side views that depict alignment and attachment of a high index glass interposer **3900** (hereinafter “interposer **3900**”) and the Si PIC **1700** of FIG. **17**, arranged in accordance with at least one embodiment described herein. The interposer **3900** includes a high index glass waveguide block **3902** and one or more interposer waveguides **3904**. The interposer waveguides **3904** may include high index glass waveguides that may be written into the high index glass waveguide block **3902**, e.g., by ion exchange method or UV laser writing or other suitable index altering radiation or process.

As illustrated in FIG. **39A**, the interposer **3900** is aligned to the etched window **1702** of the Si PIC **1700** with the interposer cores **3904** generally aligned in the x and z directions with the SiN waveguides **1712** of the Si PIC **1700** in the manner described above to form adiabatic coupler regions. The etched window **1702** may be at least partially filled with the epoxy underfill **1902**. As illustrated in FIG. **39A**, the interposer **3900** may then be moved towards the Si PIC **1700** (or vice versa) as indicated by the arrow **3906** until the interposer cores **3904** are in direct or at least close contact with the SiN waveguides **1712** of the Si PIC **1700**.

In the illustrated embodiment, the high index glass waveguide block **3902** defines one or more holes or grooves **3908** that extend vertically from a bottom surface of the high index glass waveguide block **3902**, e.g., in the positive y direction. Each of the holes or grooves **3908** may have a height (e.g., in the y direction) of 15  $\mu$ m to 20  $\mu$ m, or some other height. Each of the holes or grooves may extend a length (e.g., in the z direction) of a portion of the interposer **3900** configured to be received within the etched window **1702**. The portion of the interposer **3900** configured to be received within the etched window **1702** may be between 2 mm to 3 mm in length in some embodiments. Alternatively or additionally, a width in the x direction of the interposer **3900** may be about 1.5 mm in some embodiments.

When the interposer **3900** is inserted into the etched window **1702** of the Si PIC **1700**, the interposer **3900** may be pressed sufficiently tight against the Si PIC **1700** to at least partially displace the epoxy underfill **902** and thin it out so there is relatively little epoxy underfill **1902** between the interposer waveguides **3904** and the SiN waveguides **1712**. For instance, a thickness (e.g., in the y direction) of the epoxy underfill **1902** in the attached configuration of FIG. **39B** may be less than 1  $\mu$ m. The displaced epoxy underfill **1902** may at least partially fill the holes **3908** to achieve good adhesion of the interposer **3900** to the Si PIC **1700**.

FIG. **40A** includes an upside down perspective view of another high index glass interposer **4000** (hereinafter “interposer **4000**”), arranged in accordance with at least one embodiment described herein. The interposer **4000** includes a high index glass waveguide block **4002** and one or more interposer waveguides **4004**. The interposer waveguides **4004** may include high index glass waveguides that may be written into the high index glass waveguide block **4002**, e.g., by ion exchange, UV laser writing, or other suitable index altering radiation or process. The interposer **4000** additionally defines v-grooves **4006** longitudinally adjacent to the interposer waveguides **4004**.

FIG. **40B** includes a perspective view of the interposer **4000** adiabatically coupled to a Si PIC **4008**, arranged in accordance with at least one embodiment described herein.

45

The interposer **4000** is illustrated in FIG. **40B** as being transparent to allow the interposer waveguides **4004** and the v-grooves **4006** generally on a bottom surface of the interposer **4000** to be perceived. As can be seen from FIG. **40B**, the interposer waveguides **4004** are generally disposed within an etched window **4010** defined through one or more dielectric layers of the Si PIC above a first layer of the Si PIC **4008**. The first layer may include one or more SiN waveguides to which the interposer waveguides **4004** are adiabatically coupled within the etched window **4010**.

FIG. **40B** additionally illustrates optical fibers **4012** to which the interposer waveguides **4004** may be optically coupled. In particular, ends of the optical fibers may be stripped of a jacket and/or waveguide cladding such that optical fiber cores of the optical fibers **4012** are positioned within the v-grooves **4006**. Insofar as the v-grooves **4006** may generally be optically aligned to the interposer waveguides **4004**, positioning the optical fibers **4012** such that their optical fiber cores are positioned within the v-grooves **4006** may generally optically align each of the optical fibers **4012** to a corresponding one of the interposer waveguides **4004**.

With respect to the use of substantially any plural and/or singular terms herein, those having skill in the art can translate from the plural to the singular and/or from the singular to the plural as is appropriate to the context and/or application. The various singular/plural permutations may be expressly set forth herein for sake of clarity.

The present invention may be embodied in other specific forms without departing from its spirit or essential characteristics. The described embodiments are to be considered in all respects only as illustrative and not restrictive. The scope of the invention is, therefore, indicated by the appended claims rather than by the foregoing description. All changes which come within the meaning and range of equivalency of the claims are to be embraced within their scope.

What is claimed is:

1. A coupled system comprising:

a first waveguide having a first refractive index  $n_1$  and a tapered end;

at least one second waveguide, each having a second refractive index  $n_2$ ;

an interposer comprising a third waveguide having a third refractive index  $n_3$  and a coupler portion, wherein:

the tapered end of the first waveguide is adiabatically coupled to a coupler portion of one of the at least one second waveguide;

a tapered end of one of the at least one second waveguide is adiabatically coupled to the coupler portion of the third waveguide of the interposer;

$n_1 > n_2 > n_3$ ; and

the coupled system is configured to adiabatically couple light between the first waveguide and the at least one second waveguide and between the at least one second waveguide and the third waveguide.

2. The coupled system of claim 1 wherein:

the first waveguide has a first optical mode size;

each of the at least one second waveguide has a second optical mode size;

the third waveguide of the interposer has a third optical mode size;

the first optical mode size is substantially smaller than the second optical mode size; and

the second optical mode size is substantially smaller than the third optical mode size.

3. The coupled system of claim 2, wherein the third optical mode size of the third waveguide of the interposer is substantially similar to the mode size of a standard single mode

46

optical fiber, thereby providing for efficient optical coupling of light from the first waveguide to single mode optical fiber.

4. The coupled system of claim 1, wherein the first waveguide and at the least one second waveguide are in a silicon (Si) photonic system and fabricated in a same Si photonic integrated circuit process and wherein the third waveguide of the interposer is formed in a different material system and attached separately to the Si photonic integrated circuit.

5. The coupled system of claim 1, wherein the first waveguide comprises a silicon (Si) core and silicon dioxide ( $\text{SiO}_2$ ) cladding such that the first waveguide comprises a Si waveguide and each of the at least one second waveguide comprises a silicon nitride (SiN) core and  $\text{SiO}_2$  cladding such that the at least one second waveguide comprises a SiN waveguide.

6. The coupled system of claim 5, wherein the third waveguide of the interposer comprises a polymer.

7. The coupled system of claim 5, wherein the third waveguide of the interposer comprises a high index glass waveguide.

8. The coupled system of claim 1, wherein a value of the first refractive index  $n_1$  is in a range of 3 to 3.5 and a value of the second refractive index  $n_2$  is in a range of 1.8 to 2.2.

9. The coupled system of claim 8, wherein a value of the third refractive index of the interposer is in a range of 1.49 to 1.6.

10. The coupled system of claim 5, wherein a width of the tapered end of the Si waveguide tapers from a first width in a range from 300-330 nanometer (nm) to a tip width of about 80 nm and wherein a width of the tapered end of the SiN waveguide tapers from a first width in a range from 600 nm to 1000 nm to a tip width in a range from 170 nm to 230 nm.

11. The coupled system of claim 1, further comprising: the plurality of first waveguides that includes the first waveguide, each having the first refractive index  $n_1$ , a first end, and a tapered end opposite the first end;

a plurality of second waveguides that includes the at least one second waveguide;

a plurality of third waveguides included in the interposer, each having the third refractive index  $n_3$  and a coupler portion, wherein:

the tapered end of each of the plurality of first waveguides is adiabatically coupled to the coupler portion of a corresponding one of the plurality of second waveguides;

the tapered end of each of the plurality of second waveguides is adiabatically coupled to the coupler portion of a corresponding one of the plurality of third waveguides;

the interposer comprises a high index glass waveguide block within which the plurality of third waveguides are formed;

the plurality of third waveguides include a plurality of receive interposer waveguides and a plurality of transmit interposer waveguides;

at an input/output surface of the high index glass waveguide block that is configured to be coupled to an optical fiber end connector, ends of the plurality of receive interposer waveguides and the plurality of transmit interposer waveguides have a double-decker arrangement configured to match an arrangement of receive optical fibers and transmit optical fibers to which the optical fiber end connector is coupled.

47

12. The coupled system of claim 1, further comprising:  
 a semiconductor laser;  
 a first lens positioned in an optical path between the semiconductor laser and an input end of the third waveguide of the interposer;  
 an optical isolator positioned in the optical path after the first lens; and  
 a second lens positioned in the optical path after the optical isolator,  
 wherein the coupled system is configured to adiabatically couple light emitted by the semiconductor laser and received in the third waveguide of the interposer from the third waveguide to the at least one second waveguide and from the at least one second waveguide to the first waveguide.
13. The coupled system of claim 1, wherein:  
 the coupled system further comprises a plurality of second waveguides that includes the at least one second waveguide, a plurality of second input waveguides and a second output waveguide, each having the second refractive index  $n_2$ ;  
 a coupler portion of the second output waveguide is adiabatically coupled to the tapered end of the first waveguide;  
 the coupled system further comprises:  
   a wavelength division multiplexer (WDM mux) with a plurality of inputs each coupled to a corresponding one of the plurality of second input waveguides and an output coupled to the second output waveguide;  
   a plurality of third waveguides included in the interposer, each having the third refractive index  $n_3$  and a coupler portion, wherein the coupler portion of each of the plurality of third waveguides is adiabatically coupled to a tapered end of a corresponding one of the plurality of second input waveguides;  
   a plurality of semiconductor lasers;  
   a plurality of first lenses, each positioned in a corresponding optical path between a corresponding one of the plurality of semiconductor lasers and an input end of a corresponding one of the plurality of third waveguides;  
   a plurality of optical isolators, each positioned in the corresponding optical path after the corresponding one of the plurality of first lenses; and  
   a plurality of second lenses, each positioned in the corresponding optical path after the corresponding one of the plurality of optical isolators.
14. The coupled system of claim 1, wherein:  
 the coupled system further comprises a plurality of second waveguides, each having the second refractive index  $n_2$ ;  
 a tapered end of a first one of the plurality of second waveguides is adiabatically coupled to the coupler portion of the third waveguide;  
 the coupled system further comprises:  
   an arrayed waveguide grating (AWG) with a first input or output coupled to the first one of the plurality of second waveguides and with a plurality of second outputs or inputs each coupled to a corresponding one of others of the plurality of second waveguides; and  
   a plurality of first waveguides that includes the first waveguide, each having the first refractive index  $n_1$  and a tapered end, wherein the tapered end of each of the plurality of first waveguides is adiabatically coupled to a coupler portion of a corresponding one of the others of the plurality of second waveguides.
15. The coupled system of claim 1, wherein the first waveguide and the at least one second waveguide are formed

48

- in a silicon (Si) photonic integrated circuit (PIC), the coupled system further comprising a semiconductor chip wafer bonded to the Si PIC, wherein:  
   the semiconductor chip comprises an active optical device optically coupled to an end of the first waveguide opposite the tapered end of the first waveguide; and  
   the active optical device comprises an indium phosphide (InP)-based gain element or an InP-based pin detector.
16. The coupled system of claim 1, further comprising a silicon (Si) photonic integrated circuit (PIC), including:  
   a substrate;  
   silicon dioxide ( $\text{SiO}_2$ ) box formed above the substrate;  
   a first layer formed above the  $\text{SiO}_2$  box and in which the at least one second waveguide is formed as at least one silicon nitride (SiN) waveguide;  
   a second layer formed above the  $\text{SiO}_2$  box and above or below the first layer and in which the first waveguide is formed as a Si waveguide; and  
   a plurality of dielectric layers formed above the first layer, wherein:  
     the Si PIC defines an etched window through the plurality of dielectric layers down to the first layer, wherein the tapered end of the at least one second waveguide is exposed in the etched window;  
     the etched window is laterally bounded on three sides by the dielectric layers of the Si PIC that are above the first layer;  
     a top layer included in the dielectric layers of the Si PIC includes a plurality of metal dummies at least in a region of the top layer that bounds the etched window.
17. The coupled system of claim 16, wherein:  
 the interposer comprises an interposer substrate, an interposer cladding, and an interposer core, the interposer core and the interposer cladding collectively forming the third waveguide;  
 at least a bottom surface of the interposer core is exposed and free of the interposer cladding along the coupler portion of the third waveguide that is positioned within the etched window above the tapered end of the at least one second waveguide;  
 the interposer further comprises at least one interposer alignment ridge that extends downward from the interposer cladding and is laterally offset from the third waveguide;  
 the Si PIC defines at least one anchor window laterally offset from the etched window; and  
 the at least one interposer alignment ridge is positioned within the at least one anchor window to laterally align the third waveguide with the one of the at least one second waveguide.
18. The coupled system of claim 16, wherein:  
 the interposer comprises a high index glass waveguide block;  
 the third waveguide comprises a high index glass waveguide formed in the high index glass waveguide block;  
 the high index glass waveguide block defines one or more holes or grooves laterally offset from the high index glass waveguide;  
 the one or more holes or grooves extend vertically upward from a bottom surface of the high index glass waveguide block;  
 the coupled system further comprises an epoxy underfill positioned within the etched window between at least a portion of the first layer within the etched window and at least a portion of the bottom surface of the high index glass waveguide block;

49

a thickness of the epoxy underfill between the bottom surface of the high index glass waveguide block and the first layer is less than 1 micrometer; and each of the one or more holes or grooves is filled with the epoxy underfill.

19. The coupled system of claim 16, the interposer comprises a high index glass waveguide block;

the third waveguide comprises a high index glass waveguide formed in the high index glass waveguide block;

the high index glass waveguide block defines a v-groove longitudinally adjacent to the high index glass waveguide; and

the v-groove is configured to receive therein at least a portion of an optical fiber and to optically align the optical fiber with the high index glass waveguide.

20. The coupled system of claim 1, wherein the interposer comprises:

a silicon dioxide ( $\text{SiO}_2$ ) substrate;

a silicon oxynitride ( $\text{SiON}$ ) cladding coupled to the  $\text{SiO}_2$  substrate; and

a  $\text{SiON}$  core surrounded on all sides within a first portion of the interposer and having at least one side exposed and free of  $\text{SiON}$  cladding within a second portion of the interposer, wherein the  $\text{SiON}$  cladding and the  $\text{SiON}$  core collectively form the third waveguide.

21. The coupled system of claim 1, wherein the interposer comprises a polymer on glass interposer, including:

a glass substrate;

a polymer cladding coupled to the glass substrate; and

a polymer core surrounded on all sides by the polymer cladding within a first portion of the interposer and having at least one side exposed and free of polymer cladding within a second portion of the interposer, wherein the polymer cladding and the polymer core collectively form the third waveguide.

22. The coupled system of claim 1, further comprising a silicon (Si) photonic integrated circuit (PIC), including:

a substrate;

silicon dioxide ( $\text{SiO}_2$ ) box formed above the substrate;

a first layer formed above the  $\text{SiO}_2$  box and in which the at least one second waveguide and a plurality of second waveguides is formed;

a second layer formed above the  $\text{SiO}_2$  box and above or below the first layer and in which the first waveguide is formed as a Si waveguide; and

a SiN wavelength division demultiplexer (WDM demux) formed in the first layer, wherein an input of the SiN WDM demux is coupled to one of the plurality of SiN waveguides and each of multiple outputs of the SiN WDM demux is coupled to a corresponding different one of the plurality of SiN waveguides.

23. The coupled system of claim 22, further comprising a Si PIC polarization splitter formed in the Si PIC, wherein the Si PIC polarization splitter includes:

50

a first SiN waveguide of the plurality of SiN waveguides formed in the first layer of the Si PIC, wherein the first SiN waveguide includes a coupler portion at a first end of the first SiN waveguide;

a second SiN waveguide of the plurality of SiN waveguides formed in the first layer of the Si PIC and spaced apart from the first SiN waveguide, wherein the second SiN waveguide includes a coupler portion at a first end of the second SiN waveguide; and

the Si waveguide formed in the second layer of the Si PIC, wherein:

the tapered end of the first waveguide includes a first tapered end of the Si waveguide and the Si waveguide further includes a second tapered end opposite the first tapered end;

the first tapered end of the Si waveguide is aligned in two orthogonal directions with the coupler portion of the first SiN waveguide such that the first tapered end of the Si waveguide overlaps in the two orthogonal directions and is parallel to the coupler portion of the first SiN waveguide;

the two orthogonal directions correspond to a length direction and a width direction of the first and second SiN waveguides;

the second tapered end of the Si waveguide is aligned in the two orthogonal directions with the coupler portion of the second SiN waveguide such that the second tapered end of the Si waveguide overlaps in the two orthogonal directions and is parallel to the coupler portion of the second SiN waveguide;

each of the first and second tapered ends of the Si waveguide is configured to adiabatically couple most TE polarization of an input beam between a corresponding one of the first and second tapered ends and a corresponding one of the first and second SiN waveguides and to prevent most TM polarization of the input beam from being adiabatically coupled between the corresponding one of the first and second tapered ends and the corresponding one of the first and second SiN waveguides;

the SiN WDM demux comprises a first SiN WDM demux with its input optically coupled to a second end of the first SiN waveguide that is opposite the first end of the first SiN waveguide; and

the coupled system further comprises a second SiN WDM demux formed in the first layer of the Si PIC with a plurality of outputs and an input optically coupled to a second end of the second SiN waveguide that is opposite the first end of the second SiN waveguide.

24. The photonic system of claim 23, further comprising a polarization rotator disposed in an optical path between the second end of the second SiN waveguide and the input of the second SiN WDM demux.

\* \* \* \* \*